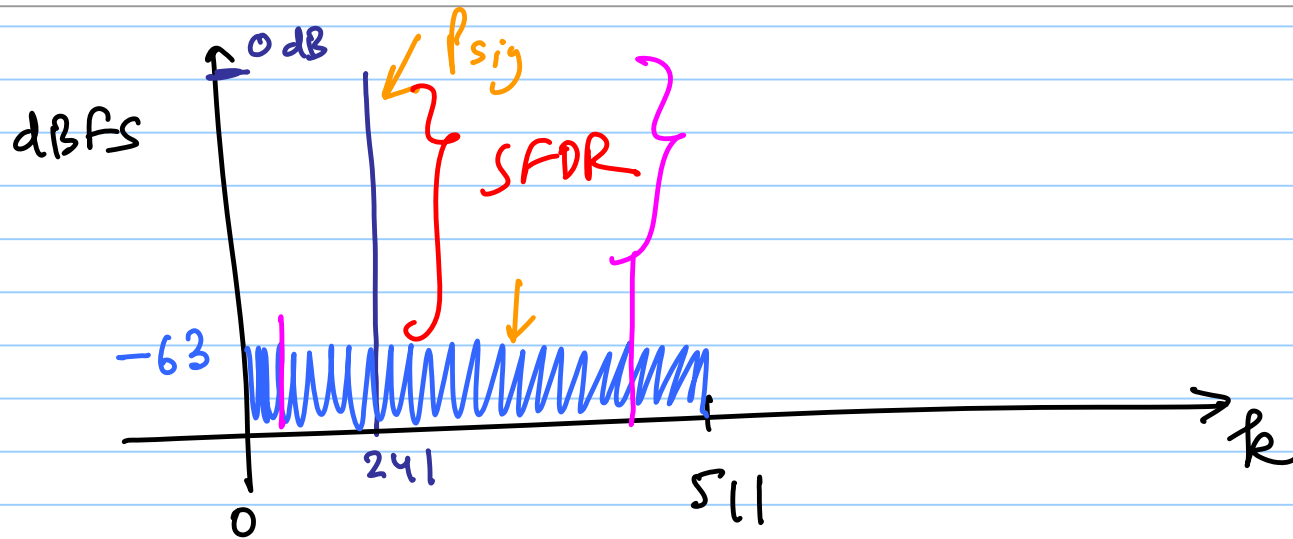


ECE 615 - Lecture 23



$$\rightarrow x_{dB} = 10 \log_{10}(x)$$

