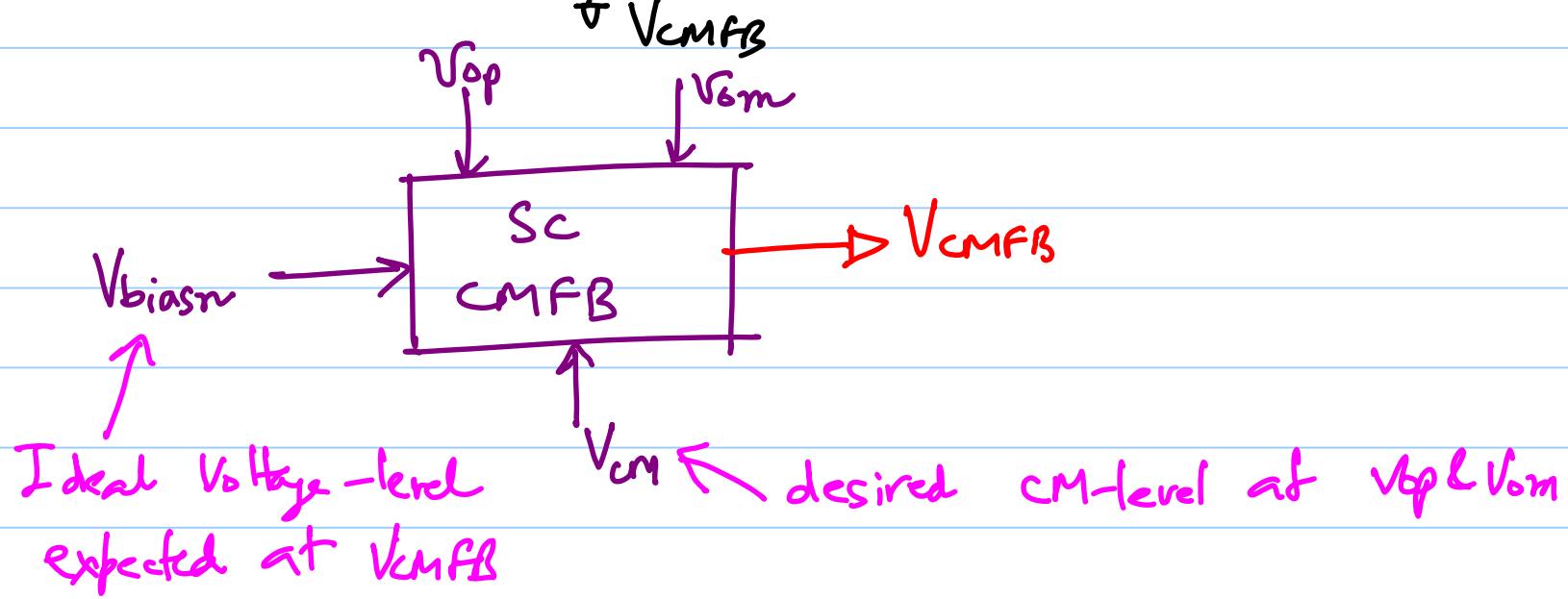
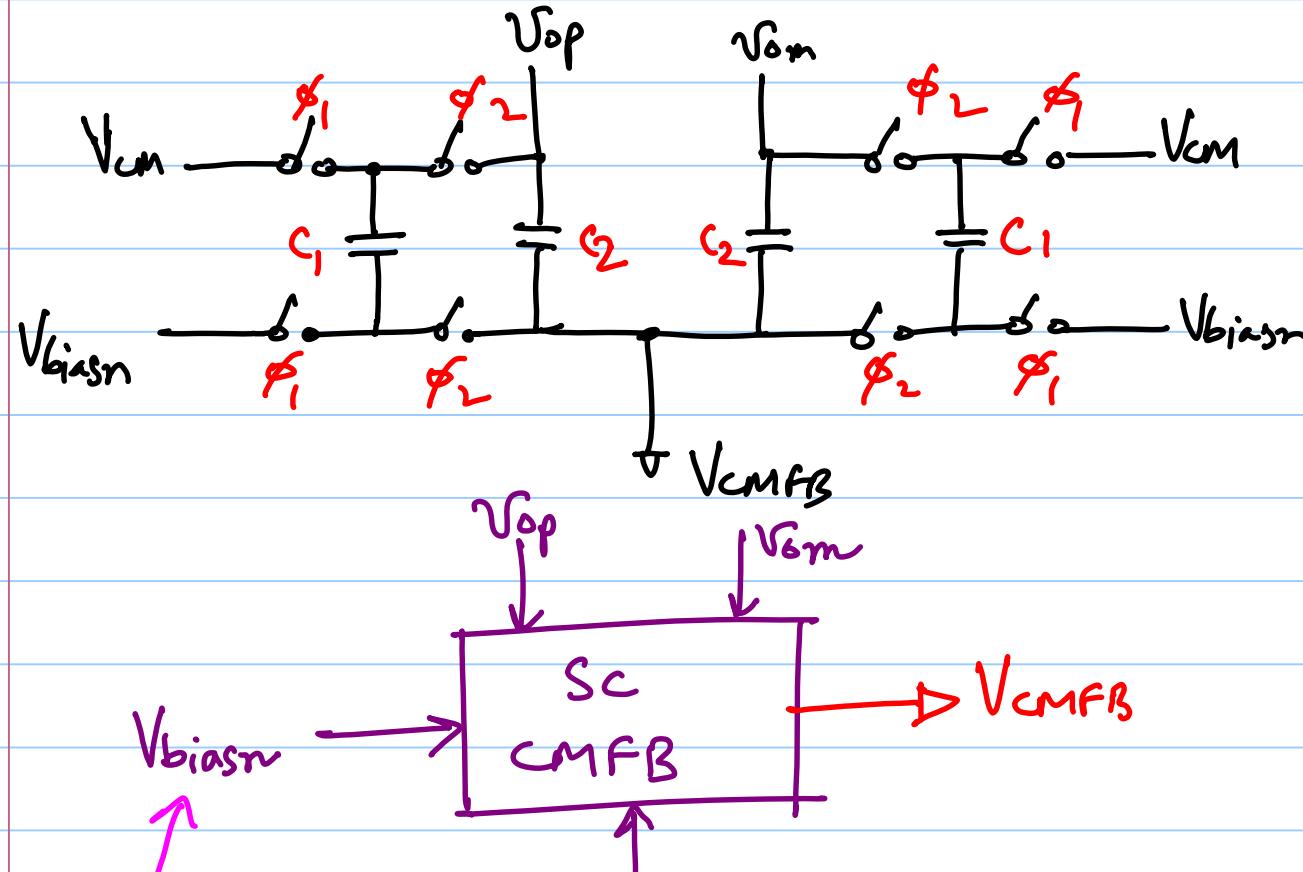


