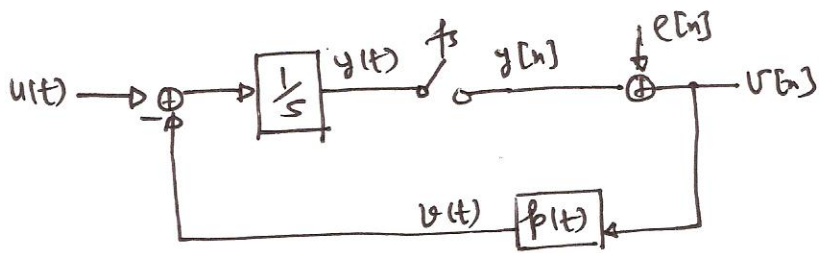
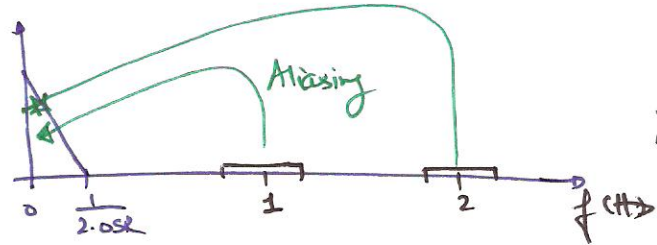


Anti-alias filtering in CT-DSMs



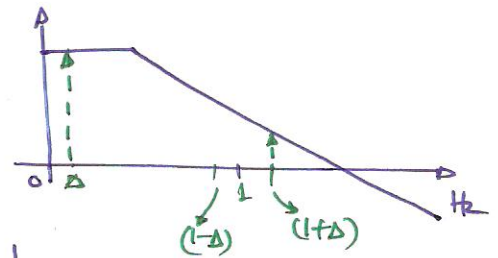
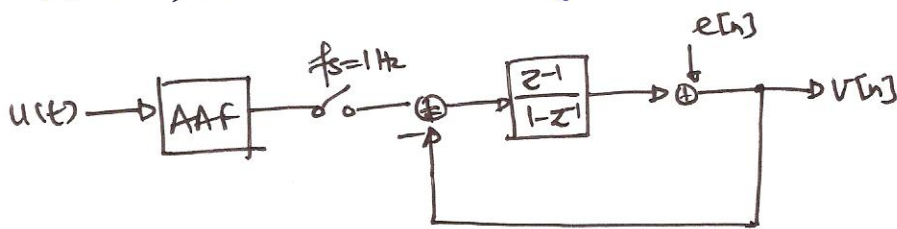
$f_s = 1 \text{ Hz}$



Inband frequency $[0, \frac{1}{2 \cdot 0.5R}]$

Alias bands: $[k - \frac{1}{2 \cdot 0.5R}, k + \frac{1}{2 \cdot 0.5R}]$
 $k = \pm 1, \pm 2$

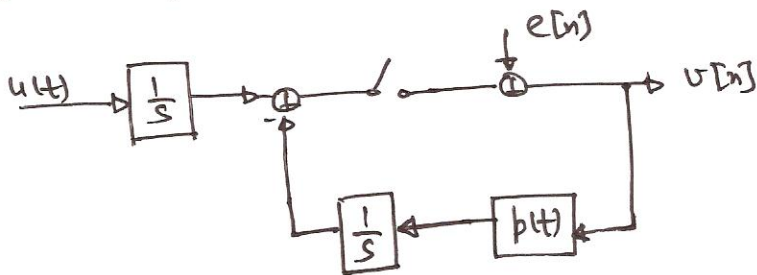
• For DT-DSM, an external AAF filter is used.



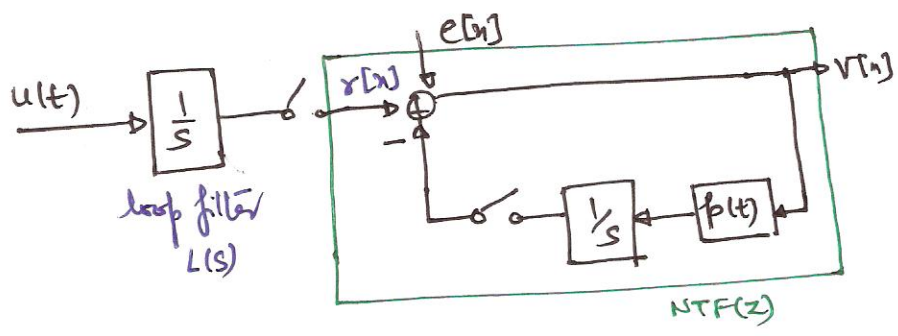
Need to understand how does the CT-DSM behave.

