

ECE 615 - Lecture 15

Note Title

10/24/2013

L-0 Cascade

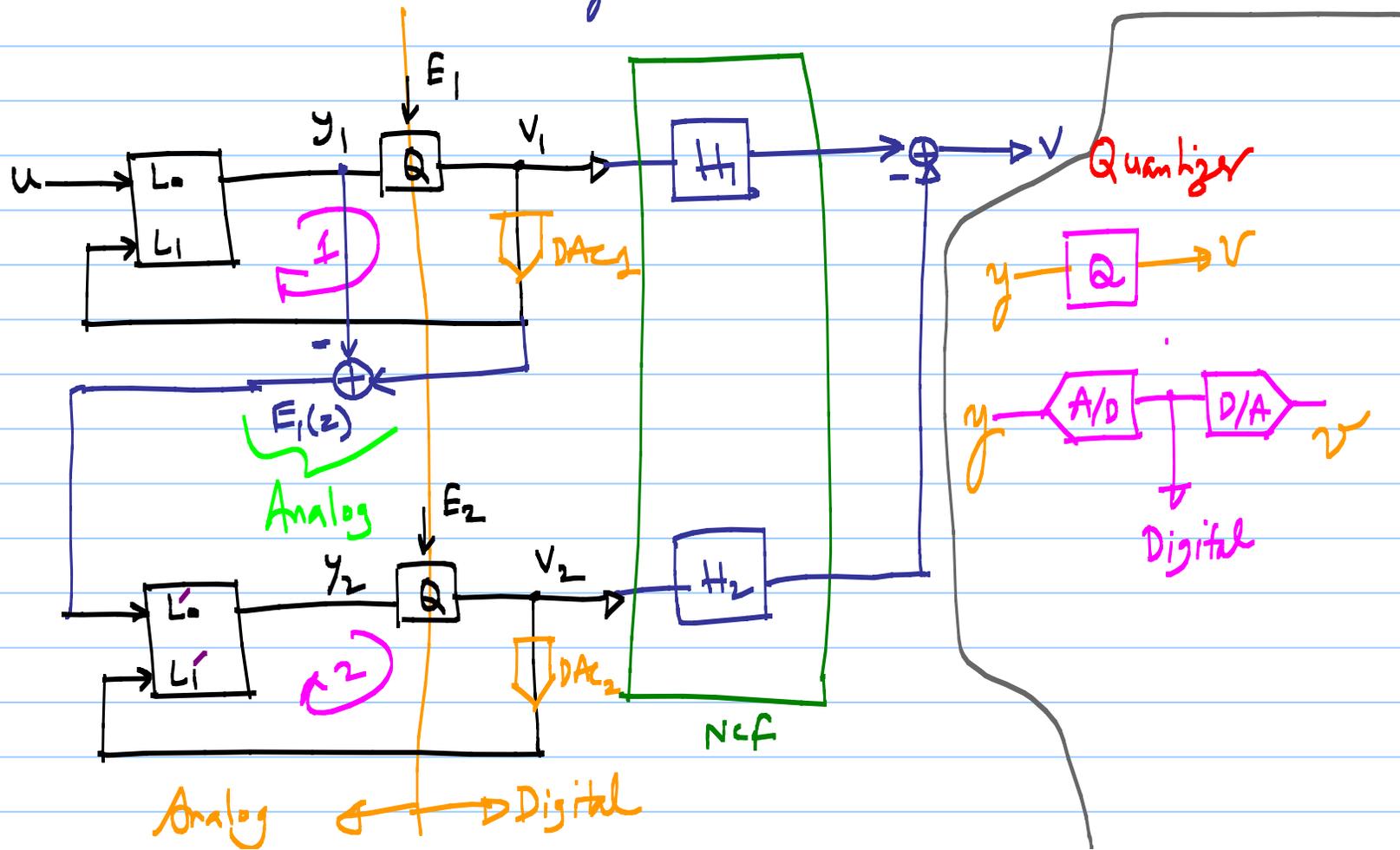
$$V(z) = \text{STF}_1 \cdot U + \underbrace{\text{NTF}_1}_{\text{digital filter}} \cdot E_2$$

$\sigma^2 = \frac{V_{LSB}^2}{12}$



Multi Stage Noise Shaping (MAST)