$$x = 10^{\left(\frac{x_{dB}}{10}\right)}$$

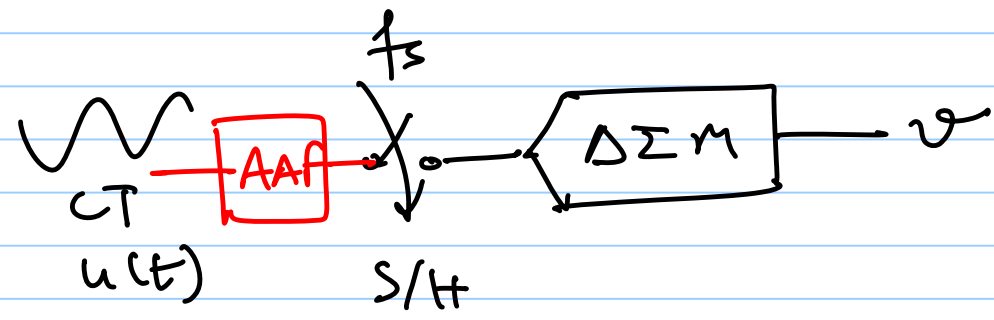
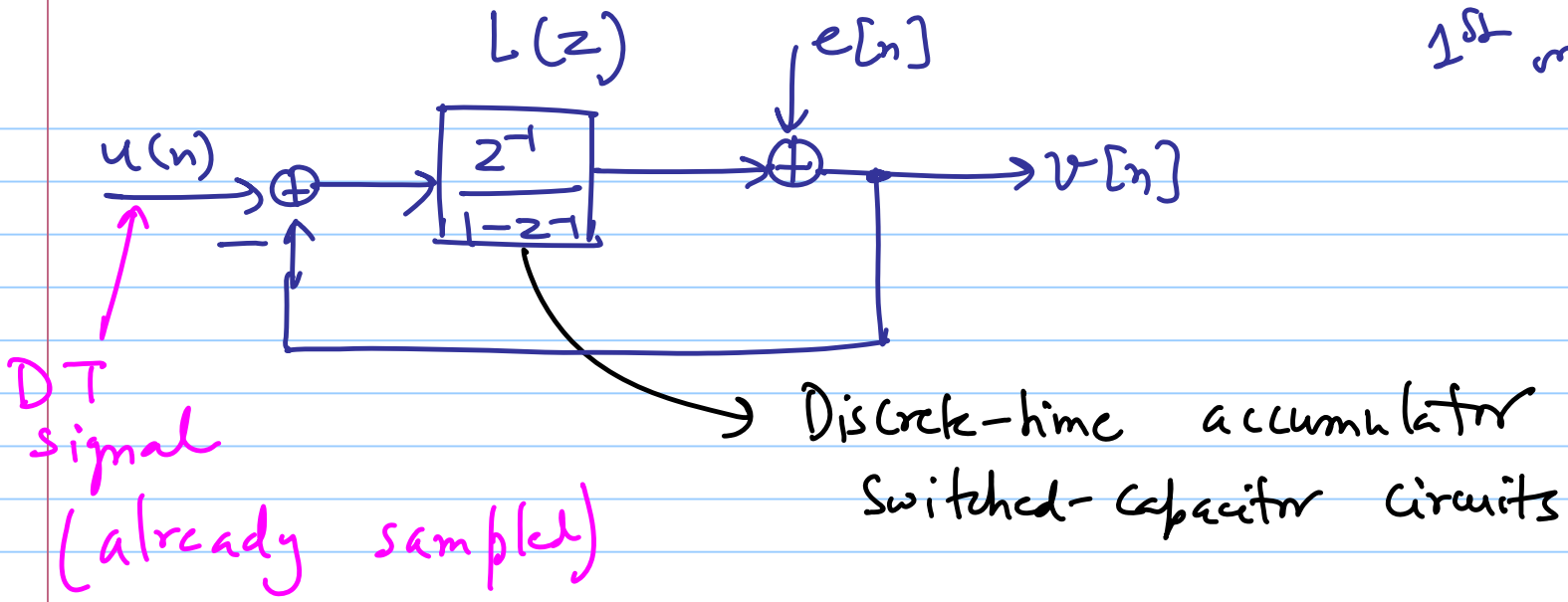
$$P_{sig} = 1$$

