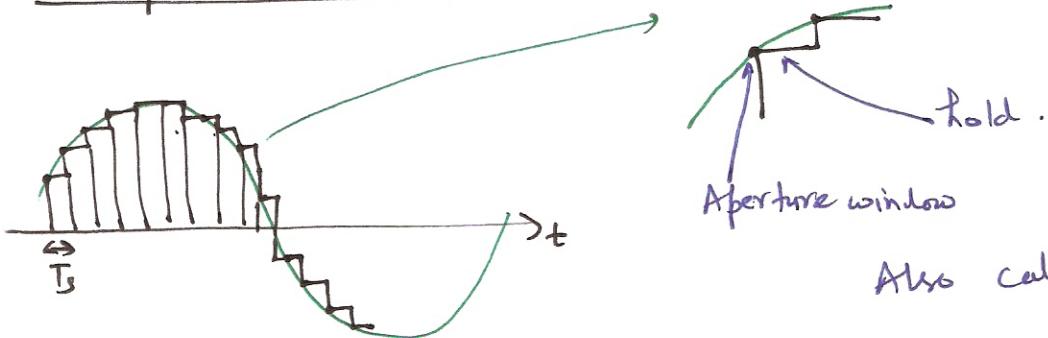


Sample and hold :

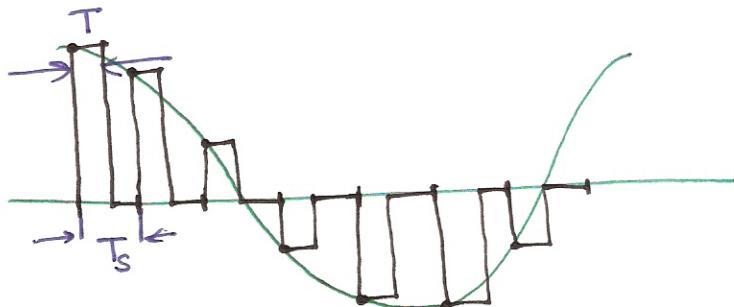


Also called zero-order hold (ZOH).

for NRZ pulse shape.

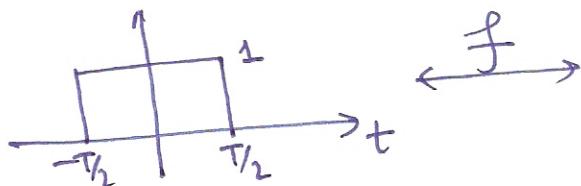
Ideal S/H \rightarrow aperture window is sufficiently narrow w.r.t T_s

Generalized S/H

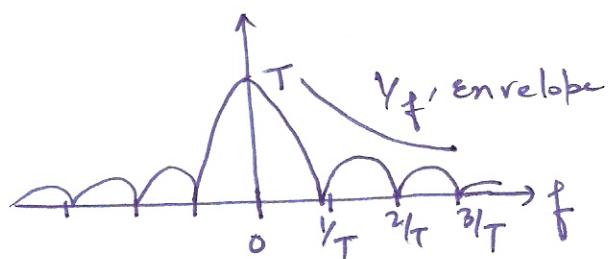


RZ pulse width $\rightarrow T$
Sampling period $\rightarrow T_s$
 $0 < T \leq T_s$

* Recap on Signals



$$\text{sinc}\left(\frac{t}{T}\right)$$



$$T \text{sinc}(ft),$$

$$\text{sinc}(x) = \frac{\sin(\pi x)}{\pi x}$$

We have:

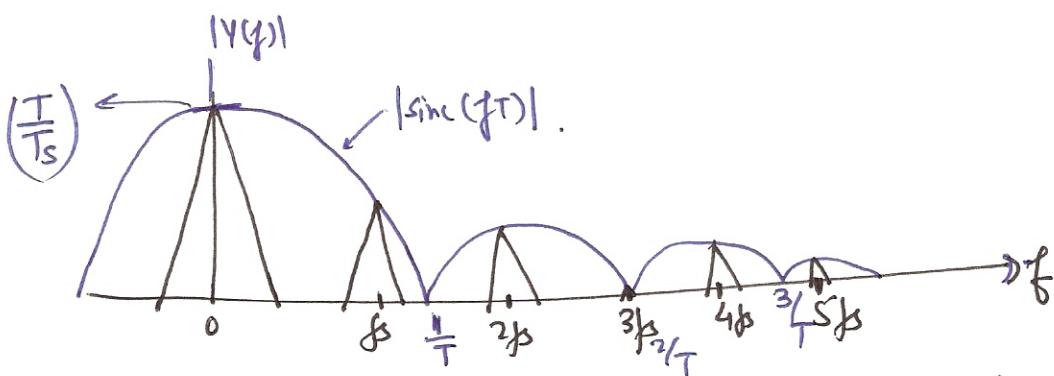
$$\begin{aligned}
 y(t) &= \sum_{n=-\infty}^{\infty} x(nT_s) \cdot \text{sinc}\left(\frac{t-t_2-nT_s}{T}\right) \\
 &= \sum_{n=-\infty}^{\infty} [x(t) \cdot \delta(t-nT_s)] \otimes \text{sinc}\left(\frac{t-t_2}{T}\right) \quad \leftarrow \text{think here!} \\
 &= \left[x(t) \cdot \underbrace{\sum_{n=-\infty}^{\infty} \delta(t-nT_s)}_{p(t)} \right] \otimes \underbrace{\text{sinc}\left(\frac{t-t_2}{T}\right)}_{h(t)} \\
 &= [x(t) \cdot p(t)] \otimes h(t)
 \end{aligned}$$

$$\Rightarrow Y(f) = [X(f) \otimes P(f)] \cdot H(f)$$

$$\begin{aligned}
 \rightarrow H(f) &= \mathcal{F}\left(\text{sinc}\left(\frac{t-t_2}{T}\right)\right) \\
 &= T \text{sinc}(fT) \cdot e^{-j\pi fT}
 \end{aligned}$$

$$\Rightarrow |H(f)| = T |\text{sinc}(fT)|.$$

$$\Rightarrow Y(f) = \left(\frac{T}{T_s} \sum_{k=-\infty}^{\infty} X(f - kf_s) \right) \cdot \underbrace{\text{sinc}(fT)}_{\text{sinc distortion!}} \cdot e^{-j\pi fT}$$



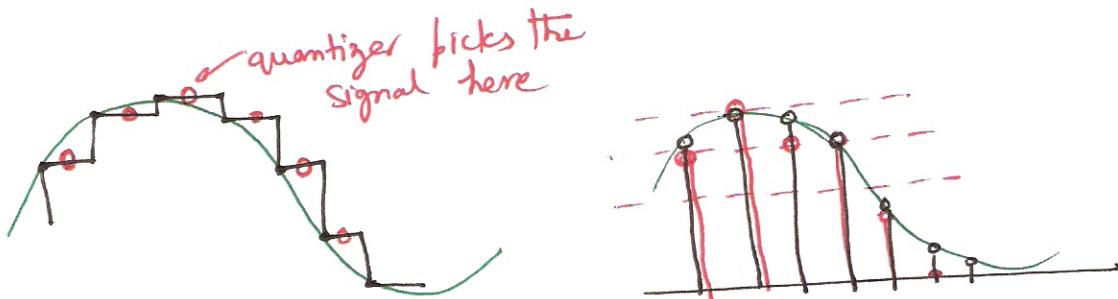
The replicas are weighted by the sinc response.

for $T=T_S \Rightarrow X_0 H \rightarrow$ worst Sinc distortion

for $\frac{T}{T_S} \rightarrow 0$, sinc distortion vanishes but the output signal power of the S/H diminishes.

* Is the S/H's sinc distortion a problem in an ADC with a S/H in the front-end ??

Ans → No!



In an ADC, the quantizer senses the output of the front-end S/H. only during the hold mode.

↳ the quantized value only corresponds to the sampled points on the input

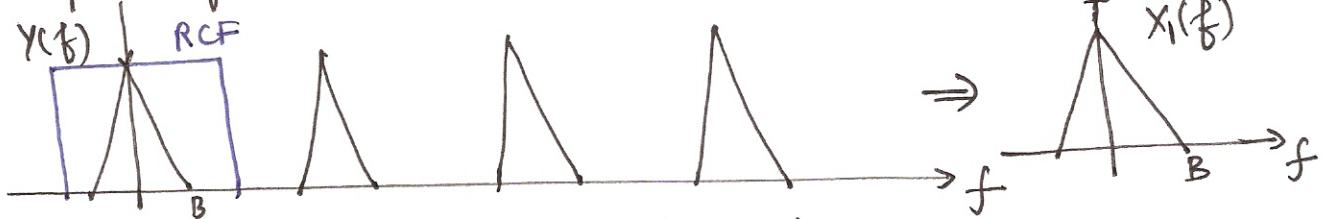
⇒ Not an issue in the ADC!