* All the stages are a $\Delta\Sigma$ modulator



1st stage: $V_1(z) = \text{STF}_1 \cdot U + \text{NTF}_1 \cdot E_1$

$$V_2(z) = \text{STF}_2 \cdot E_1 + \text{NTF}_2 \cdot E_2$$

final output:

$$V(z) = \overset{\text{Dis}}{H_1} \cdot V_1 - \overset{\text{Dis}}{H_2} \cdot V_2$$

Cancel out

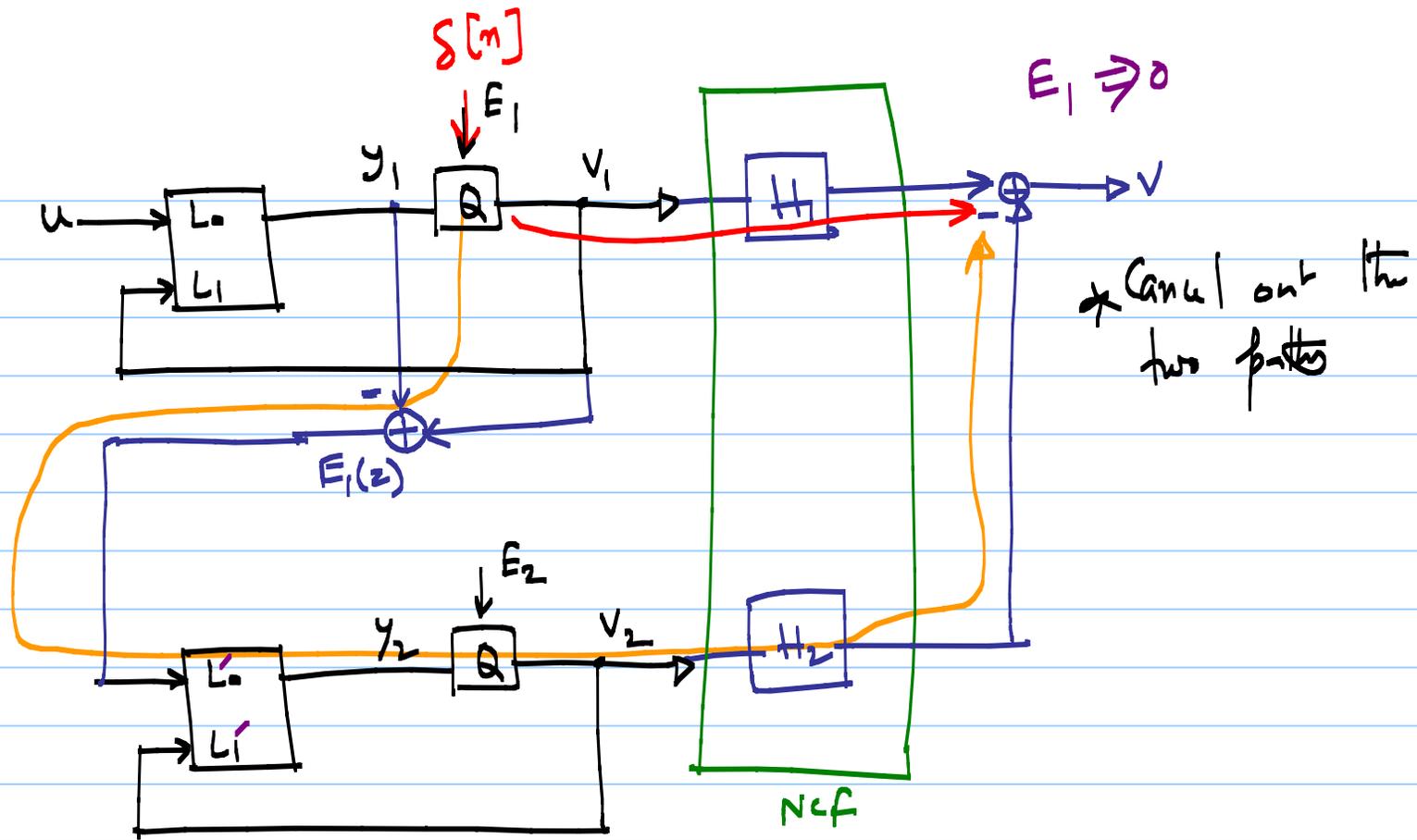
$E_1 \leftarrow$ coarse Q-noise

$E_2 \leftarrow$ fine Q-noise

$$= H_1 (\text{STF}_1 \cdot U + \text{NTF}_1 \cdot E_1) - H_2 (\text{STF}_2 \cdot E_1 + \text{NTF}_2 \cdot E_2)$$

