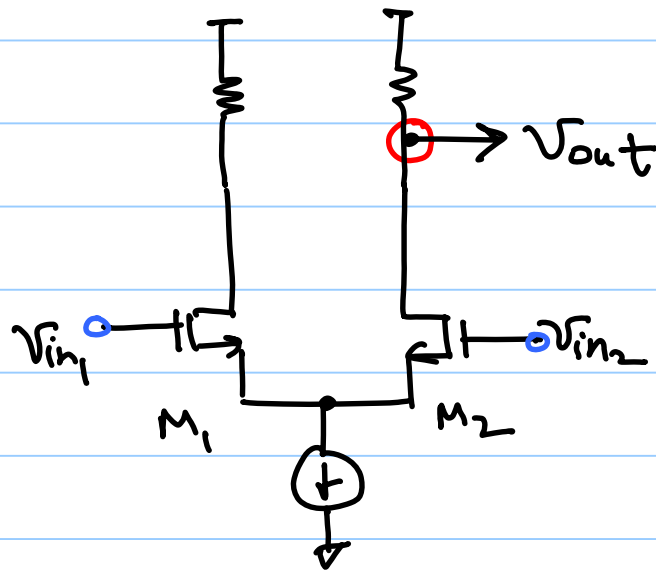
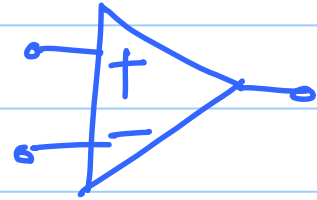


ECE 511 - Lecture 22

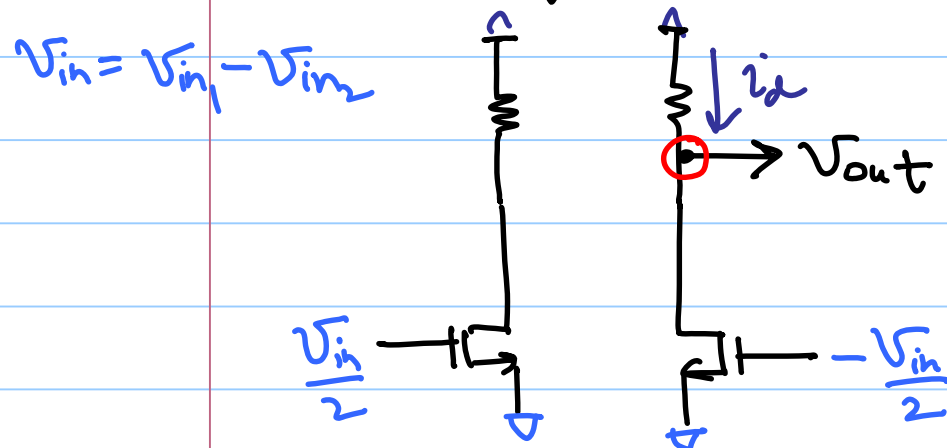
Note Title

4/9/2015

Single-ended Diffamp



$$A_{V,DM} =$$



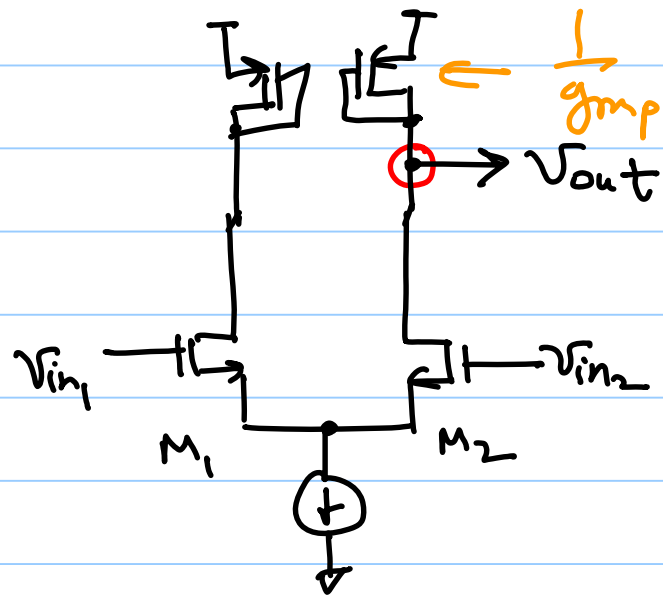
Half DM circuit

$$\begin{aligned} V_{out} &= -i_d (R_D \parallel r_o) \\ &= -(-g_m \frac{V_{in}}{2}) R_D \parallel r_o \end{aligned}$$

