

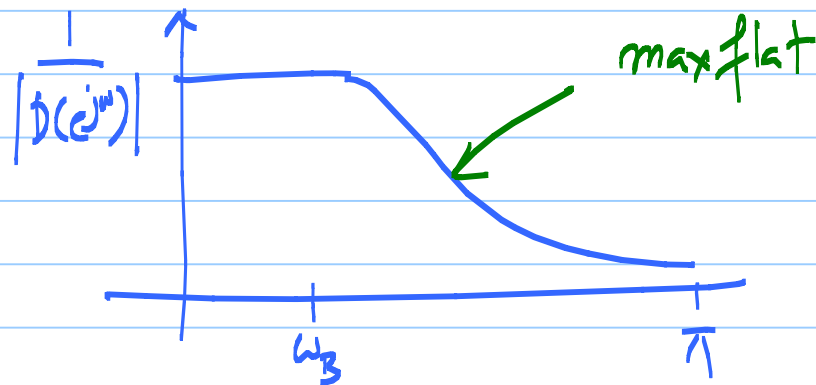
ECE 615 - Lecture 12

Note Title

10/15/2013

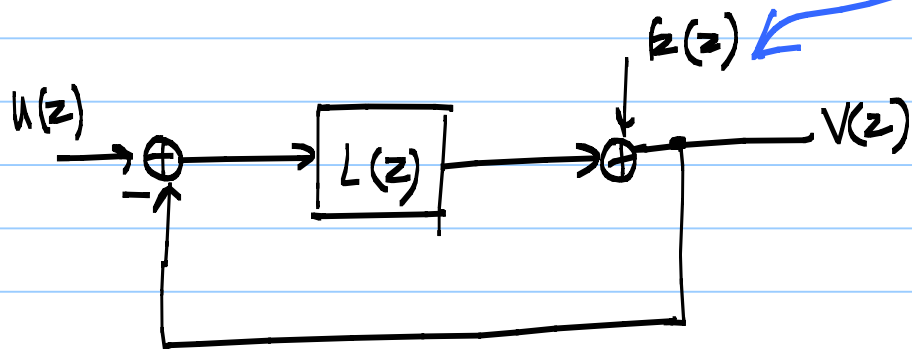
Systematic Design of NTF \rightarrow HW 4

$$NTF(z) = \frac{\prod_i (1 - \bar{z}_i z_i)}{D(z)}$$



Sensitivity of a feedback loop

disturbance injected



$$V(z) = U(z) \cdot \frac{L(z)}{1+L(z)} + E(z) \frac{1}{1+L(z)}$$

$E(z) \frac{1}{1+L(z)}$

$|L| \rightarrow \infty$ in the signal band

$$\left| \frac{1}{1+L} \right|$$

sensitivity of the loop

$$\frac{1}{1+L(e^{j\omega})}$$

\rightarrow how effectively the loop suppresses the disturbance

↳ loop is insensitive to the disturbance at low frequencies

⇒ $|L(e^{j\omega})|$ is high at low-frequencies

Sensitivity for DΣ loop → NTF

* $h(0) = \underline{NTF(\omega)} = 1 \leftarrow$ Realizability Condition

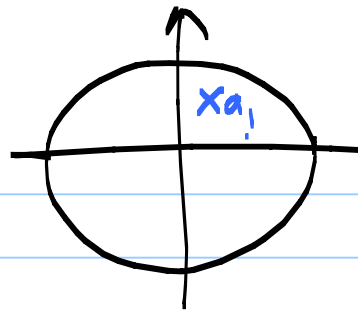
$$NTF(z) = \frac{\begin{array}{c} \downarrow \text{zero at DC} \\ (1 + a_1 z^{-1}) \end{array} \begin{array}{c} \nearrow \text{Complex zero pairs} \\ (1 + a_2 z^{-1} + a_3 \bar{z}^2) \end{array} (\dots)}{(1 + b_1 z^{-1}) (1 + b_2 z^{-1} + b_3 \bar{z}^3) (\dots)}$$