• intuitively, the continuous-time filter before the sampler should provide some alias suppression.

• Rearrange the signal flow graph for the CT-DSM:

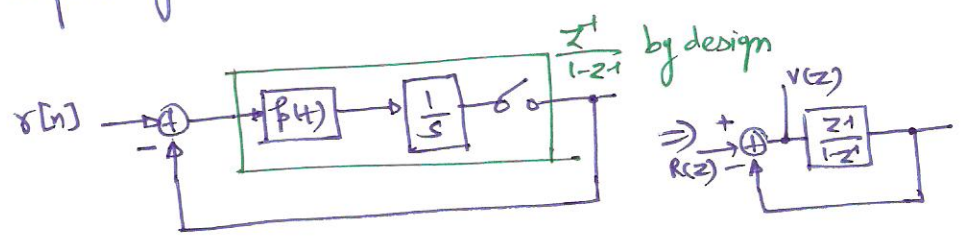


push $\frac{1}{s}$ out of the loop.



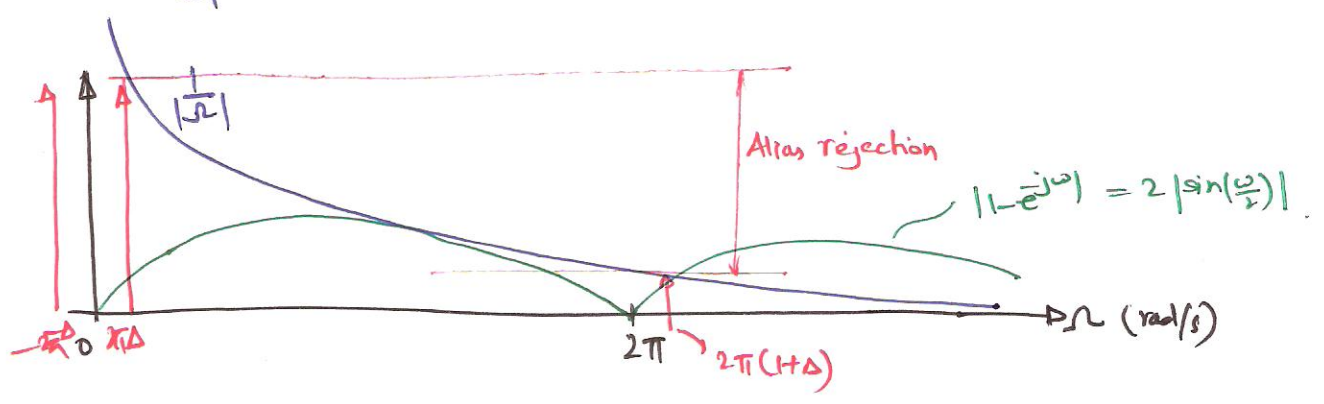
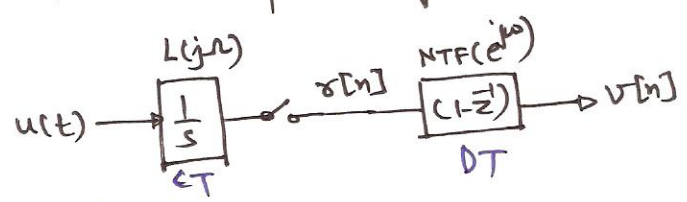
Cascade of a CT and a DT filter.

Observe that the response of the DT block is same as that of the NTF.



$$\Rightarrow R(z) \rightarrow \left[\frac{z}{1-z} \right] \rightarrow V(z)$$

Let $e[n]=0$, for the signal path



for sinusoidal input of frequency $2\pi\Delta$,

$$|V(e^{j\omega})| = \frac{1}{2\pi\Delta} \cdot |1 - e^{-j4\pi\Delta}| = \frac{1}{2\pi\Delta} \cdot 2\pi\Delta = 1.$$

\Rightarrow STF = 1 for a low-frequency sinusoidal input.

\Rightarrow Loop gain \times NTF gain $\cong 1$ at low frequencies.

