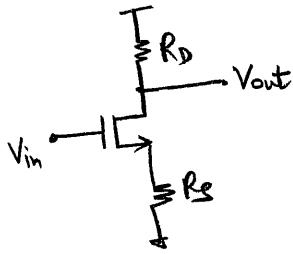


HW3 solutions

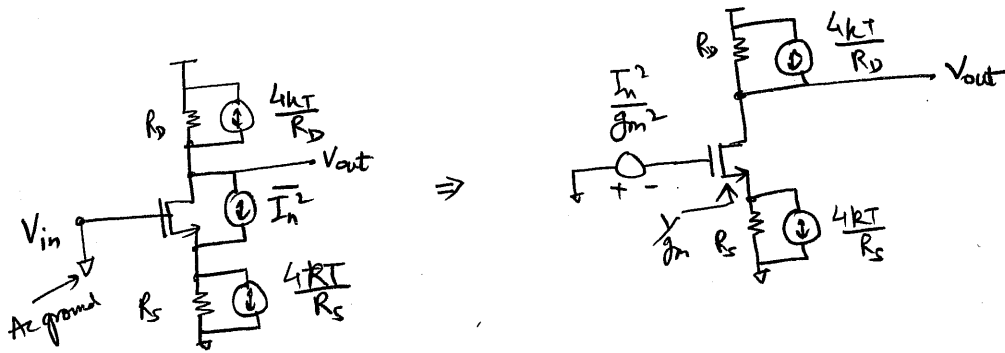
①

Problem 3 :

(a)



$$A_v = - \frac{g_m R_D}{1 + g_m R_S}$$



$$\overline{I_n^2} = \frac{8}{3} kT g_m$$

for the $\overline{I_n^2}$ noise current it is divided between $\frac{1}{g_m}$ and R_S

⇒ current flowing into transistor and buffered to the

$$\text{output} \Rightarrow \left(\frac{R_S}{R_S + \frac{1}{g_m}} \right) \cdot \overline{I_n^2}$$

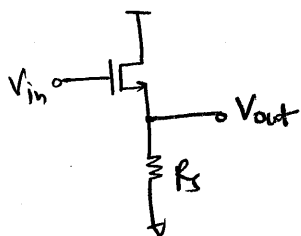
$$\Rightarrow \overline{V_{n,out}^2} = \frac{4kT}{R_D} \times R_D^2 + \frac{\overline{I_n^2}}{g_m^2} \times \left(\frac{g_m R_D}{1 + g_m R_S} \right)^2 + \left(\frac{R_S}{R_S + \frac{1}{g_m}} \right)^2 \times \frac{4kT}{R_S} \times R_D^2$$

$$= 4kT R_D + \frac{8}{3} kT \cdot \frac{1}{g_m} \cdot \left(\frac{g_m R_D}{1 + g_m R_S} \right)^2 + 4kT R_S \cdot \left(\frac{g_m R_D}{1 + g_m R_S} \right)^2$$

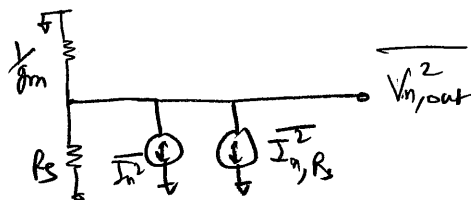
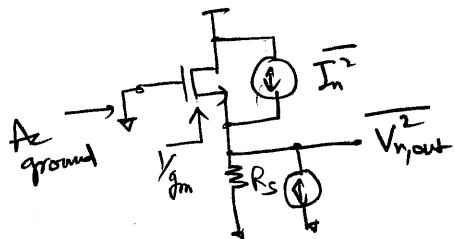
$$\Rightarrow \overline{V_{n,in}^2} = \frac{\overline{V_{n,out}^2}}{A_v^2} = \frac{8}{3} kT \cdot \frac{1}{g_m} + 4kT R_S + 4kT R_D \left(\frac{1 + g_m R_S}{g_m R_D} \right)^2$$

⇒ to minimize $\overline{V_{n,in}^2}$, $g_m \uparrow$, $R_S \downarrow$, $R_D \uparrow$

(b)



$$A_v = \frac{R_S}{\frac{1}{g_m} + R_S} = g_m \cdot (\frac{1}{g_m} \parallel R_S)$$



$$\overline{V_{n,out}^2} = (\overline{I_n^2} + \frac{4kT}{R_S}) (\frac{1}{g_m} \parallel R_S)^2$$