$$A_{V,DM} = + \frac{g_m R_D \parallel r_o}{2}$$

$$\approx \frac{1}{2} g_m R_D$$

Diode-connected load $\rightarrow$ low-gain



$$A_v = + \frac{g_{mn}}{2} \cdot \frac{1}{g_{mp}}$$

$\hookrightarrow$ low-gain

③ Current Source load

Single ended output

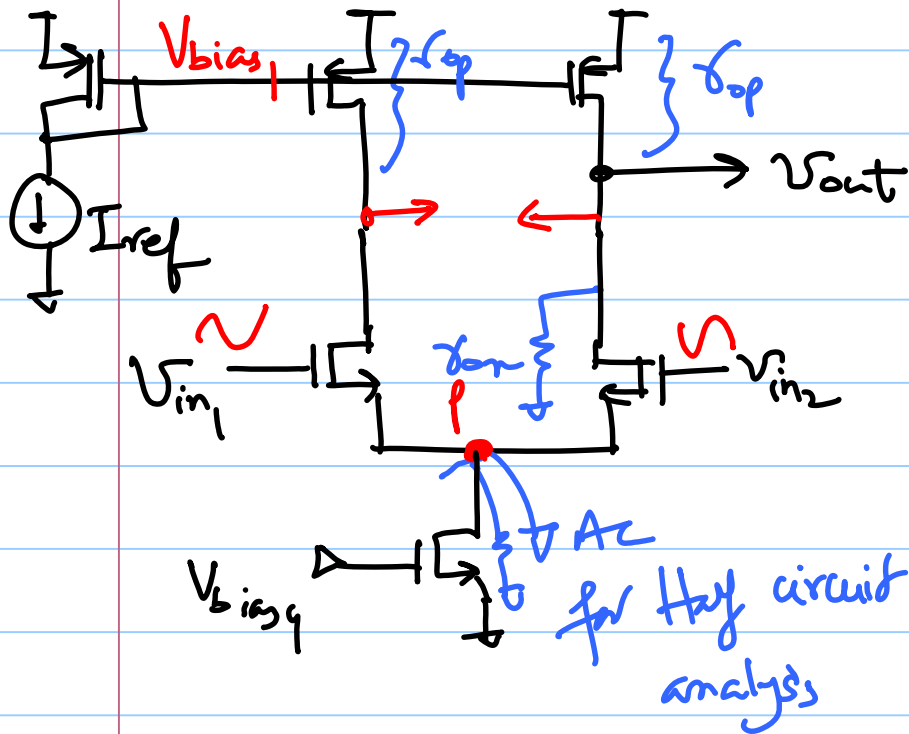
$$A_{v,DM} = \frac{1}{2} g_{m_n} (r_{on} || r_{op})$$