BUT, the sinc distortion is an issue in a scenario where the sampler is following a DAC. (post-processing a DAC's output).

Reconstruction :

Sampled signal

$$Y(f) \cdot \text{rect}\left(\frac{f}{B}\right)$$

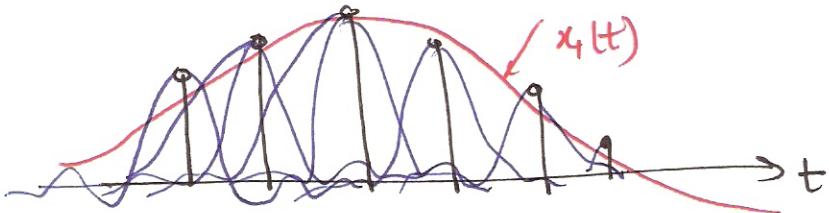


in time domain its a sinc interpolation

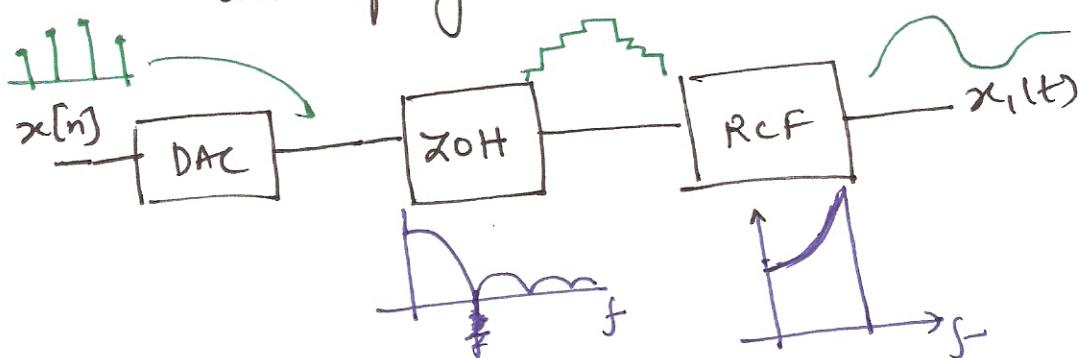
$$Y(f) \cdot \text{rect}\left(\frac{f}{B}\right) \xleftrightarrow{f^{-1}} y(t) + \text{sinc}(tB)$$

Using,
 $\text{Bisinc}(tB) \xleftrightarrow{f} \text{rect}\left(\frac{f}{B}\right)$

Duality property

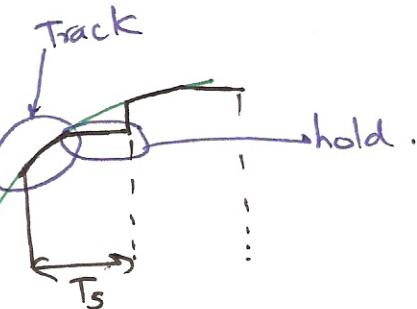
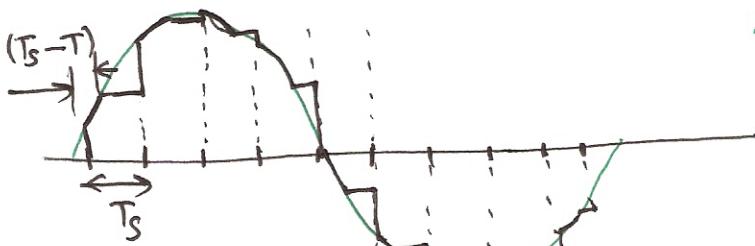


Again, the requirements on the RCF are relaxed by oversampling.



sinc^{-1} response shape is used in the RCF to compensate for the sinc distortion in the ZOH

Track and hold (T/H).