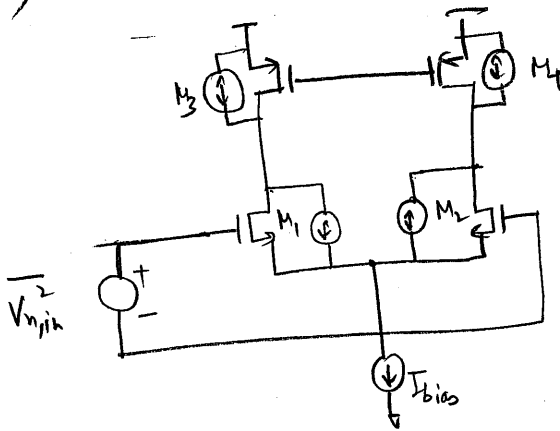
$$= (4kT \cdot \frac{2}{3} g_m + 4kT \cdot \frac{1}{R_S}) (\frac{1}{g_m} \parallel R_S)^2$$

$$\Rightarrow \overline{V_{n,in}^2} = \frac{\overline{V_{n,out}^2}}{A_v^2} = 4kT \cdot \frac{2}{3} \frac{1}{g_m} + 4kT \cdot \frac{1}{g_m^2 R_S}$$

$$\Rightarrow \overline{V_{n,in}^2} \downarrow \Rightarrow g_m \uparrow, R_S \uparrow$$

(3)

(c)



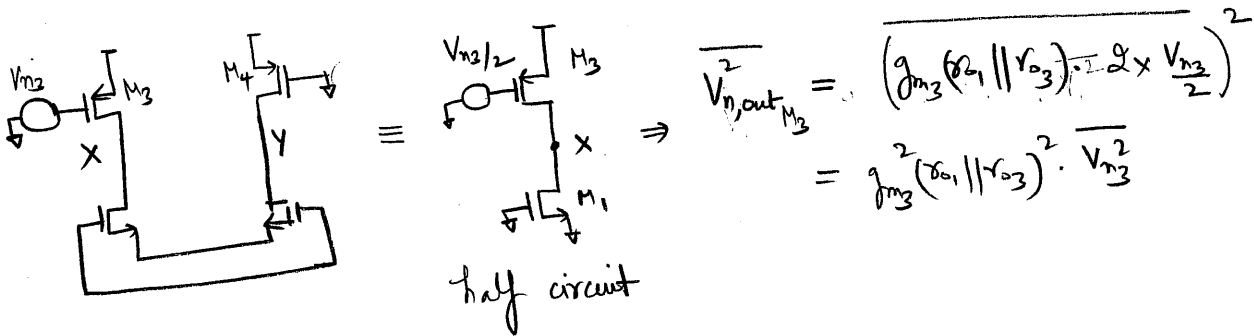
Noise current due to I_{bias} is
 CM at the output $\Rightarrow$ no effect on $V_{n,in}^2$

* short the input ports to find $V_{n,in}^2$

* Reflect $\overline{I_{n1}^2}$, $\overline{I_{n2}^2}$, $\overline{I_{n3}^2}$ & $\overline{I_{n4}^2}$ to the input side to find $V_{n,in}^2$

$$\overline{V_{n,in}^2} |_{M1, M2} = 2 \overline{V_{n1}^2} = 2 \frac{\overline{I_{n1}^2}}{g_{m1}^2} = 2 \times \frac{8}{3} kT \frac{g_{m1}}{g_{m1}^2} = 2 \times \frac{8}{3} \frac{kT}{g_{m1}} \rightarrow (1)$$

for noise contribution from $M3$ & $M4$



$$\overline{V_{n,out}^2} |_{M3} = \left(g_{m3} (r_{o1} \parallel r_{o3}) \cdot 2 \times \frac{V_{n3}}{2} \right)^2 = g_{m3}^2 (r_{o1} \parallel r_{o3})^2 \cdot \overline{V_{n3}^2}$$

$$\Rightarrow \overline{V_{n,out}^2} |_{M3, M4} = g_{m3}^2 (r_{o1} \parallel r_{o3})^2 \overline{V_{n3}^2} + g_{m4}^2 (r_{o2} \parallel r_{o4})^2 \overline{V_{n4}^2} = 2 \times g_{m3}^2 (r_{o1} \parallel r_{o3})^2 \overline{V_{n3}^2} \rightarrow (2)$$