• a tone at the first alias band.

$$f_{in} = 2\pi(1+\Delta) \quad \frac{1}{2}$$

$$\Rightarrow |K e^{j\omega}| = \frac{1}{2\pi(1+\Delta)} \cdot |1 - e^{j2\pi\Delta}| = \frac{2\pi\Delta}{2\pi(1+\Delta)} = \frac{\Delta}{1+\Delta} \approx \Delta$$

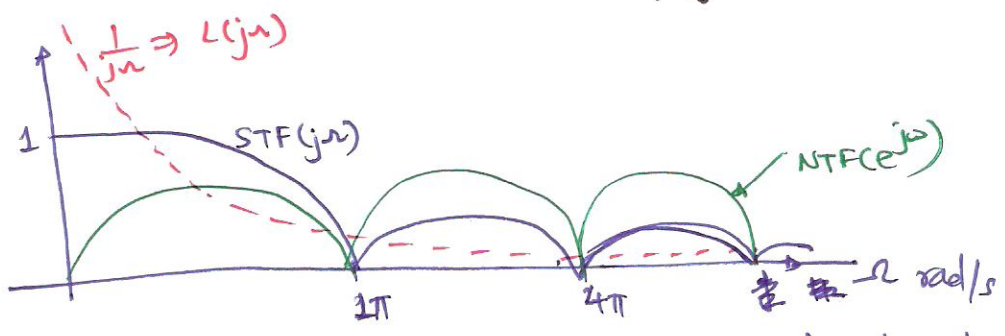
⇒ STF is very small for the first alias-band.

$$\Rightarrow \text{Alias rejection} \Rightarrow \frac{\Delta}{1+\Delta}, \frac{\Delta}{2+\Delta}, \dots, \frac{\Delta}{K+\Delta}$$

⇒ STF at the frequencies around alias band is much smaller than in the signal-band

↳ implicit anti-aliasing occurs in the CT-DSM

↳ AAF is much better for higher order loop-filters.



⇒ STF has notches at the alias-bands due to the NTF response in cascade with the loop-filter response

⇒ Double suppression of the interferers in the alias-bands

↳ very lucrative feature of the CT-DSMs.

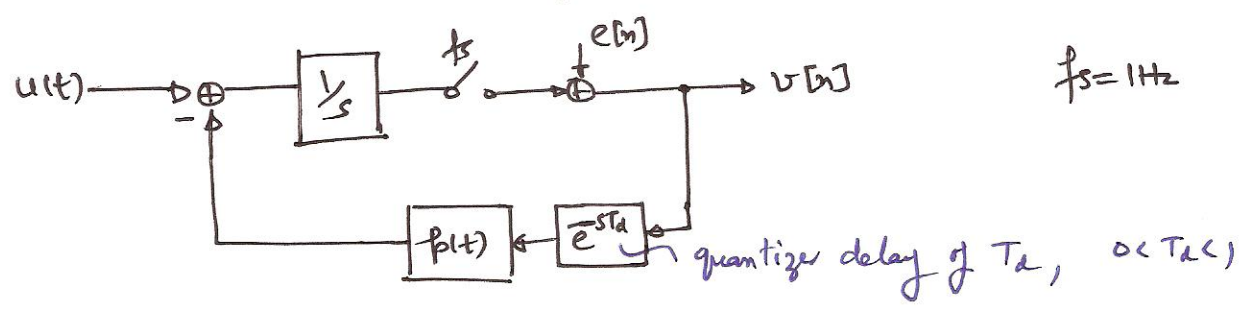
In general, the alias rejection is given by

$$\frac{|L[2\pi(1+\Delta)]|}{|L(2\pi\Delta)|}$$

• for generic, higher order topologies, we will revisit this topic later.

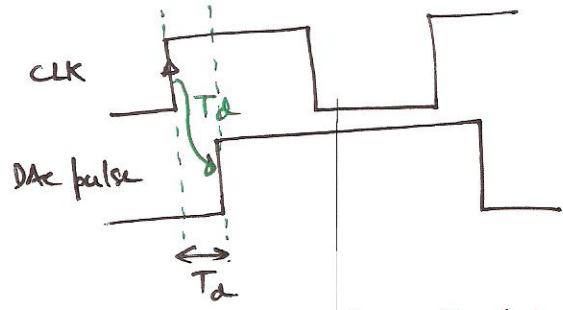
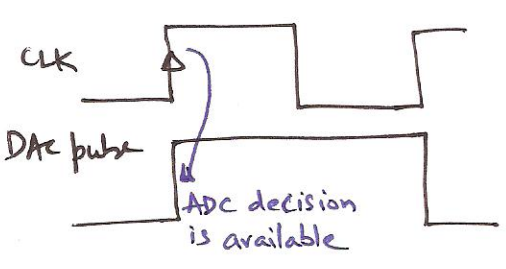
Excess loop-delay in CT-DSMs