$y(t)$ follows $x(t)$ during the track (aka acquisition) phase and is held during the hold phase

At high speeds ($100 \text{ MHz} \rightarrow 10 \text{ Hz}$)
the aperture time increases w.r.t the sample period
 \Rightarrow distinction between S/H and T/H disappears at such speeds.
Ex. 10 Hz ADC all employ T/H's in the front-end.

Analysis of T/H

$$y(t) = y_{\text{FE}}^{(t)} + y_{\text{TH}}^{(t)}$$

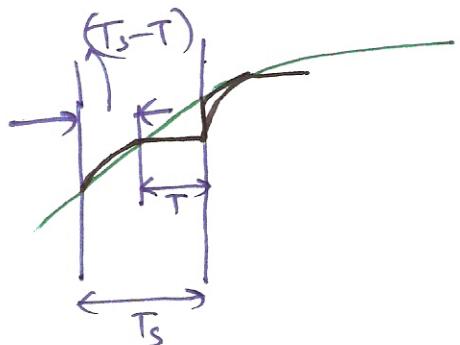
track hold

← summation of two responses signals

* $y_{\text{FE}}^{(t)}$ is same as in the RZ S/H response

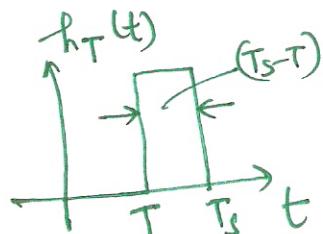
* need to find $y_{\text{TH}}^{(t)}$

* Note that $y_{\text{TH}}^{(t)} = x(t) \cdot \left[h_{\text{TH}}^{(t)} \otimes \sum_{n=-\infty}^{\infty} \delta(t-nT_s) \right]$.



hold lasts for T
track for $(T_s - T)$

$$\Rightarrow h_{\text{TH}}^{(t)} = \text{rect}\left(\frac{t - \left(\frac{T+T_s}{2}\right)}{(T_s - T)}\right)$$



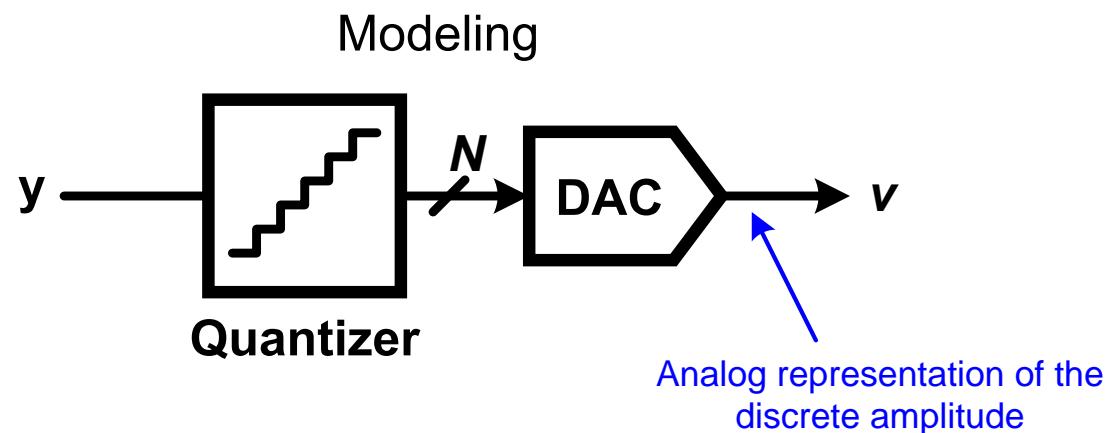
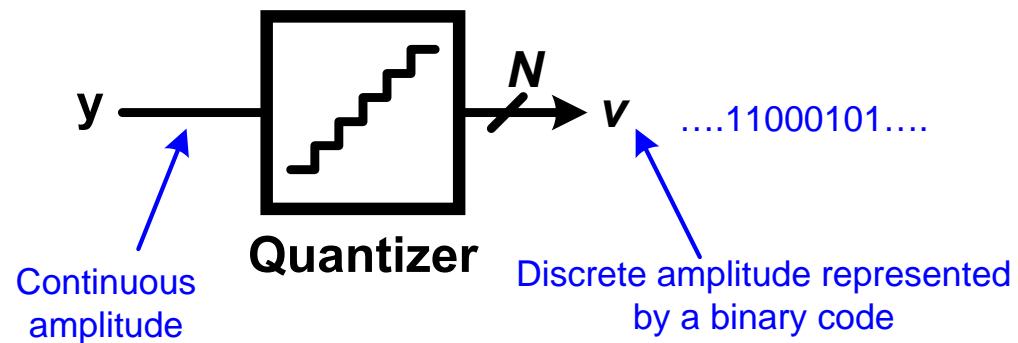
REMAINING IS A HW PROBLEM !