$$= (H_1 \cdot \text{STF}_1 \cdot U - H_2 \cdot \text{NTF}_2 \cdot E_2) + \underbrace{H_1 \cdot \text{NTF}_1 \cdot E_1 - H_2 \cdot \text{STF}_2 \cdot E_1}_{=0}$$

$$H_1 \cdot \text{NTF}_1 = H_2 \cdot \text{STF}_2$$



The simplest choice for H_1 & H_2

$$H_1 \cdot NTF_1 = H_2 \cdot STF_2$$

easy to realize \rightarrow

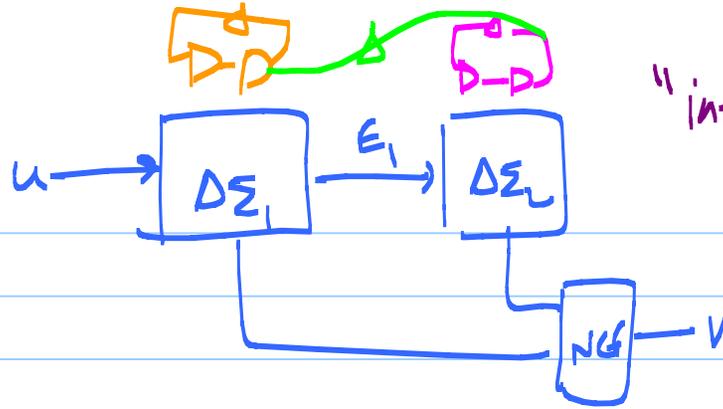
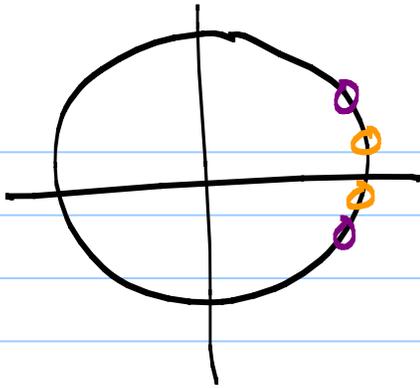
$$\left. \begin{array}{l} H_1 = STF_{2,d} \\ H_2 = NTF_{1,d} \end{array} \right\} \text{digital filters}$$

$$STF_2(z) = z^{-k} \text{ or } \underline{\underline{1}}$$

overall output:

$$V = H_1 \cdot V_1 - H_2 \cdot V_2 = \underbrace{STF_1 \cdot STF_2}_{\text{orange}} \cdot U - \boxed{NTF_1 \cdot NTF_2}_{\text{purple}} \cdot E_2$$

$$NTF = NTF_1 \cdot NTF_2$$



$$NTF = \prod_i NTF_i$$

$$STF = \prod_i STF_i$$

Ex:

2-2 MASH (SOSO)

2-1

2-2

2-2-1

2-1-1

$$STF_1 = STF_2 = z^{-2}$$

$$NTF_1 = NTF_2 = (1-z^{-1})^2$$

$$V(z) = z^{-4} U(z) - (1-z^{-1})^4 E_L(z)$$

~~1X~~ or ~~1X~~

tonal Q-noise

"lots of space in the spectrum"

* 4th-order noise shaping

Stability is governed by 2nd-order

* loop

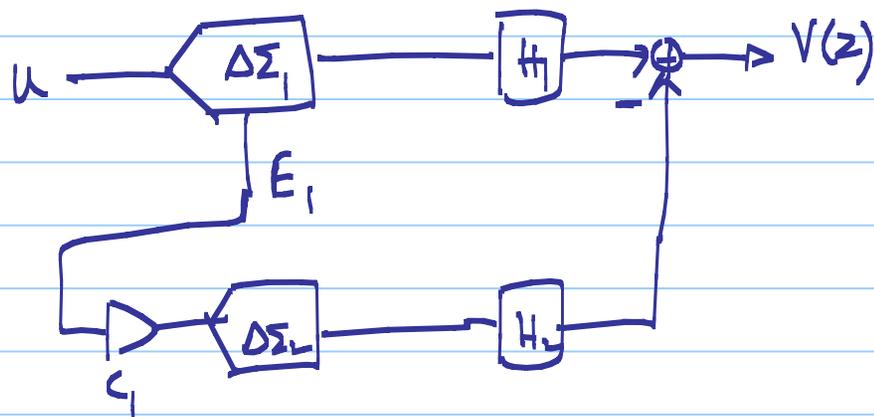
* E_1 input to the second modulator needs to be scaled to fit it within the stable range (MSA)