$$P_{noise} = 511 \times 10^{(-63/10)}$$

$$SNR = \frac{P_{sig}}{P_{noise}} \Rightarrow 36 \text{ dB}$$

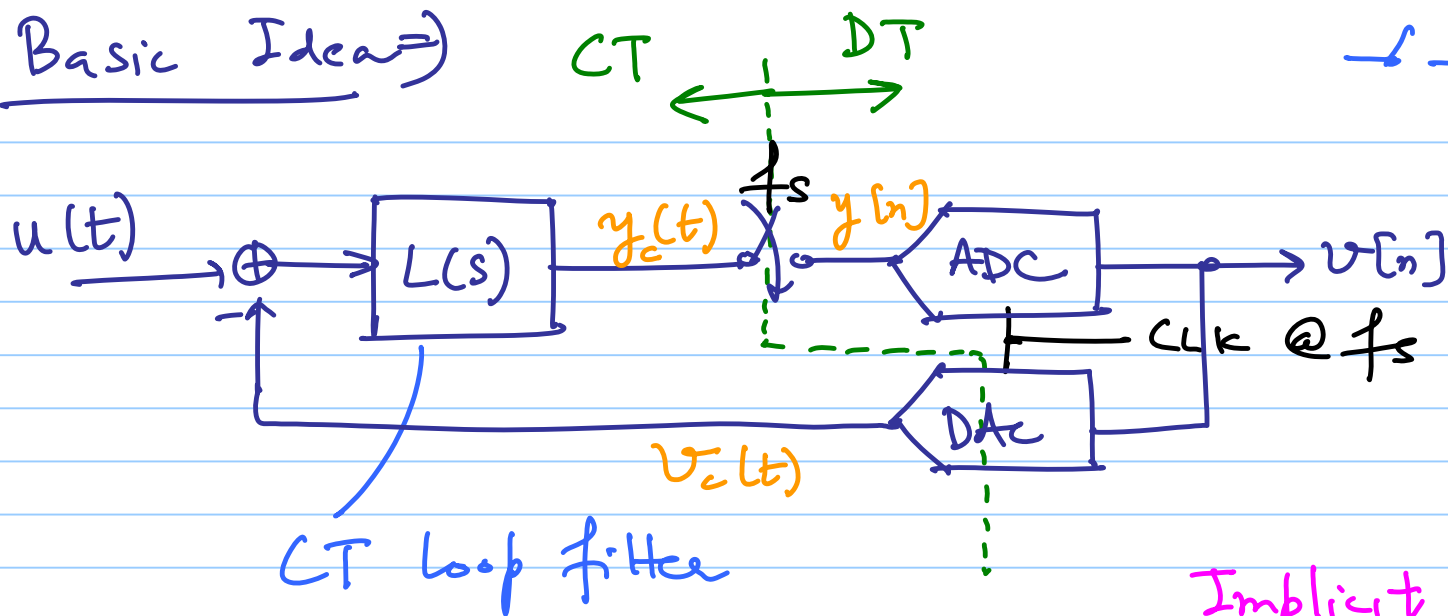
$$\Rightarrow 5.7 \text{ bits}$$

1st order $\Delta\Sigma$ modulator



Need additional AAF
↳ oversampling relaxes the requirements on the AAF

Basic Idea ⇒



Implicit AAF!

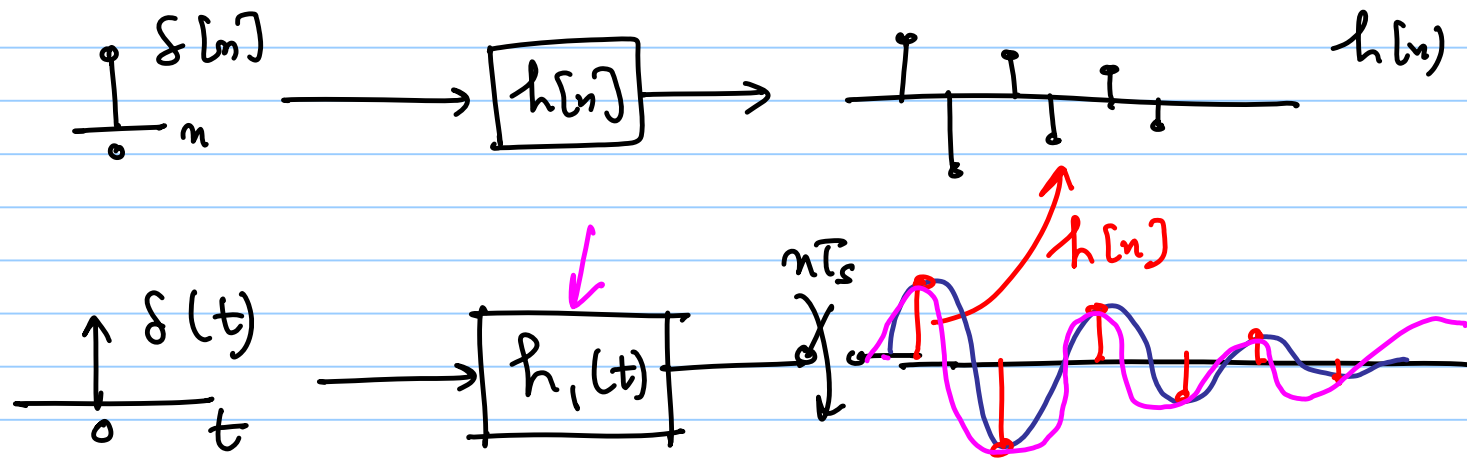
Continuous-time $\Delta\Sigma$ Modulator