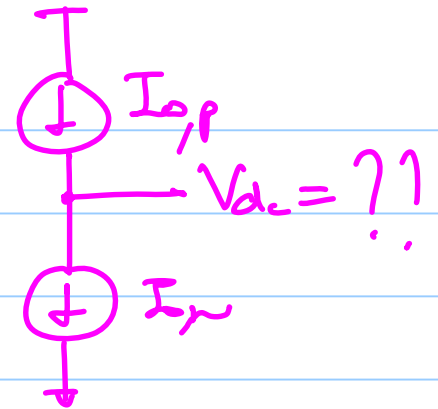
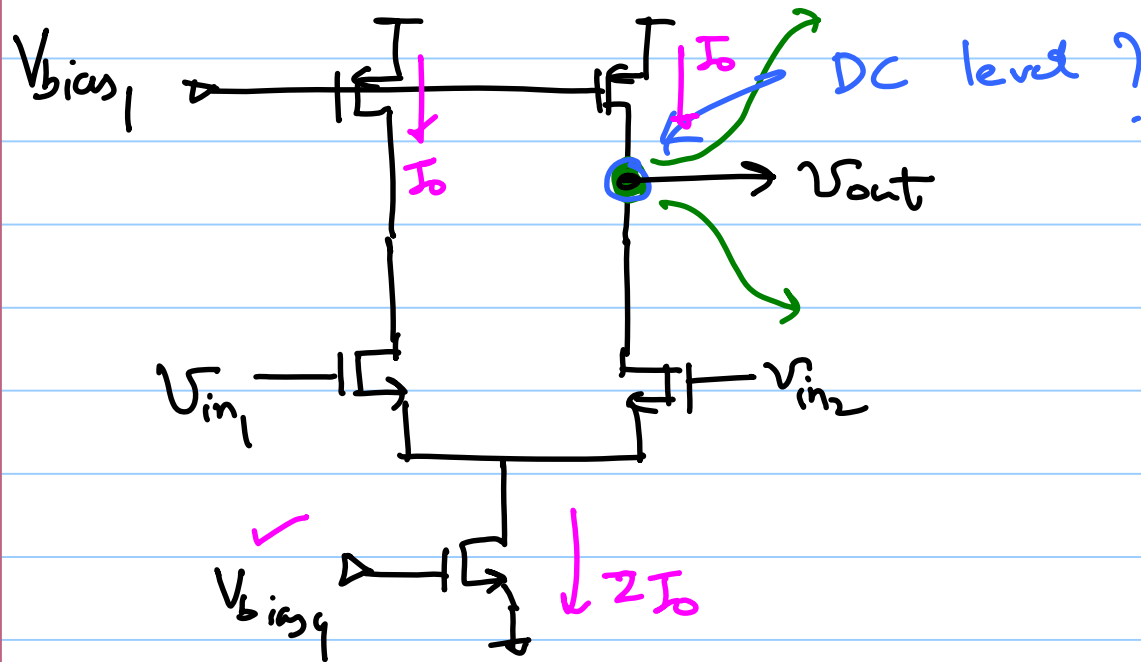
$$\approx \frac{1}{4} g_m r_o$$

if $r_{op} = r_{on} = r_o$

differential gain $\Rightarrow g_{m_n} (r_{op} || r_{on})$

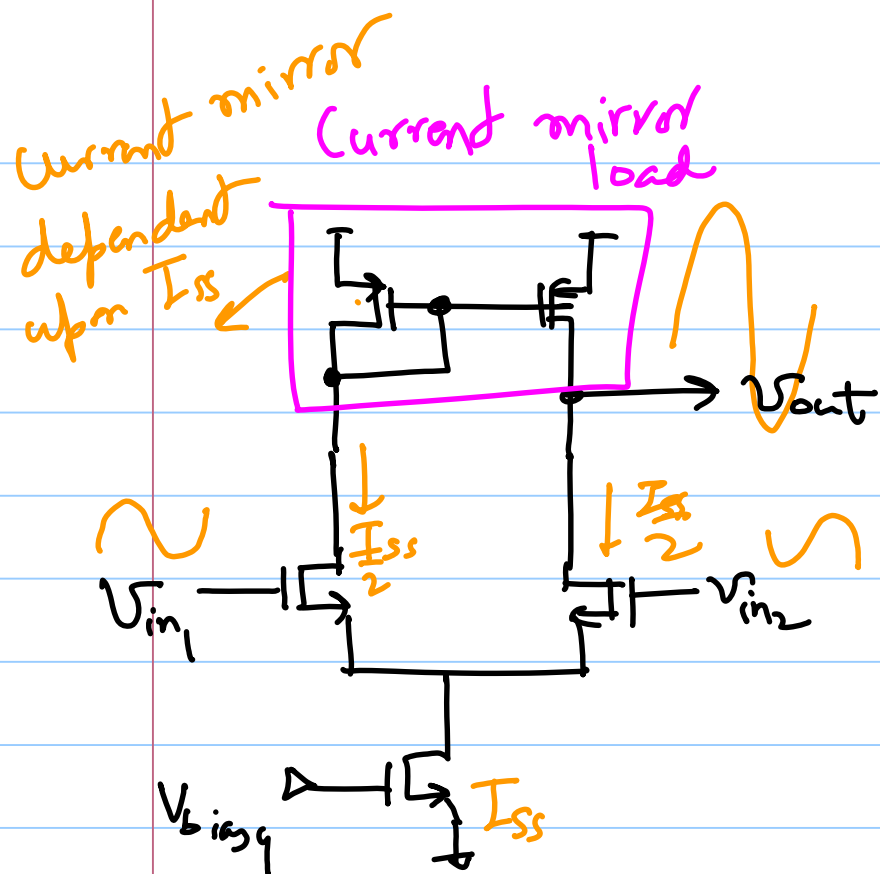
"higher gain"