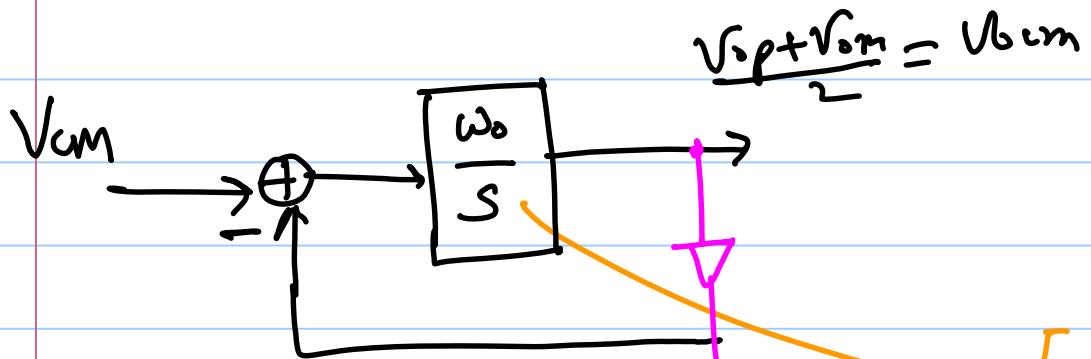
ECE 614 - Lecture 8

Note Title

9/18/2014

SC CMFB Circuit

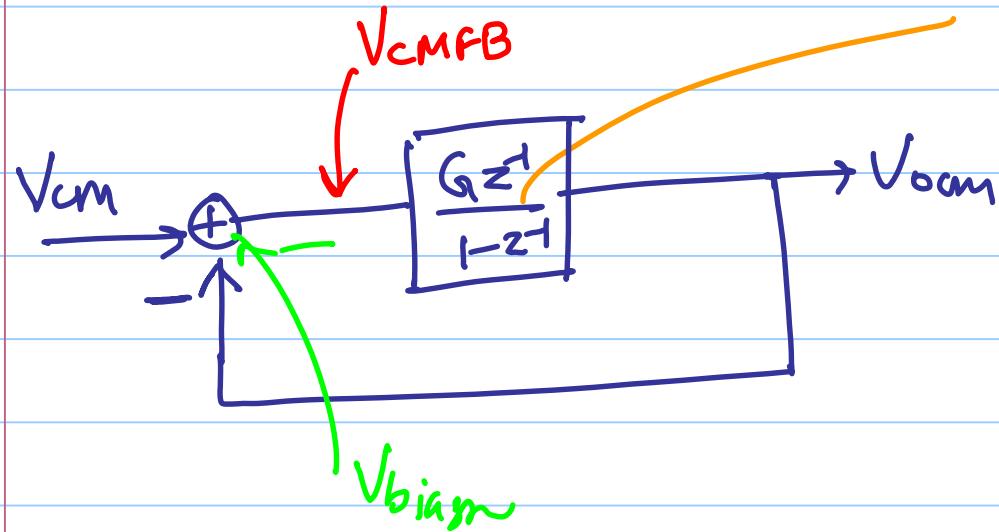




$$\frac{V_{opt} + V_{cm}}{2} = V_{outm}$$

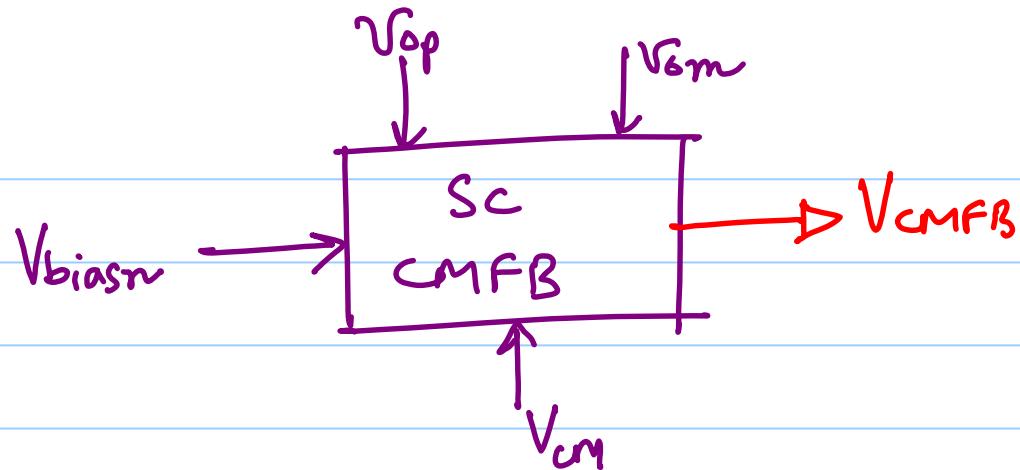
$V_{outm} \rightarrow V_{cm}$

Integrating controller



-ve feedback loop