↳ loop filter is a CT filter

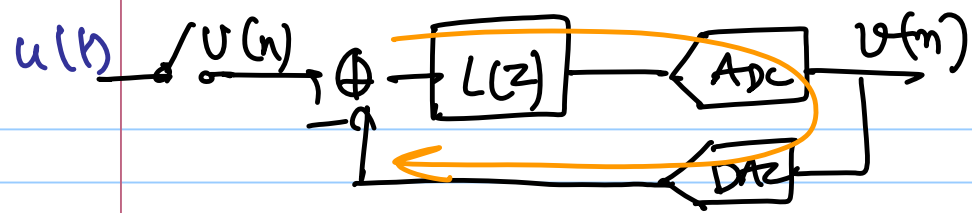
NTF(z) or ~~NTF(s)~~

✓ Overall, the system is still a DT system!

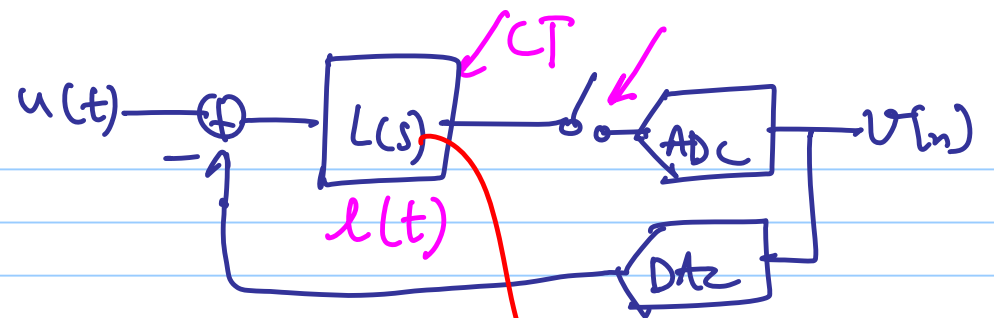
Consider the DT impulse response, $h[n]$



* Can use a CT impulse response $h_1(t)$ such that the sampled response is $h[n]$
↳ many CT responses $h_1(t)$ are possible
↳ impulse invariant transformation