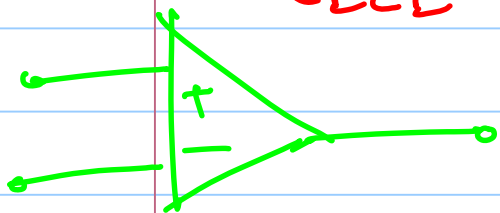


Not biased properly
 ↳ 2 independent current sources fighting

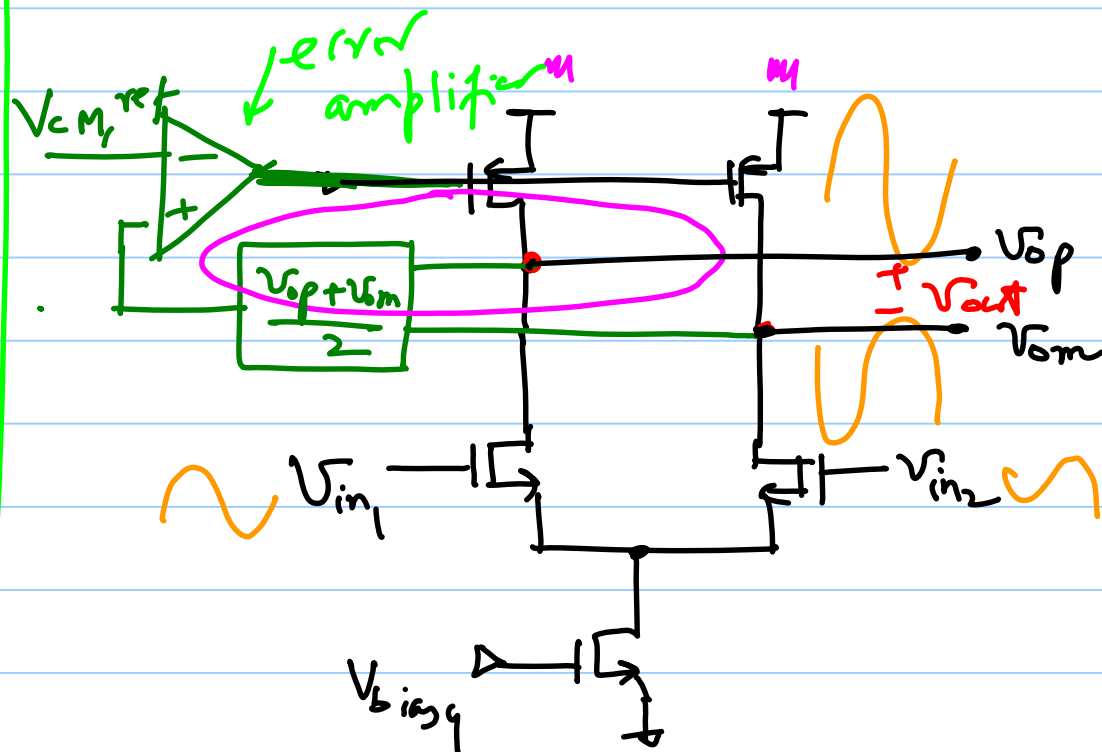
Solution: Make one of the current sources dependent on another