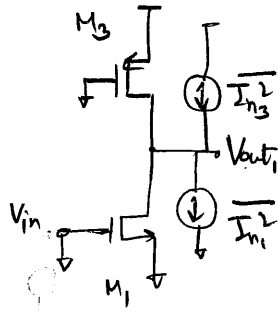
$$\Rightarrow \overline{V_{n,in}^2} = 2 \overline{V_{n1}^2} + 2 \cdot \frac{g_{m3}^2}{g_{m1}^2} \cdot \overline{V_{n3}^2} \quad \therefore A_v = g_{m1} (r_{o1} \parallel r_{o3})^2$$

$$\boxed{\overline{V_{n,in}^2} = 8kT \left(\frac{2}{3g_{m1}} + \frac{2g_{m3}}{3g_{m1}^2} \right)}$$

Short-cut for differential circuits

(4)

* find input referred noise of the half circuit
and multiply by 2

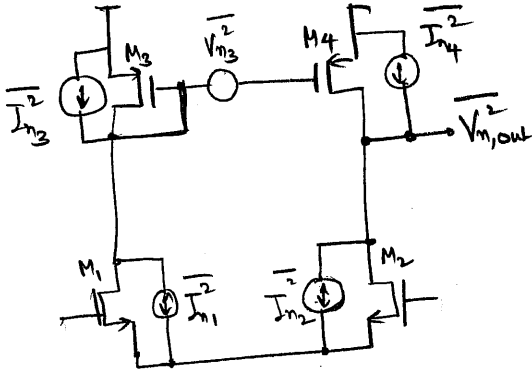


$$\Rightarrow \overline{V_{n,in}^2} = 2 \times \left(\frac{\overline{I_{n1}^2}}{g_{m1}^2} + \frac{\overline{I_{n3}^2} \cdot (\delta_{o1} \parallel r_{o3})^2}{g_{m1}^2 (\delta_{o1} \parallel r_{o3})^2} \right)$$

$$= 2 \times \left(\frac{8KT}{3} \frac{1}{g_{m1}} + \frac{8}{3} KT \frac{g_{m3}}{g_{m1}^2} \right)$$

$$\boxed{\overline{V_{n,in}^2} = 8KT \left(\frac{2}{3g_{m1}} + \frac{2g_{m3}}{3g_{m1}^2} \right)}$$

(d)



Most of the noise current $\overline{I_{n1}}$ and $\overline{I_{n3}}$ flows into M_3 due to $\frac{1}{g_{m3}}$ impedance

$\Rightarrow$ This can be referred to the gate of M_3 as

$$\overline{V_{n3}}^2 = \left(\frac{\overline{I_{n3}}^2 + \overline{I_{n1}}^2}{g_{m3}^2} \right)$$

$$g_{m1} = g_{m2} \quad \& \quad g_{m3} = g_{m4}$$

$$r_{o1} = r_{o2} \quad \& \quad r_{o3} = r_{o4}$$

This noise voltage is then reflected into the output $\overline{V_{n,out}}^2$.

$\Rightarrow$

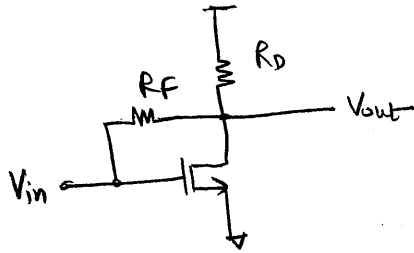
$$\overline{V_{n,out}}^2 = \left[\overline{I_{n2}}^2 + \overline{I_{n4}}^2 + \frac{2}{g_{m4}} \frac{(\overline{I_{n3}}^2 + \overline{I_{n1}}^2)}{g_{m3}^2} \right] (\overline{v_{o3}} \parallel r_{o4})^2$$

$$= \frac{8}{3} kT \left[g_{m2} + g_{m4} + \frac{2g_{m3}}{g_{m1}^2} \right] \cdot (\overline{v_{o3}} \parallel r_{o4})^2$$

$$\Rightarrow \overline{V_{n,in}}^2 = \frac{\overline{V_{n,out}}^2}{g_{m1}^2 (\overline{v_{o3}} \parallel r_{o4})^2} = \boxed{\frac{8}{3} kT \left[\frac{2}{g_{m1}} + \frac{2g_{m3}}{g_{m1}^2} \right]}$$

$\Rightarrow$ Same input referred noise as part (c)