poles must be within the unit circle

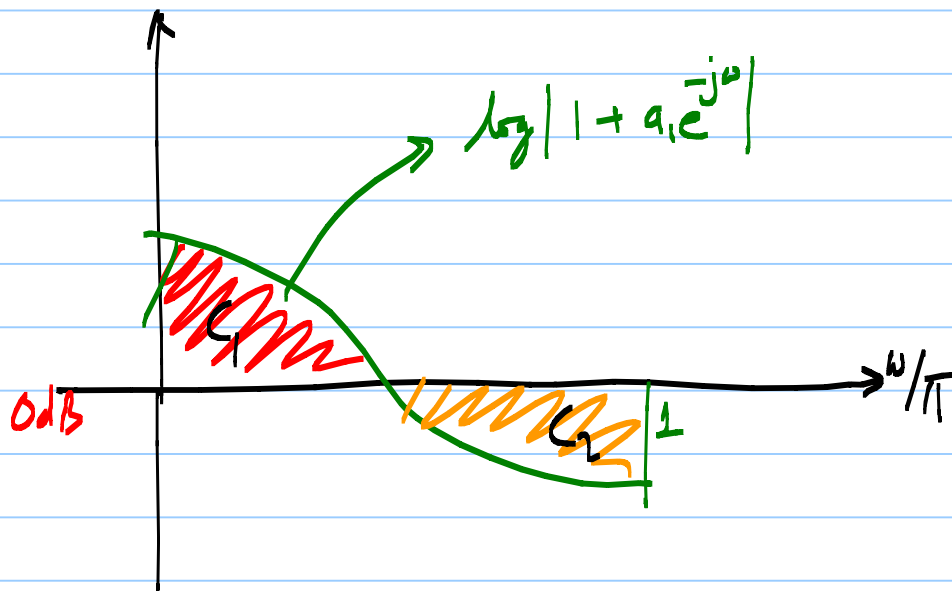
& zeros are on the unit circle.

$$\frac{1}{1+a_1 z^{-1}}$$

↑ pole at a_1



it can be shown that $\int_0^\pi \log |1+a_1 e^{-j\omega}| d\omega = 0$ if $|a_1| < 1$



$$C_1 = C_2$$

Area above 0dB line
= Area below 0dB
line

Similarly . $\int_0^{\pi} \log |1 + a_2 e^{-j\omega} + a_3 e^{-j2\omega}| d\omega = 0. \checkmark$

$$\int_0^{\pi} \log |NTF(e^{j\omega})| \cdot d\omega = \int_0^{\pi} \log \left| \frac{(1 + a_1 e^{-j\omega})(1 + a_2 e^{-j2\omega} + a_3 e^{-j3\omega})}{(1 + b_1 e^{-j\omega})(1 + b_2 e^{-j2\omega} + b_3 e^{-j3\omega})} \right| d\omega$$

$$= \int_0^{\pi} \log |1 + a_1 e^{-j\omega}| + \int_0^{\pi} -\log |1 + b_1 e^{-j\omega}| + \dots$$