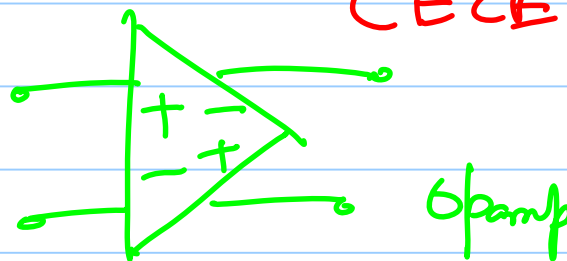
Single-ended o/p
(ECE 5/411)



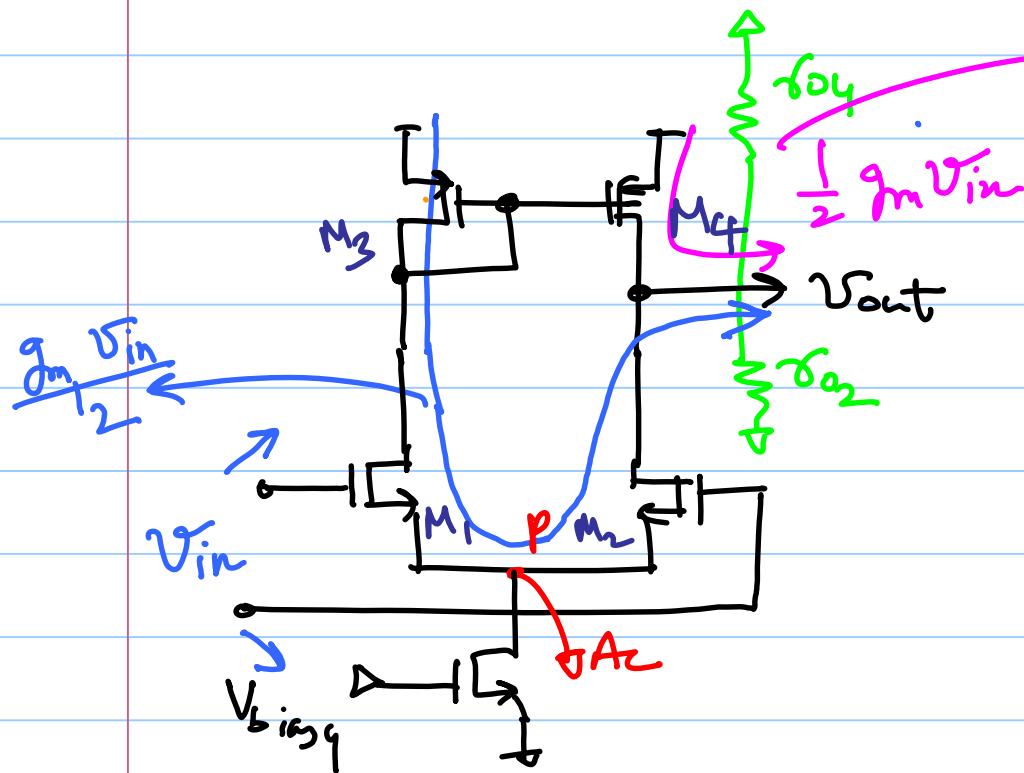
fully-differential amplifier



Common-mode feedback loop
(ECE 614)