Ex. for 2nd-order single-bit first-stage $\Delta\Sigma$ output
 $\Rightarrow c_{12} = 1/4$

↳ if multibit quantization is used in the first stage,
 c_{12} can be greater than 1

if $V_{CSB_1} < MSA_2 \Rightarrow c_{12} > 1$
 $\Rightarrow c_{12} \Rightarrow$ changes in the NCF logic

Coupling of steps :



$$H_1 = STF_{2,d}$$

$$H_2 = \frac{1}{c_1} \cdot NTF_{1,d}$$

$$V(z) = STF_1 \cdot STF_{2,d} \cdot U(z) + \frac{1}{c_1} \cdot NTF_{1,d} \cdot NTF_2 \cdot E_2(z)$$

$$NTF_{cascade} = \frac{(1-z^{-1})^{N_{cascade}}}{\prod_i^M c_i}$$

$$N_{cascade} = \sum_{i=1}^M N_i$$

$M \Rightarrow \text{steps}$

$$IBN = \frac{IBN_0}{\prod c_i^2}$$

$$c_i < 1$$

$$\Rightarrow IBN > IBN_0$$

$\prod c_i^2 < 1 \Rightarrow$ MASH performance is below
ideal

* Noise leakage

$$H_1 \cdot NTF_1 \neq H_2 \cdot NTF_2$$

E_1 leaks into $V(z)$

* Use low-distortion topology in the first stage.

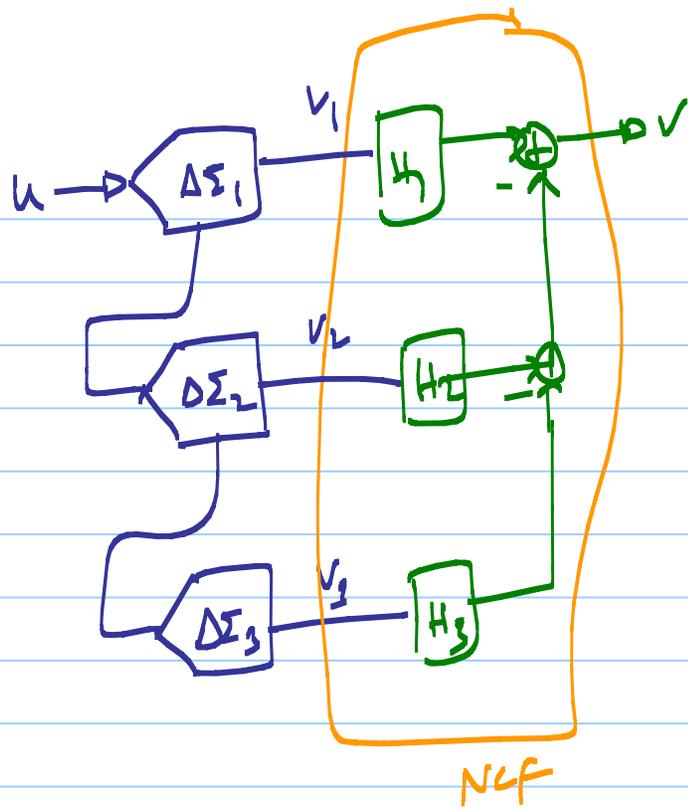
* In a MASH

$$E_2 = Q(E_1)$$

↑ more noise-like

→ less correlated with $U(z)$

↳ requires lower dithering



2-1-1

2-2-1

2-2-2 \Rightarrow 6th-order NSF

* Single-loop $\Delta\Sigma$ modulator, issues with s/c implementation:

↳ imperfect matching of capacitors \Rightarrow changes $\begin{matrix} I(z) \\ \downarrow \\ NTF(z) \end{matrix}$

↳ A_v : finite of opamps

$$I(z) = \frac{z^1}{1-z^{-1}} \Rightarrow A_v = \infty$$

$A_v \Rightarrow$ finite

↳ incomplete settling and slewing of opamps

* All these change NTF & STF of the modulator

$$|NTF| \approx \frac{1}{|L|} \ll 1;$$

for single-loop $\Delta\Sigma$
not a big issue

"Use SIMSIDES
to simulate this"

as long as

$$A_v \approx \frac{0.5R}{\tau}$$

"Look at the notes for
analysis for MASH ADC"