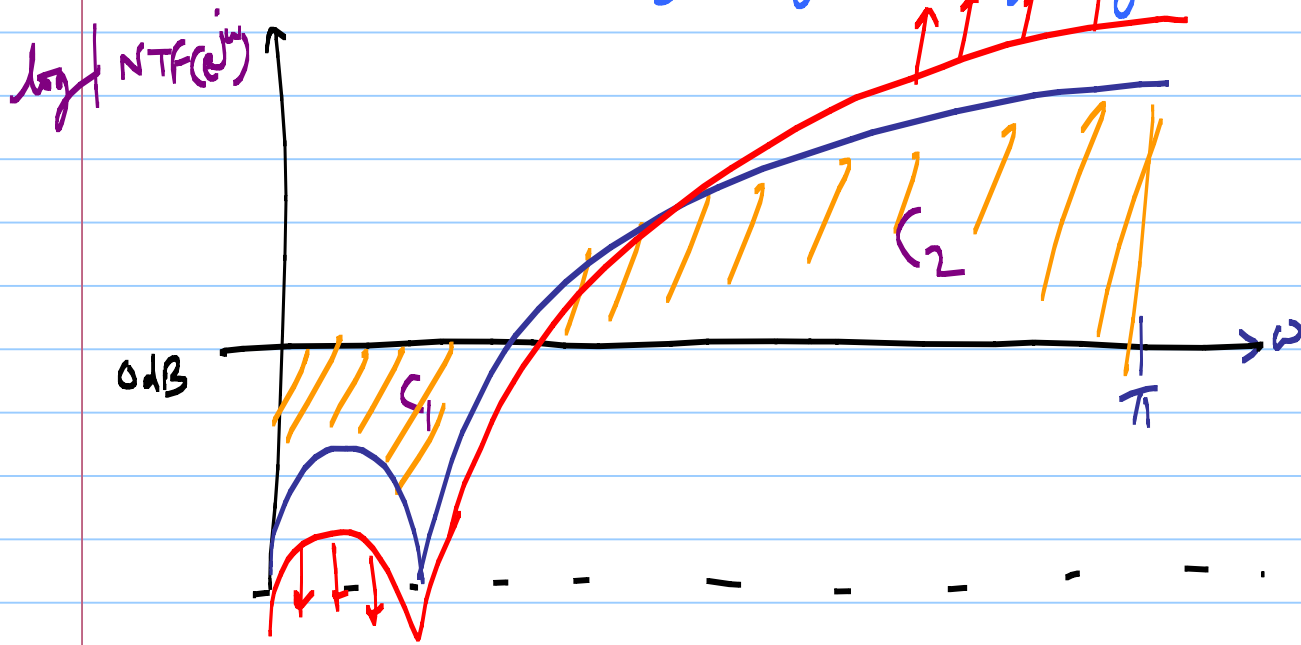
$$= 0$$

When all NTF poles are within
unit circle
zeros on the unit circle

$$\int_0^{\pi} \log |NTF(e^{j\omega})| d\omega = 0$$

Bode's Sensitivity
Theorem

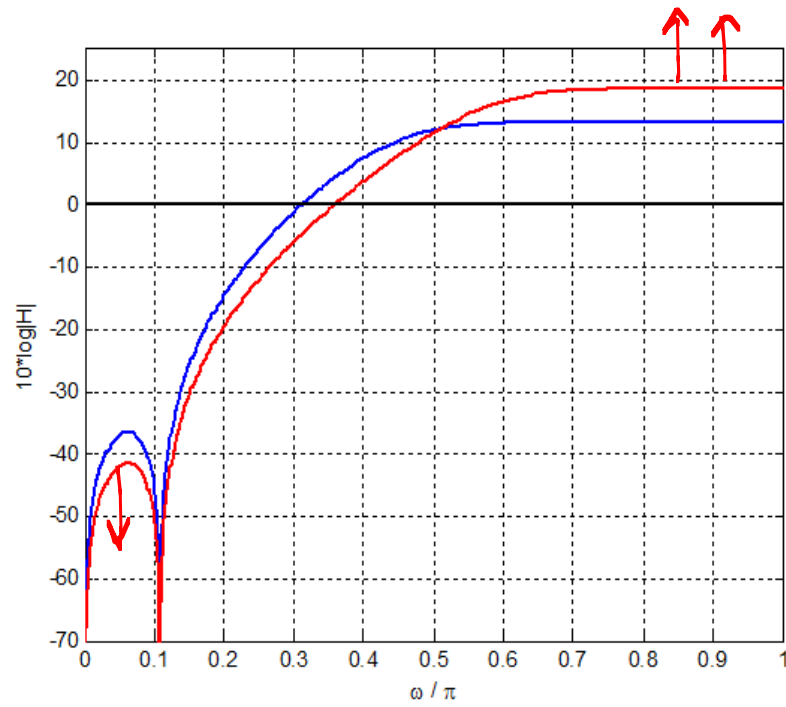
the integral of the log-magnitude of a 'stable' NTF = 0