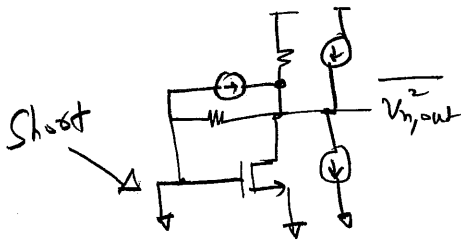
7



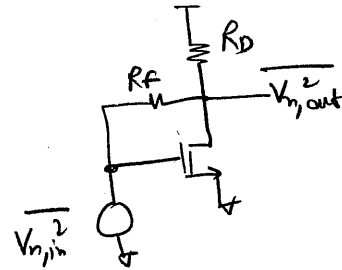
6

Step 1: find $\overline{V_{n,in}^2}$

* shoot the input to ground and equate the output noise of the circuits below



&



$$\Rightarrow \overline{V_{n,out}^2} = (\overline{I_n^2} + \overline{I_{n,R_F}^2} + \overline{I_{n,R_D}^2}) (R_D \parallel R_F)^2$$

$$= 4kT \left(\frac{2}{3} g_m + \frac{1}{R_F} + \frac{1}{R_D} \right) (R_D \parallel R_F)^2 \quad \text{①}$$

$$\overline{V_{n,out}^2} = \overline{V_{n,in}^2} \cdot A_v^2 \quad \text{②}$$

Here $A_v = \left(-g_m + \frac{1}{R_F} \right) (R_F \parallel R_D)$

Equating ① + ②, we get

$$\overline{V_{n,in}^2} = \frac{4kT \left(\frac{2}{3} g_m + \frac{1}{R_F} + \frac{1}{R_D} \right) (R_D \parallel R_F)^2}{\left(-g_m + \frac{1}{R_F} \right)^2 (R_D \parallel R_F)^2}$$

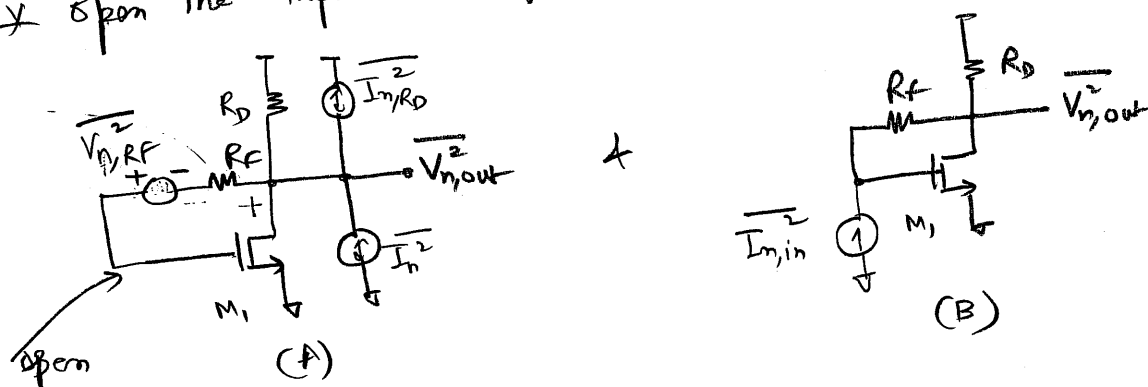
$$\overline{V_{n,in}^2} = \frac{4kT \left(\frac{2}{3} g_m + \frac{1}{R_F} + \frac{1}{R_D} \right)}{\left(-g_m + \frac{1}{R_F} \right)^2}$$

Ans.

Step 2: find $\overline{I_{n,in}}^2$

⑦

* open the input and equate the output noise of the circuit below



Circuit (A):

Sum the currents at the output node:

$$\frac{V_{n,out}}{R_D} + I_{n,M_1} - I_{n,RD} + g_m (V_{n,out} - V_{n,RF}) = 0$$

$$\Rightarrow V_{n,out} = \frac{-I_{n,M_1} + I_{n,RD} + g_m V_{n,RF}}{(g_m R_D + 1)} \cdot R_D \rightarrow \textcircled{1}$$