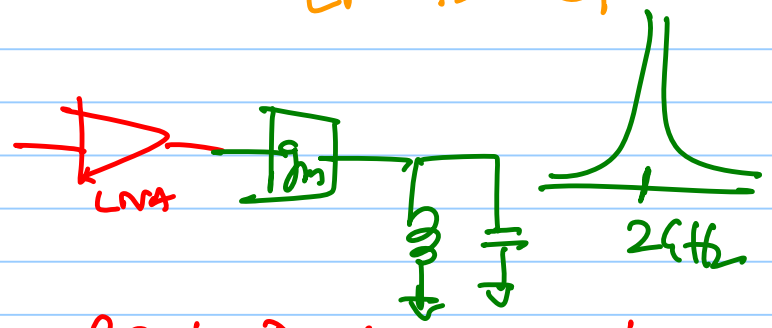
$$NTF(z) = \frac{1}{1+L(z)}$$



NTF(z) ??
 DT system
 LF is CT

CT-ΣΔM

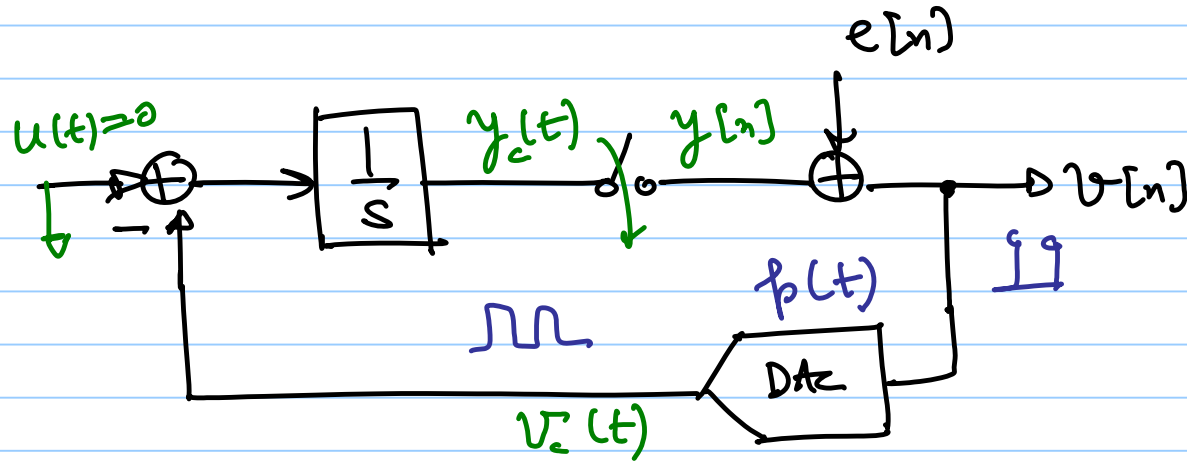
- ↳ lower power dissipation
- ↳ research activity
- ↳ > GHz clock rates



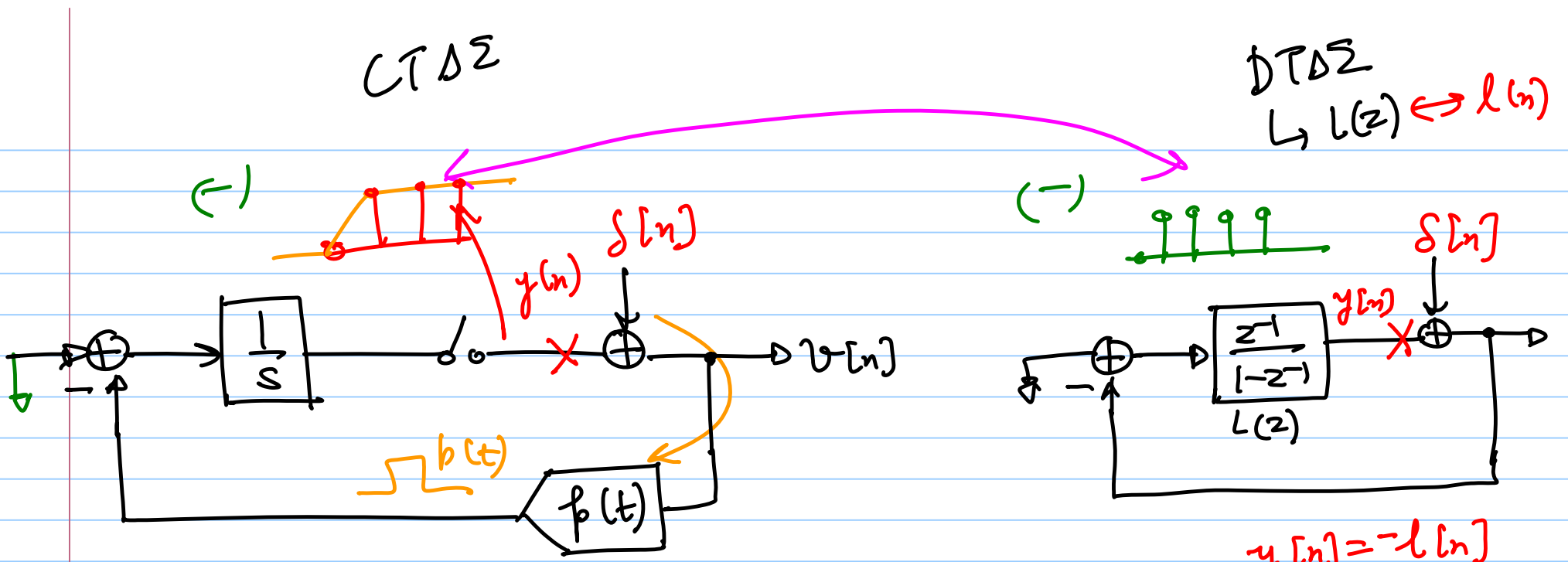
RF to Digital Converter

1st-order CT $\Delta\Sigma M$:

Sampling rate Normalized to 1Hz
 $f_s = 1 \text{ Hz}$



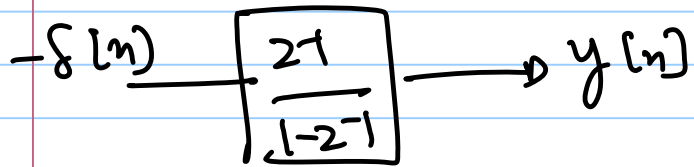
DAC is converting a DT signal to a CT signal
 ↳ need to account for the DAC pulse shape, $p(t)$
 ↳ The NTF should be same as the DT NTF, $NTF(z)$



$y[n] \triangleq$ $y[n] = -l[n]$

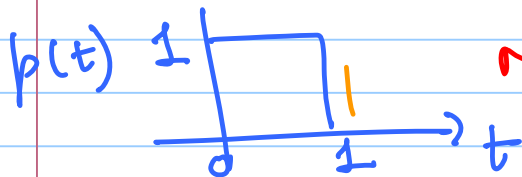
if $l[n]$ or $L(z)$ is same for the CT & DT loops,
 their NTF = $\frac{1}{1+L(z)}$ is also the same

DT impulse response

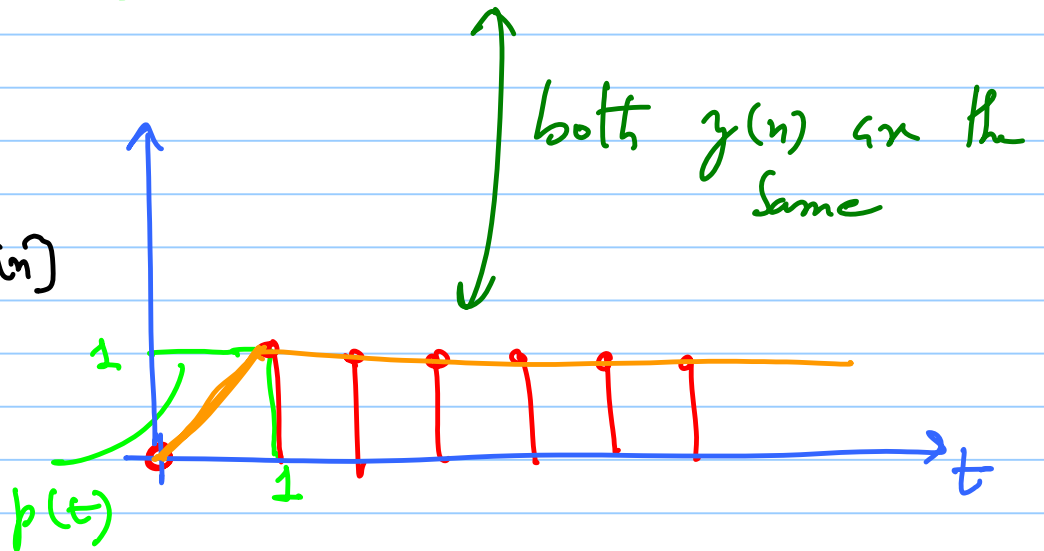
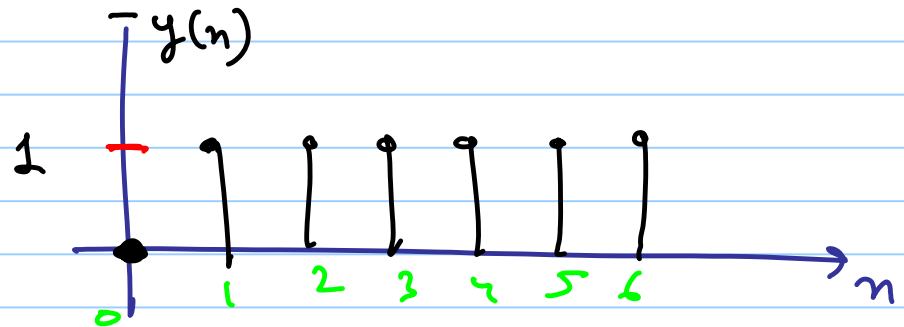