$$C_1 = C_2$$

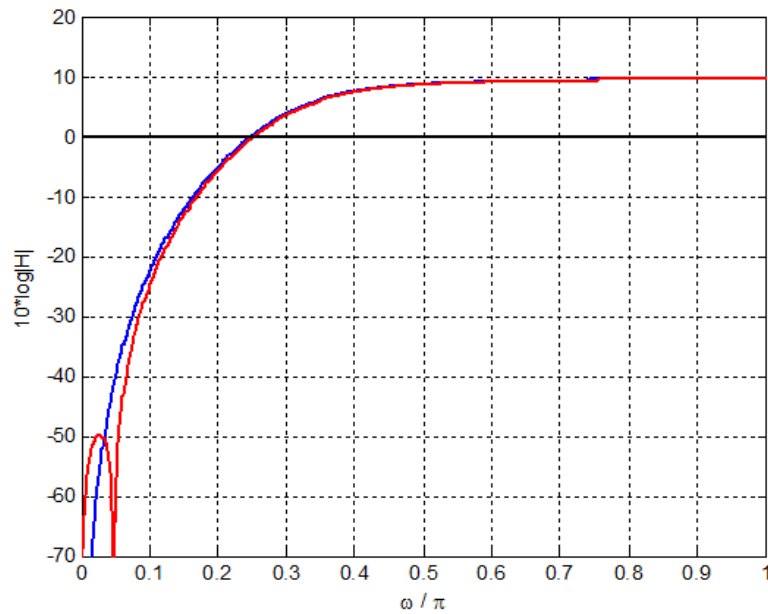
Trade-off between IBN & OBG

"Good in-band performance comes at the cost of poor OBG"



Same order

different OBG

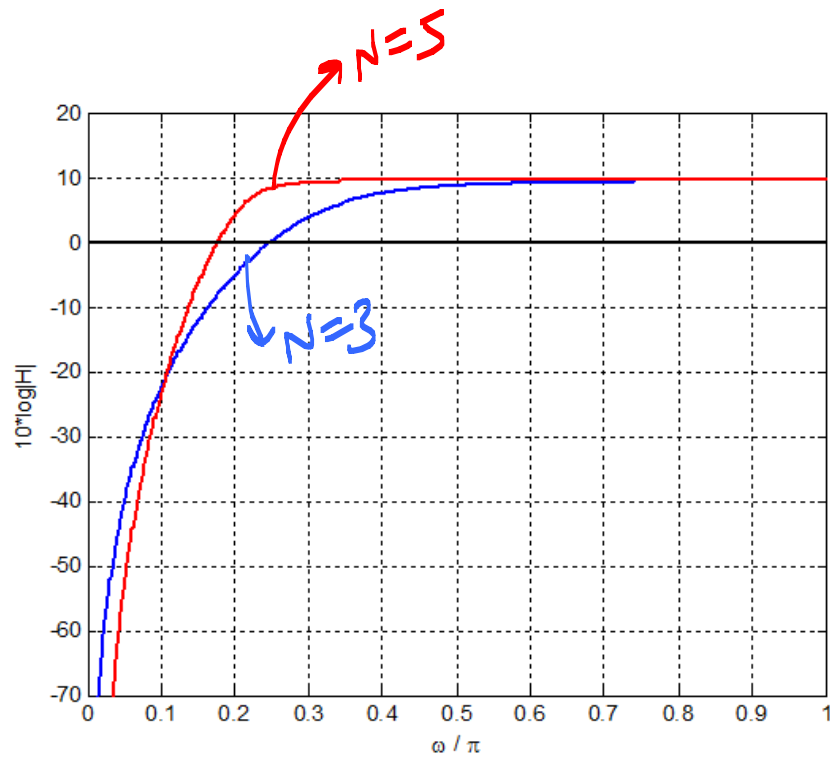


Same OBG

but complex zeros

result in better SNR

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Same OBG
higher-order
↳ better SQNR

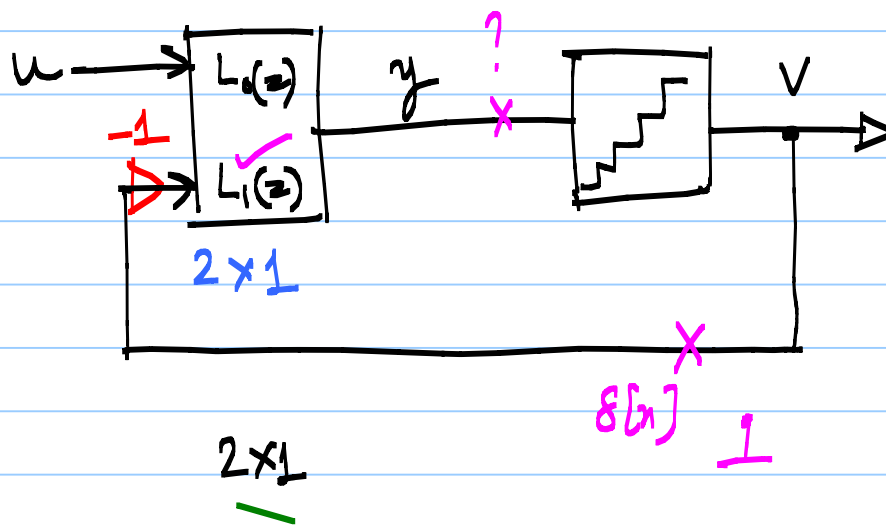
Higher-order Modulators

$$NTF(z) = \frac{N(z)}{D(z)}$$

Architectures?