that drives

$$\frac{V_{opt} + V_{cm}}{2} \rightarrow V_{cm}$$

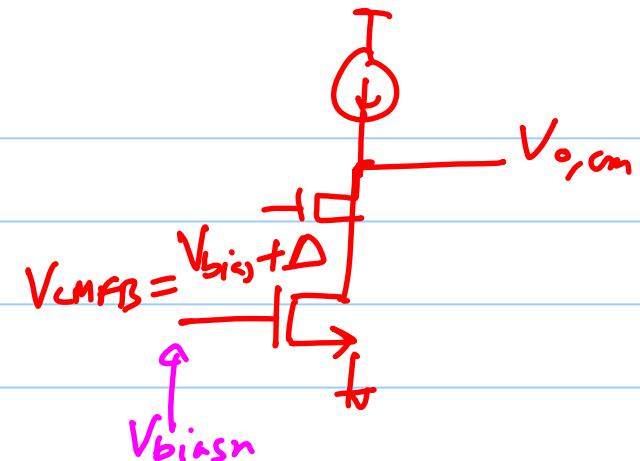


$$V_{error} = V_{CM} - V_{o,cm} = V_{biasn} - V_{CMFB} \Rightarrow 0$$

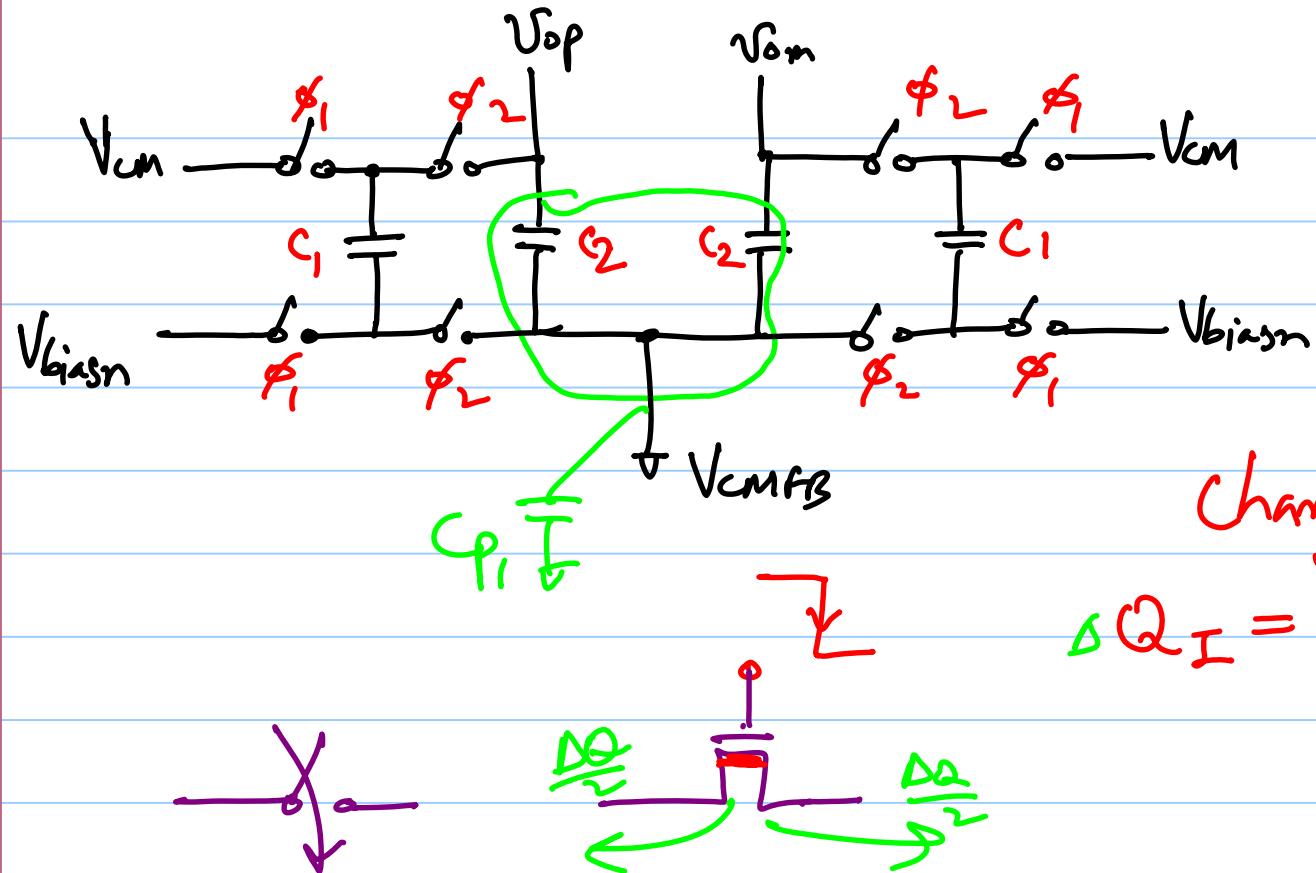
$$\begin{matrix} \uparrow \\ (\frac{V_{op} + V_{cm}}{2}) \end{matrix}$$