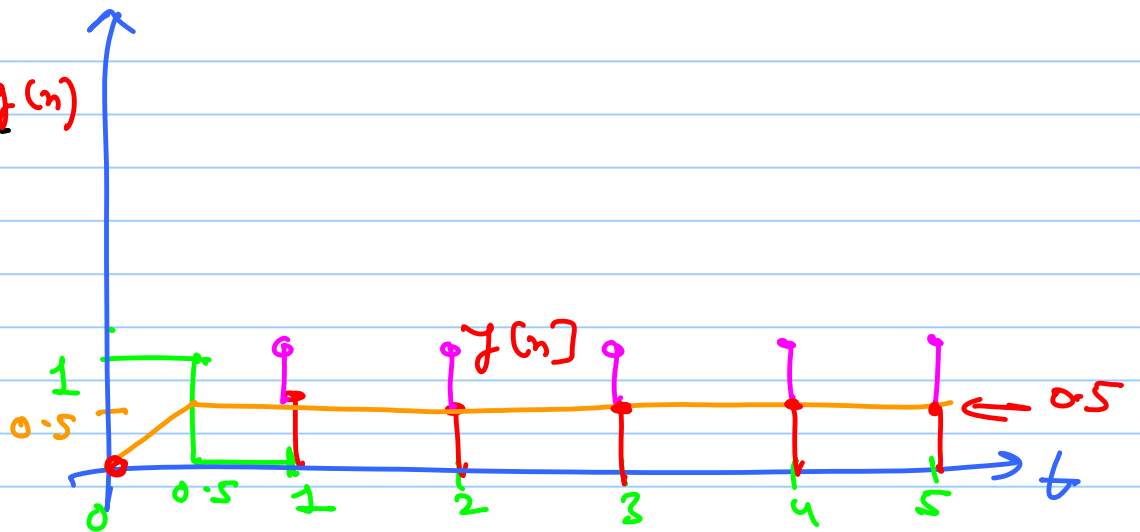
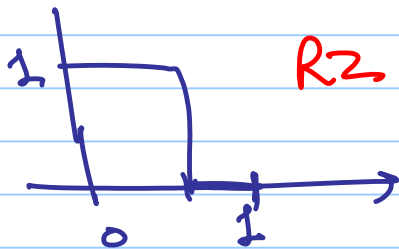
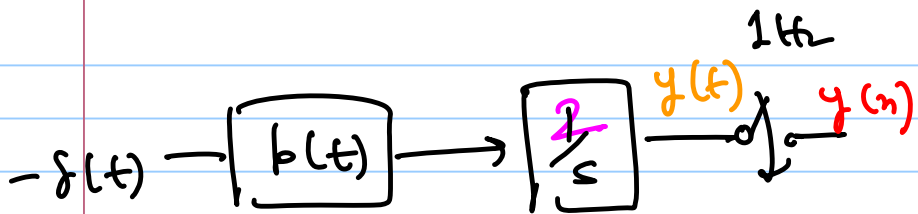
$1, 0, 0, 0, \dots$