Non-idealities \rightarrow Quantizer delay



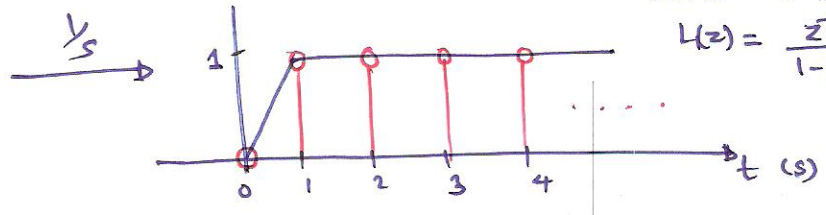
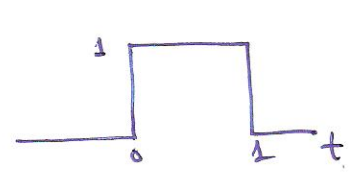
Ideal (No delay) case

Real case (with quantizer delay)



\Rightarrow More delay in the loop \Rightarrow NTF will be affected as $L(z)$ changes.

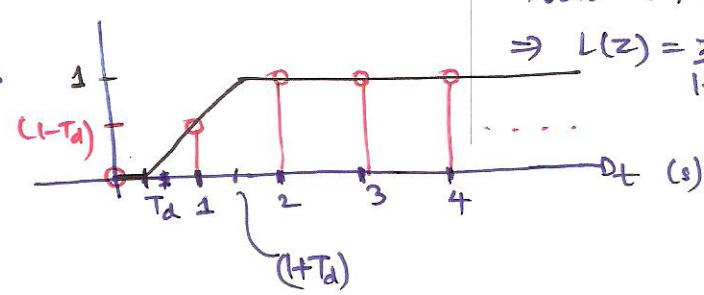
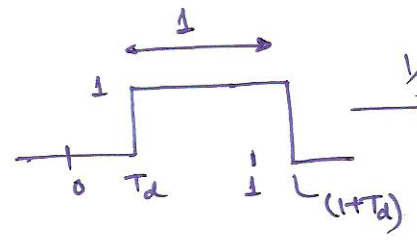
Ideal case:



$$l[n] = \{0, 1, 1, \dots\}$$

$$L(z) = \frac{z^{-1}}{1-z^{-1}}$$

with delay:



$$l[n] = \{0, (1-Ta), 1, 1, \dots\}$$

$$\Rightarrow L(z) = \frac{z^{-1}}{1-z^{-1}} - Ta z^{-1}$$

\Rightarrow first sample after the unit-delay (T_s) is smaller than expected. ($l[n]$ must always be equal to 0).

with ELD:

(2)

$$\begin{aligned} \text{NTF}(z) &= \frac{1}{1+L(z)} = \frac{1}{1 + \frac{z^{-1}}{1-z^{-1}} - T_d z^{-1}} \\ &= \frac{(1-z^{-1})}{1 - T_d z^{-1} (1-z^{-1})} = \frac{(1-z^{-1})}{1 - T_d z^{-1} + T_d z^{-2}} \end{aligned}$$

for low frequency, $z \approx 1$, $\Rightarrow \text{NTF}(z)|_{z=1} \approx (1-z^{-1})$
 \Rightarrow for DC input the NTF is unchanged.

• poles of the NTF are at $\frac{T_d \pm \sqrt{T_d^2 - 4T_d}}{2}$

\Rightarrow As T_d increases, the poles start moving out of the unit circle.

\hookrightarrow modulator becomes unstable.

\hookrightarrow too much delay \Rightarrow phase of the loop-response is too high

\hookrightarrow loop-becomes unstable.

\Rightarrow As the order of the filter becomes higher, the excess loop delay (ELD) problem gets worse.

\hookrightarrow amount of T_d tolerable, as the loop-order increases, decreases.

\Rightarrow only one NTF zero.

\hookrightarrow noise-shaping is not enhanced

\hookrightarrow but the ~~the~~ order of the modulator is increased.