ECE 697 Delta-Sigma Converters Design

Lecture#2 Slides

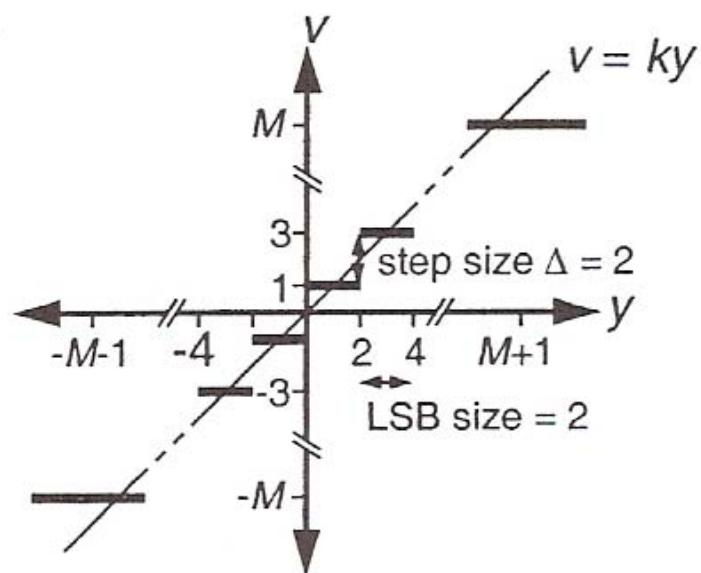
Vishal Saxena
(vishalsaxena@u.boisestate.edu)

Quantizer

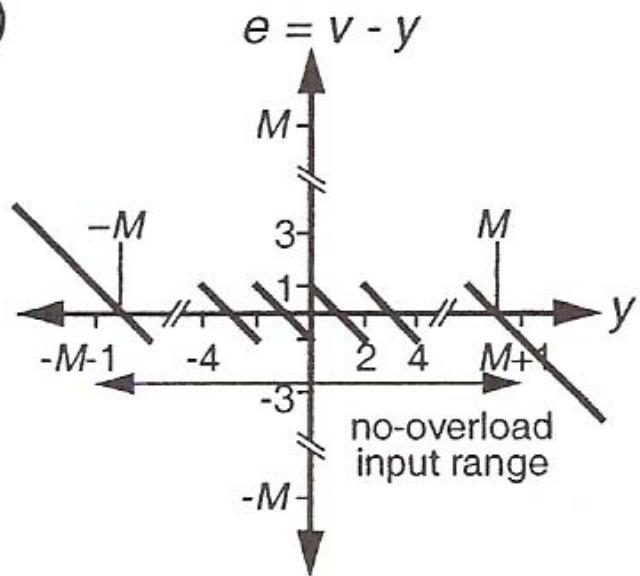


Mid-Rise Quantizer (even number of levels)

a)