Circuit (B):

the transimpedance gain can be found as

$$R_T = \frac{V_{out}}{I_{in}} = -\frac{(g_m R_F - 1)}{(1 + g_m R_D)} \cdot R_D$$

$$\Rightarrow V_{n,out} = I_{n,in} \times \frac{-(g_m R_F - 1)}{(1 + g_m R_D)} \cdot R_D \rightarrow \textcircled{2}$$

from ① & ②

$$I_{n,in} = \frac{-I_{n,M_1} + I_{n,RD} + g_m V_{n,RF}}{(-g_m R_F + 1)}$$

Computing the mean square values and assuming $g_m R_F \gg 1$,

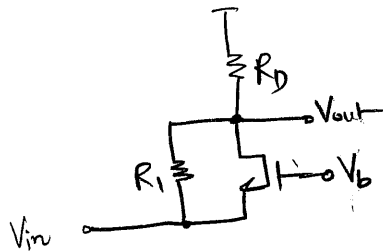
⑧

$$\overline{I_{n,in}^2} = \frac{\overline{I_{n,n}^2} + \overline{I_{n,R_D}^2} + g_m^2 \cdot \overline{V_{n,R_F}^2}}{g_m^2 R_F^2}$$

$$\boxed{\overline{I_{n,in}^2} = 4kT \left(\frac{2}{3} \cdot \frac{1}{g_m R_F^2} + \frac{1}{g_m^2 R_F^2 R_D} + \frac{1}{R_F} \right)} \quad \text{Ans.}$$

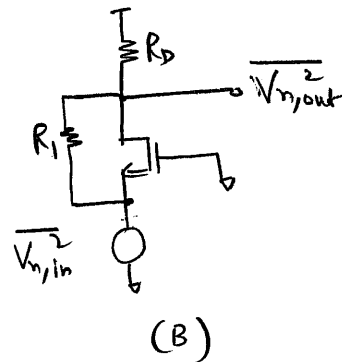
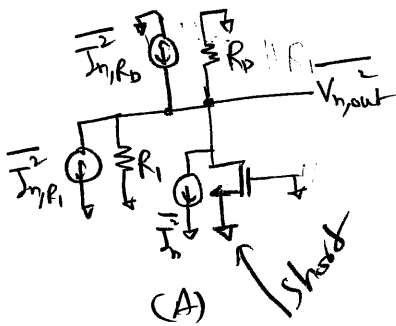
(b)

9



Step 1: find $\overline{V_{n,in}^2}$:

* Short the input and equate $\overline{V_{n,out}^2}$



$$(A) \rightarrow \overline{V_{n,out}^2} = 4kT \left[\frac{2}{3} g_{m1} + \frac{1}{R_1} + \frac{1}{R_D} \right] (R_1 \parallel R_D)^2 \rightarrow (1)$$

$$(B) \rightarrow \text{Voltage gain } A_v = (g_{m1} + \frac{1}{R_1}) (R_1 \parallel R_D)$$

$$\Rightarrow \overline{V_{n,in}^2} = \frac{\overline{V_{n,out}^2}}{A_v^2} \rightarrow (2)$$

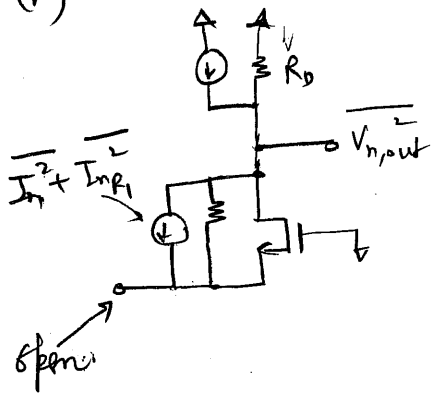
from (1) & (2),

$$\boxed{\overline{V_{n,in}^2} = 4kT \left(\frac{1}{g_{m1} + \frac{1}{R_1}} \right)^2 \left(\frac{2}{3} g_{m1} + \frac{1}{R_1} + \frac{1}{R_D} \right)} \quad \text{Ans}$$

Step 1: find $\overline{I_{n,in}^2}$

* Open the input and equate $\overline{V_{n,out}^2}$

(A)

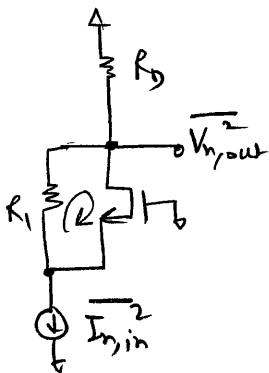


$\therefore$ current at the source of $M_1 \Rightarrow I_n + I_{n,R_1} + I_D = 0$