$$\begin{matrix} \uparrow \\ (\frac{V_{biasn} + V_{cmfB}}{2}) \end{matrix}$$

$$V_{o,cm} \simeq V_{cm} - \Delta$$



Advantages: φ_p swing is not limited by the CM-detector
& no resistive loading



→ Switches ϕ_1 inject charge into $C_1 \Rightarrow \Delta Q$

In steady-state

$$C_1(V_{CM} - V_{biasn}) = C_1(V_{o,cm} - V_{CMFB}) + \Delta Q$$

$$V_{cm} - V_{o,om} = V_{biasn} - V_{CMFB} + \underbrace{\frac{\Delta Q}{C_1}}$$

Induces an offset into
 $V_{o,om}$

$V_{o,om}$ is away from V_{cm} by $\frac{\Delta Q}{C_1}$

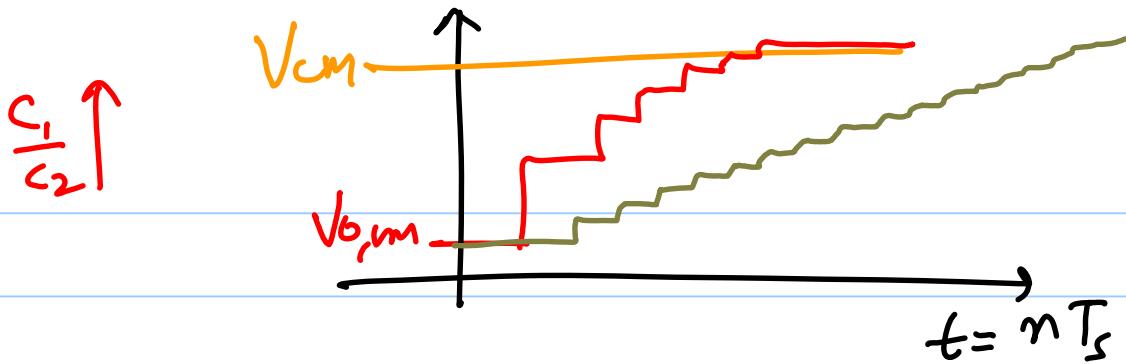
① $\because \Delta Q \propto W$, small WL \Rightarrow switch resistance
 $\hookrightarrow R_C$ time constant

② $C_1 \uparrow$
 \hookrightarrow reduce the offset due to C.I.

Single-stage opamp \Rightarrow more loading on the outputs during
 ϕ_2 phase

$$f_m = \frac{Q_m I}{C_L}$$

Analysis:



final value $\overline{V_{0,cm}} = V_{cm} + \frac{V_{off} + V_{on}}{2}$

$$\overline{V_{0,cm}} = \frac{V_{cm} + \left[\left(1 + \frac{C_1}{C_2} \right) (V_{cm} - V_{biasn}) \right] - \frac{\Delta Q}{C_1} + \frac{I_{Leak} \cdot T}{2C_1}}{1 + \frac{1}{A_{cm}} \cdot \left(1 + \frac{C_1}{C_2} \right)}$$