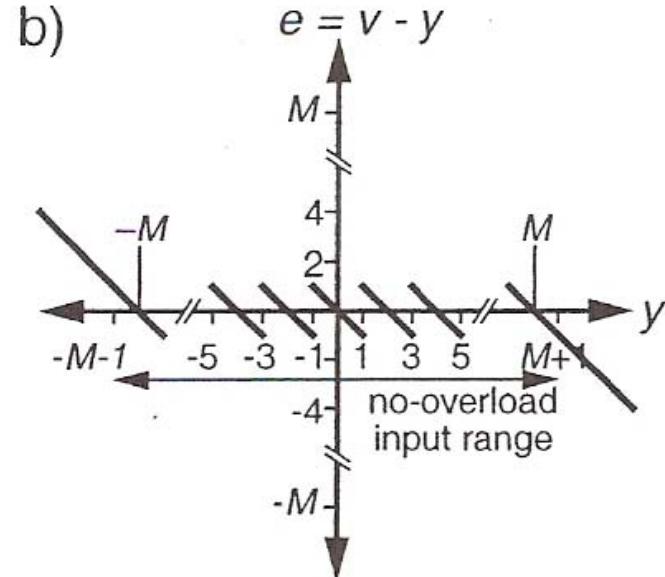
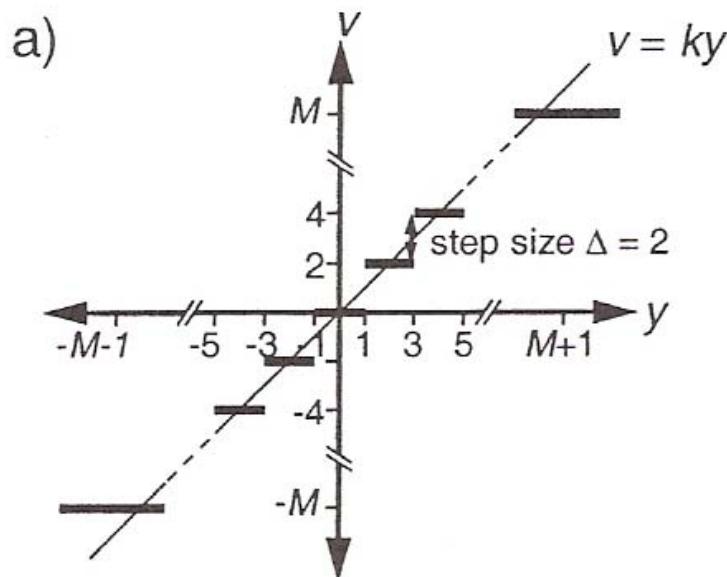


b)



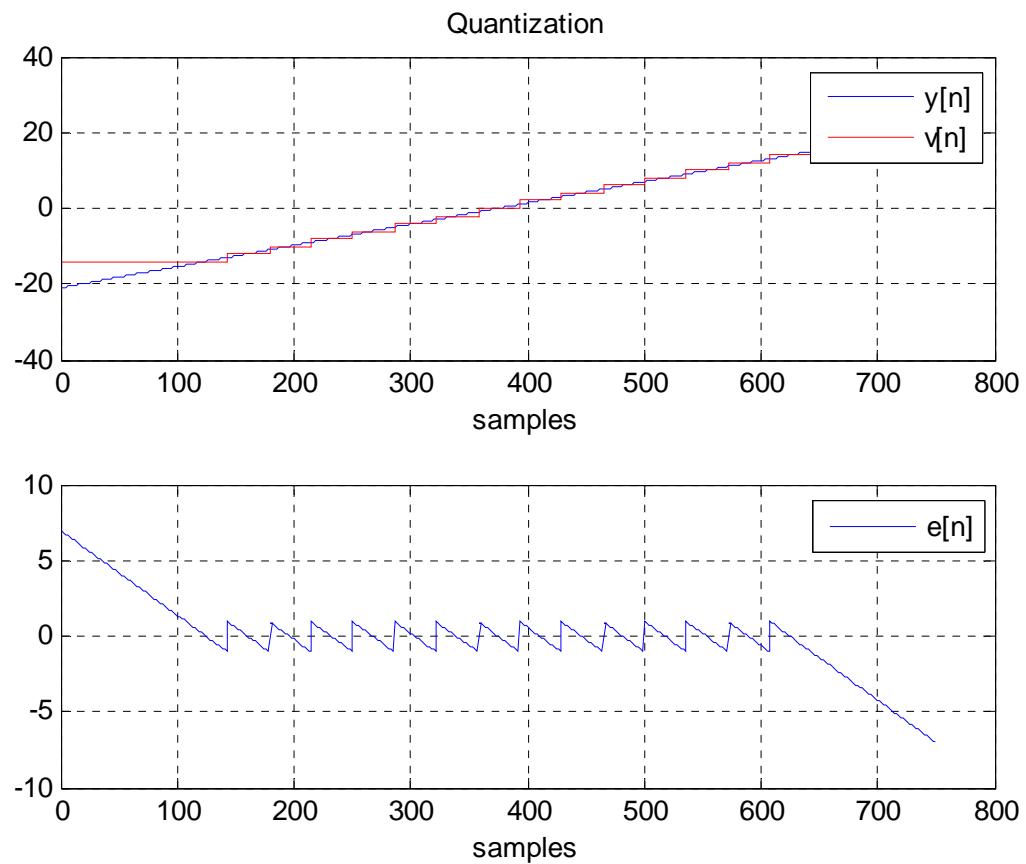
- Step rising at $y=0$ (mid-rise).
- In this figure (DSM toolbox model), $\text{ LSB} = \Delta = 2$
- $M = \text{Number of steps}$, (M is odd here)
 - Number of levels ($n\text{Lev}$) = $M+1$, (even)
- Input thresholds: $0, \pm 2, \dots, \pm(M-1)$.
- Output levels: $\pm 1, \pm 3, \dots, \pm M$.