" $\Delta\Sigma$ Toolbox"

In this notation



$$NTF(z) = \frac{1}{1+L_1(z)}$$

$$STF(z) = \frac{L_0(z)}{1+L_1(z)}$$

$L_1 \in$ loop filter seen by the feedback path

$L_0 \Rightarrow$ loop-filter seen by the input

$$NTF = \frac{1}{1-L_1(z)}$$

Observations

* $|NTF| \approx \frac{1}{|L_1|}$ in the signal band

↑ $|L_1|$ has large gain in the signal band

⇒ quantization noise is reduced

* $|STF| \approx \frac{|L_0|}{|L_1|} \approx 1$ in the signal band

⇒ signal is not distorted

loop filter $L_1(z) = \frac{N_1(z)}{D_1(z)}$

$$NTF(z) = \frac{1}{1-L_1(z)} = \frac{1}{1-\frac{N_1(z)}{D_1(z)}} = \frac{D_1(z)}{D_1(z)-N_1(z)}$$

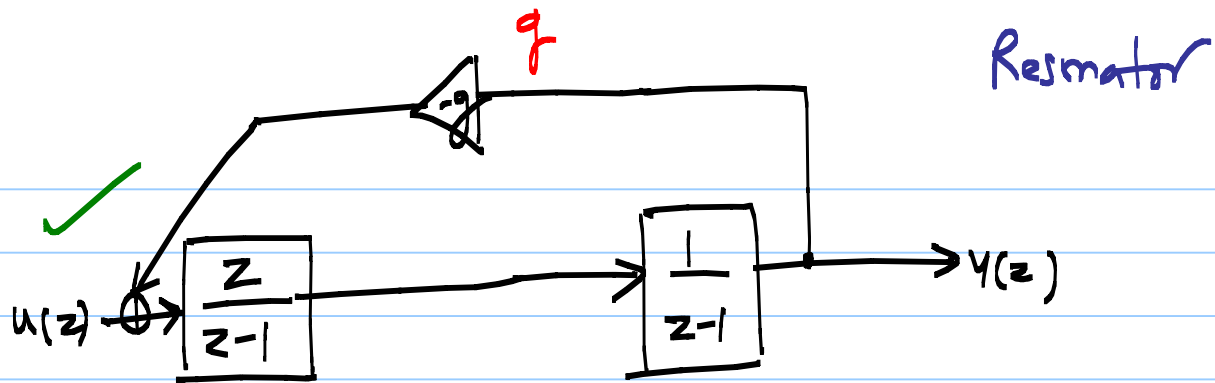
* poles of loop filter \Rightarrow zeros of the NTF
 \uparrow important

* NTF & STF share the same poles

\rightarrow roots of $1-L(z)=0$

$$\text{NTF}(z) \rightarrow \begin{matrix} L_0(z) \\ L_1(z) \end{matrix}$$

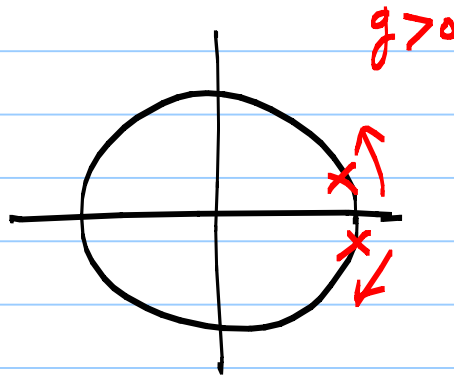
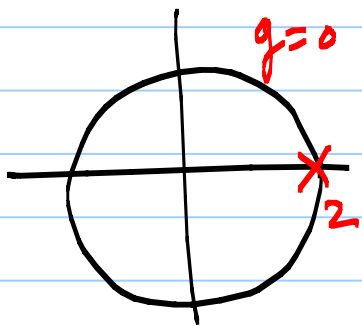
Loop-filter architectures