Step-size of settling depends on $\frac{C_1}{C_2}$

If $\frac{C_1}{C_2} \gg 1 \Rightarrow$ settling is fast

Excess loading on the amplifier

$$\phi_2 \Rightarrow C_1 + C_2 + C_{\text{load}}$$

$$\phi_1 \Rightarrow C_2 + C_{\text{load}}$$

Algorithm: choose C_2 such that

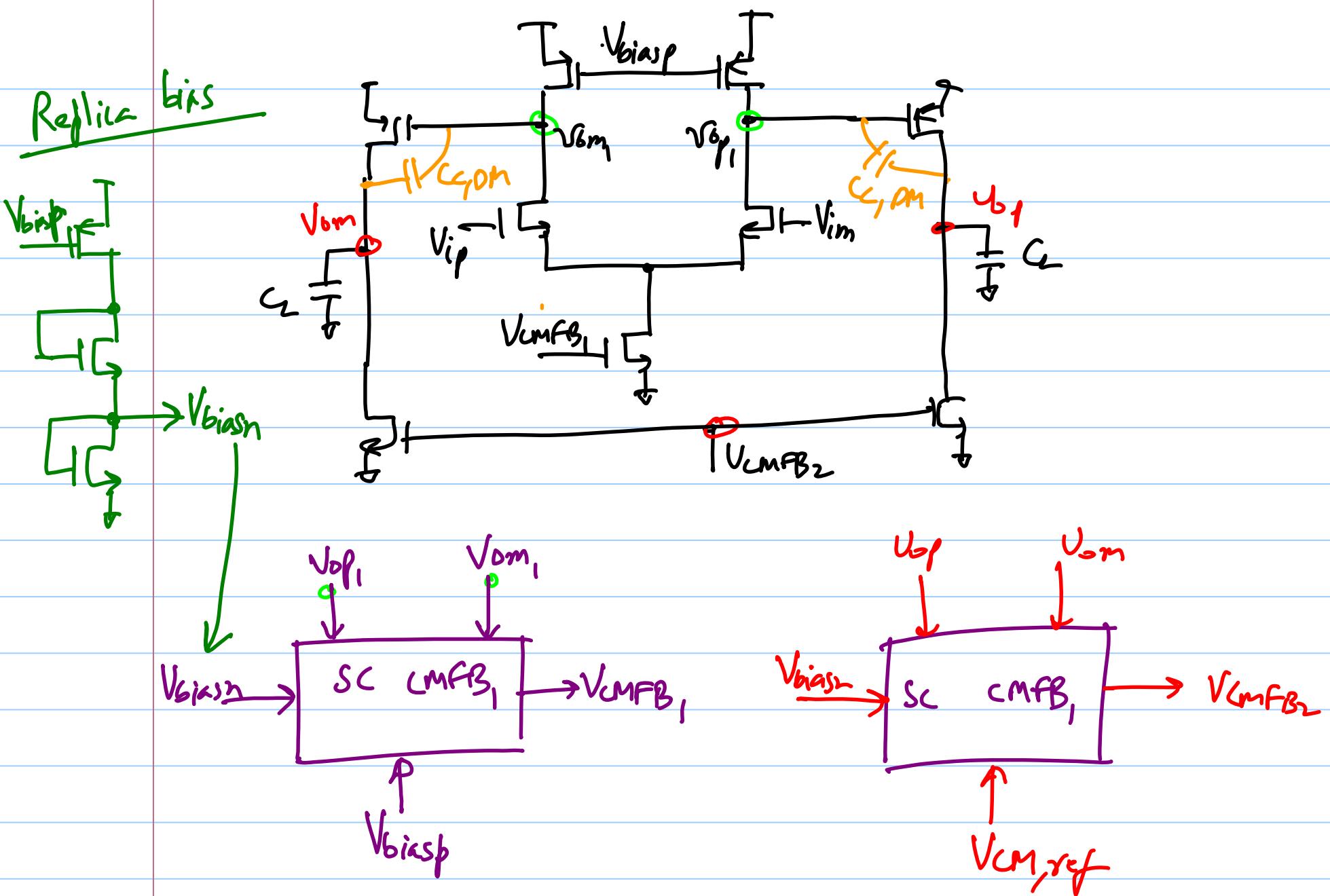
$$\omega_{a, \text{CMFB}} \simeq \omega_{h, \text{DM}}$$