Mid-Tread Quantizer (odd number of levels)



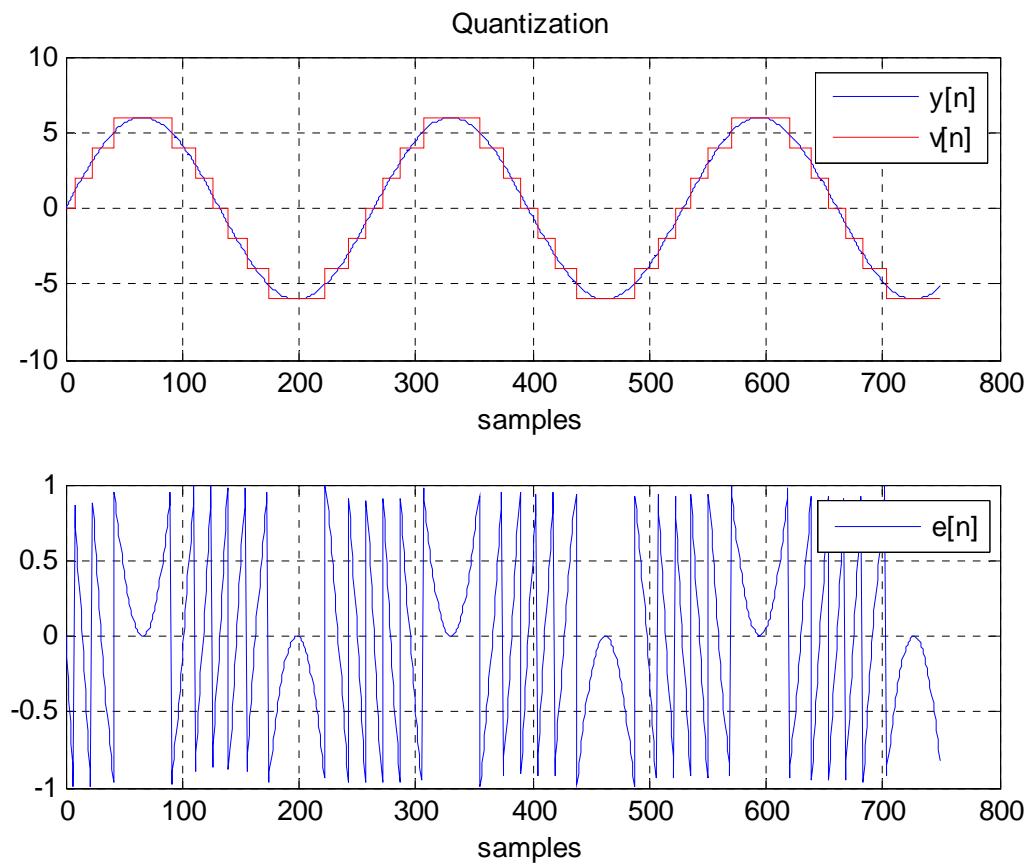
- Flat part of the step at $y=0$ (mid-tread).
- Here, $\text{LSB} = \Delta = 2$
- $M = \text{Number of steps}$, (M is even here)
 - ✓ Number of levels (n_{Lev}) = $M+1$, (odd)
- Input thresholds: $0, \pm 2, \dots, \pm(M-1)$.
- Output levels: $0, \pm 2, \pm 4, \dots, \pm M$.

Quantizer characteristics : Slow ramp input



File: Quantizer_ramp_input.m

Quantizer characteristics : Sine input



File: Quantizer_sine_input.m