The current $I_n + I_{n,R_1}$ doesn't flow into R_D

$$\Rightarrow \overline{V_{n,out}^2} = 4kT R_D \rightarrow (1)$$

(B)



$$\overline{V_{n,out}^2} = \overline{I_{n,in}^2} R_D^2 \rightarrow (2)$$

from (1) & (2)

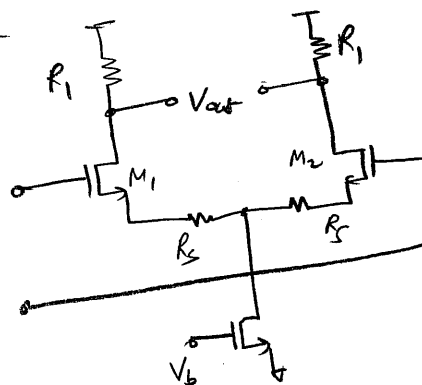
$$\boxed{\overline{I_{n,in}^2} = \frac{4kT}{R_D}}$$

Ans.

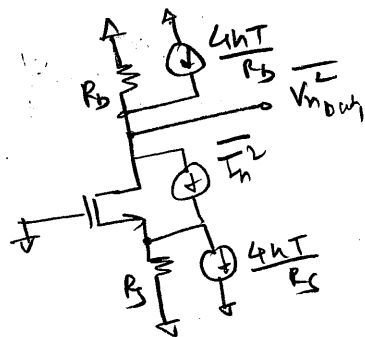
Extra Problem 1 :

(a) M_3 doesn't contribute differential noise

$$|A_v| = \frac{g_{m1} R_1}{1 + g_{m1} R_S}$$



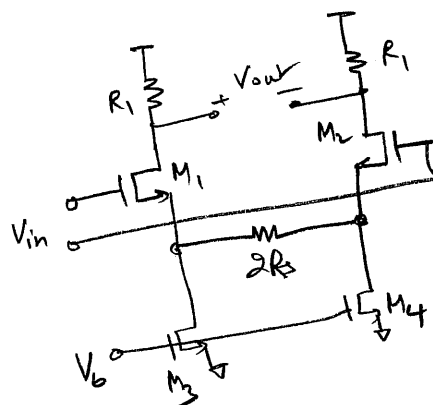
Half Circuit



$$\overline{V_{n,out}^2} = 2 \times 4kT \times \left[\frac{1}{R_1} + \frac{2}{3} g_{m1} \left(\frac{g_m}{1 + g_{m1} R_S} \right)^2 + \frac{1}{R_S} \left(\frac{R_S}{1 + g_{m1} R_S} \right)^2 \right] R_D^2$$

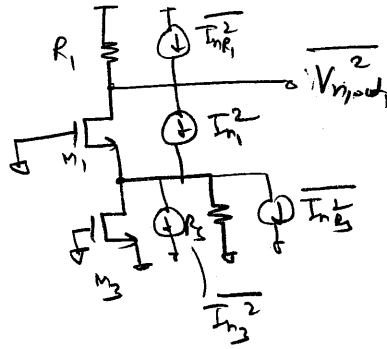
$$\Rightarrow \overline{V_{n,in}^2} = 8kT \left[\frac{2}{3} g_{m1} + R_S + \frac{1}{R_1} \left(\frac{1 + g_{m1} R_S}{g_{m1}} \right)^2 \right] A_m$$

(b) Here M_3 & M_4 contribute differential noise



Half circuit

* I_{n3} is divided between R_s and $1/g_{m1}$



$$\overline{V_{n,out}(b)}^2 = \overline{V_{n,out}(a)}^2 + 2 \times \frac{8}{3} kT g_{m3} \left(\frac{R_s}{R_s + 1/g_{m1}} \right)^2 R_D^2$$

$\Rightarrow$

$$\overline{V_{n,in}(b)}^2 = 8kT \left[\frac{2}{3} g_{m1} + R_s + \frac{1}{R_D} \left(\frac{1 + g_{m3} R_s}{g_{m1}} \right)^2 + \frac{2}{3} g_{m3} R_s^2 \right]$$

$$\Rightarrow \overline{V_{n,in}(b)}^2 = \overline{V_{n,in,a}}^2 + \underbrace{2(4kT) \left(\frac{2}{3} g_{m3} R_s^2 \right)}_{\text{Extra noise contributed by } M_3 \text{ \& } M_4}$$

$\Rightarrow$ circuit (a) has large input CMR but suffers from higher input referred noise.

The gains of the circuits are equal.

Extra problem (2) : See lecture notes.