and choose $C_1 = 5$ to 10 times of C_2
for faster settling

Example

$$C_2 \simeq 10fF$$

$$C_1 = 50fF$$



* A periodically switched system

Spec RF

CT equivalent

periodic steady-state \Rightarrow PSS \leftarrow operating point

periodic stability \Rightarrow PSTB \leftarrow STB

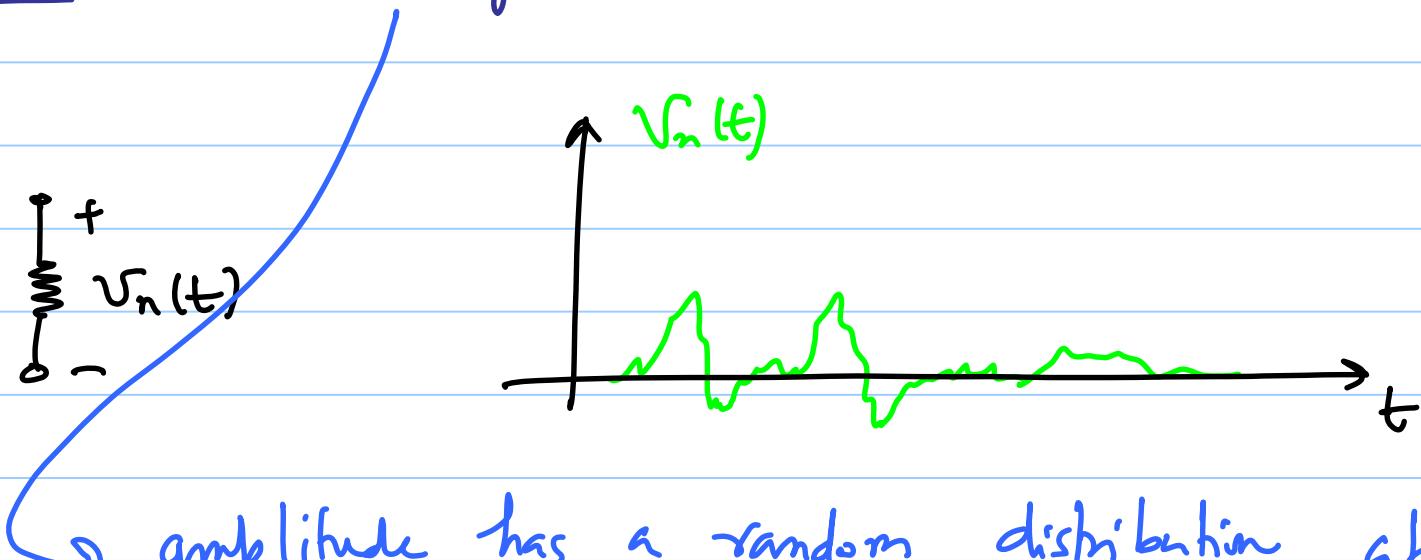
" Az response \Rightarrow PAC \nwarrow $X(e^{j\omega})$