$$\frac{1}{1-z^{-1}}$$

$$\frac{z^{-1}}{1-z^{-1}}$$

Small amount of
local feedback



Complex poles
in $L_1(z)$

↳ Complex NTF
zeros

$$u \cdot \frac{z}{(z-1)^2} - \frac{gT}{(z-1)^2} \cdot y = y$$

$$\Rightarrow R(z) = \frac{y}{u} = \frac{z}{(z-1)^2 + gT} = \frac{z}{z^2 - (2-g)z + 1}$$

$$= \frac{z}{z^2 - (2 \cos \alpha)z + 1}$$

$$\text{Let } \cos \alpha = 1 - \frac{g}{2}$$

$$= \frac{z}{(z - e^{j\alpha})(z - e^{-j\alpha})}$$

Complex poles of L_1 at $e^{\pm j\alpha}$

$$\text{where } \alpha = \cos^{-1}\left(1 - \frac{g}{2}\right)$$

$$\begin{aligned} \text{Complex roots at } \omega &= \pm \alpha \\ &= \pm \cos^{-1}\left(1 - \frac{g}{2}\right) \end{aligned}$$

$$\cos \alpha = 1 - \delta/2$$

$$1 - 2 \sin^2 \frac{\alpha}{2} = 1 - \delta/2$$

$$\Rightarrow \sin \left(\frac{\alpha}{2} \right) = \pm \sqrt{\frac{\delta}{2}}$$

$$\Rightarrow \alpha \approx \pm \sqrt{\delta} \quad \text{for } \alpha \ll \pi \quad \because \sin \alpha \approx \alpha$$

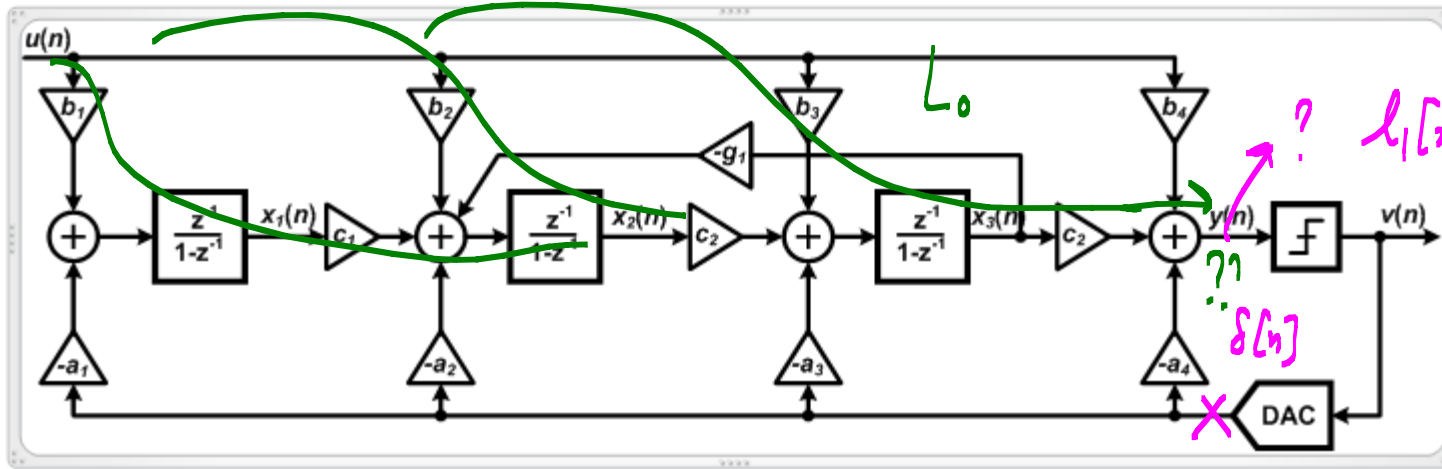
poles at $z = e^{\pm j\sqrt{\delta}}$ → complex NTF zeros

NTF

realize NTF() in the DS Toolbox

↳ [a, b, g] values

$\delta[n]$



By inspection:

$$L_1(z) = - \frac{a_1 + a_2(z-1) + \dots + a_N(z-1)^{N-1}}{(z-1)^N} \leftarrow \text{NTF}(z)$$