$$L(s) = \frac{1}{s}$$



NRZ



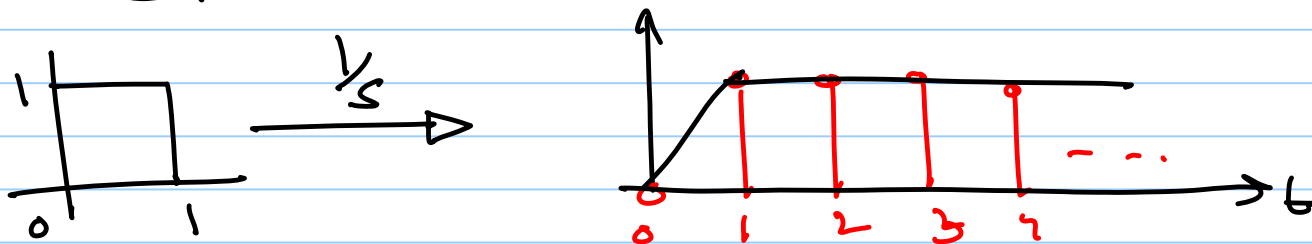


$$L(s) = \frac{2}{s}$$

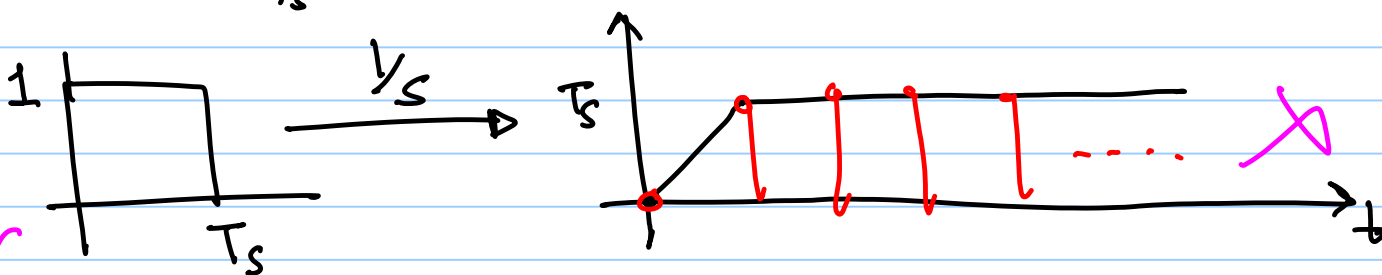
$$\{p(t), L(s)\} \Rightarrow l[n] \xleftrightarrow{Z} L(z) \rightarrow \text{NTF}(z) = \frac{1}{1+L(z)}$$

changing the sampling rate:

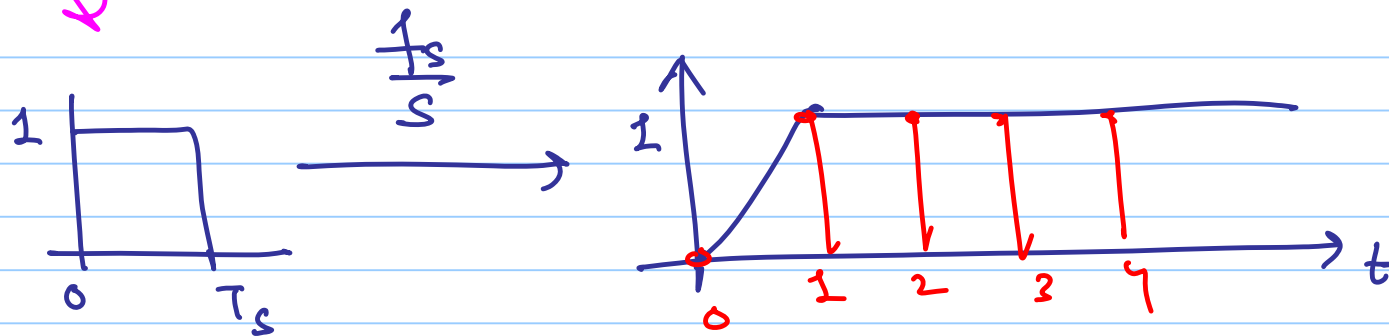
@ 1 Hz



@ $f_s = \frac{1}{T_s}$



flux



$$L(s) = \frac{1 \cdot s}{s} = \frac{1}{s T_s}$$

Not!
 ~~$\frac{1 \cdot s}{s}$~~