" Transient "

T_{SH} parameter

Noise

Noise: Random process



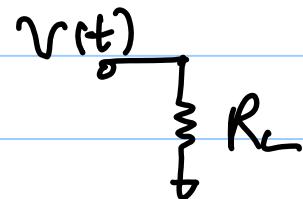
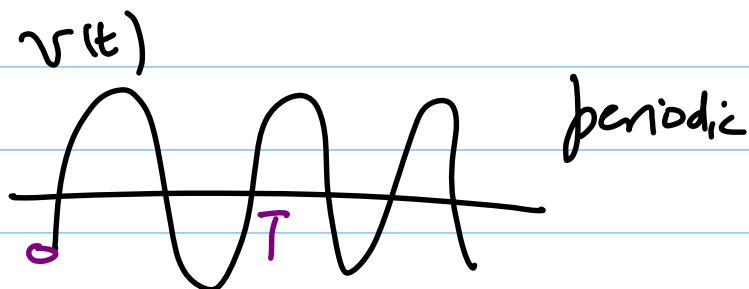
amplitude has a random distribution at any instance of time

↳ need to look at it statistically

* Which properties of noise can be predicted?

⇒ In many cases, average power of noise is predictable

↳ most noises in circuits fundamentally exhibit constant average power.

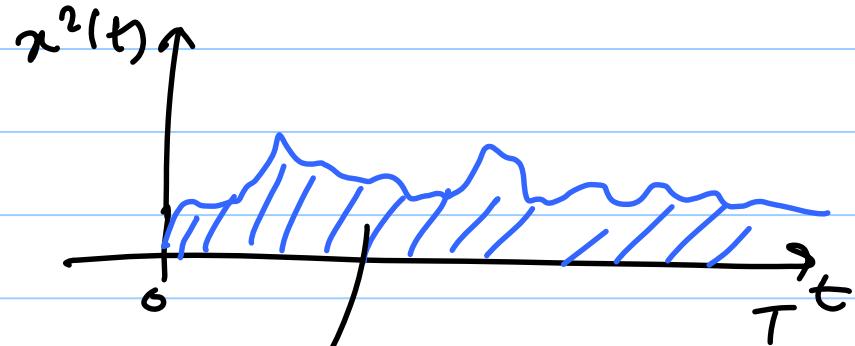
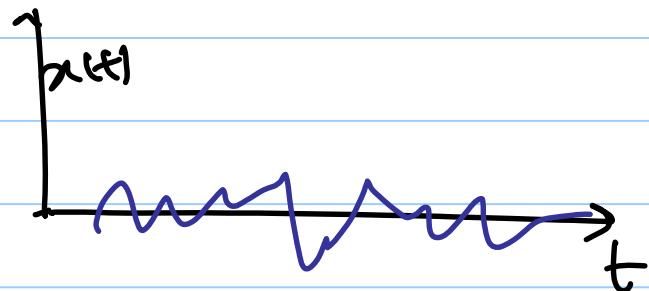


The average power delivered by a periodic voltage source $v(t)$ to a load R_L

$$P_{av} = \frac{1}{T} \int_{-T/2}^{T/2} \frac{v^2(t)}{R_L} dt = \frac{V_p^2}{2R_L} \text{ for sine}$$
$$\frac{V_{DC}^2}{R_L} \text{ for DC}$$

for a random signal $x(t)$

$$P_{av} = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T_L}^{T_L} \frac{x^2(t)}{R_L} dt$$



$$\frac{\text{Area}}{T} \Rightarrow P_{av}$$