Current Mirror load

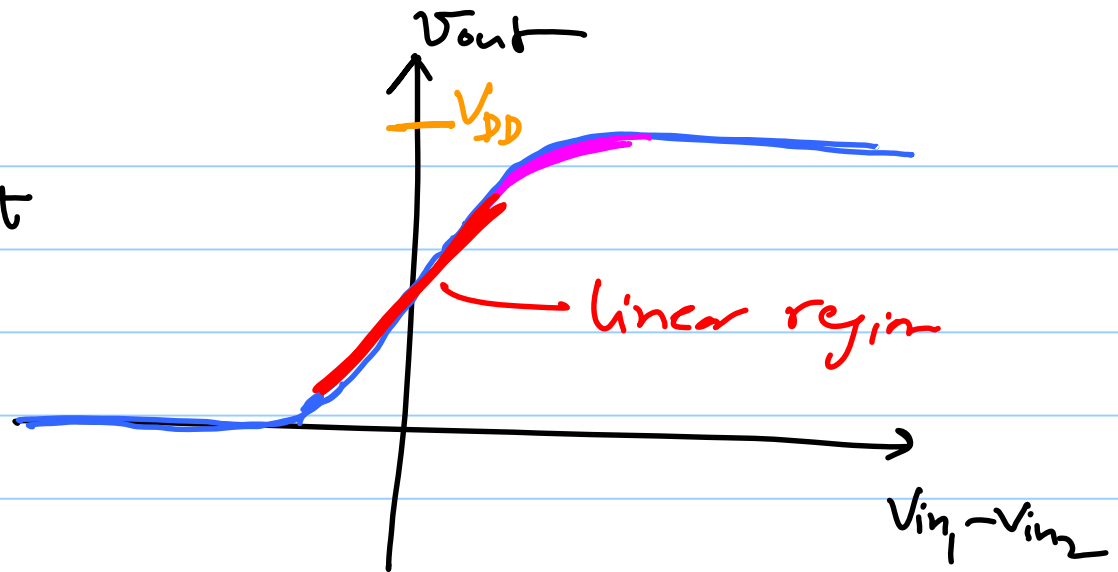
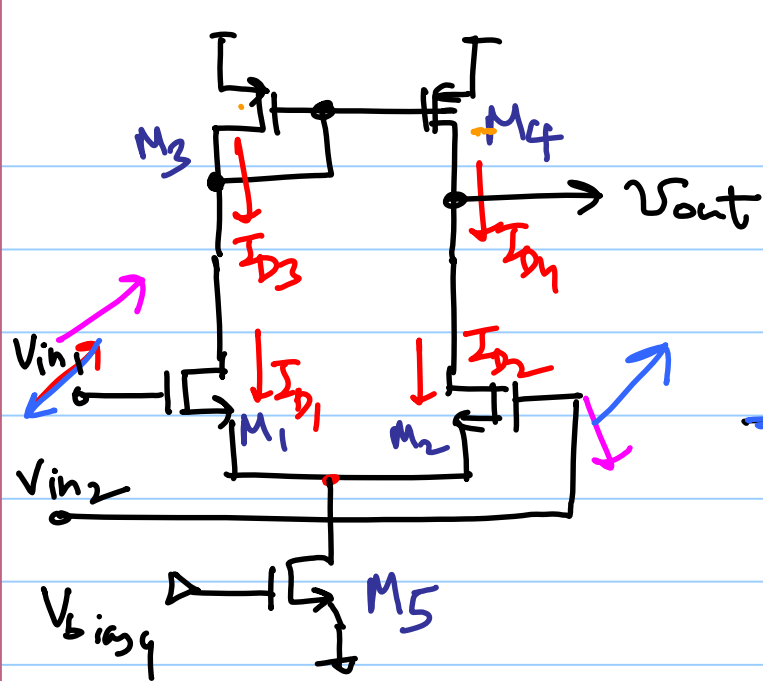


Current mirror also contributes to the output.

total current flowing into V_{out}
 $= g_{m1} V_{in}$

$$V_{out} = g_{m1} V_{in} (r_{o2} \parallel r_{o4})$$

$$A_{v,PM} = + g_{m1} (r_{o2} \parallel r_{o4})$$



① V_{in1} is more negative than V_{in2}

M_1 - off, M_3 & M_4 are off too

M_2 & M_5 are in deep triode $\Rightarrow V_{out} = 0$

② as V_{in1} approaches V_{in2} , M_1 turns on, drawing part of I_{SS} , M_3 & M_4 turn on

③ as V_{in1} gets more positive than V_{in2} ,

I_{D1} , I_{D3} & I_{D4} increase

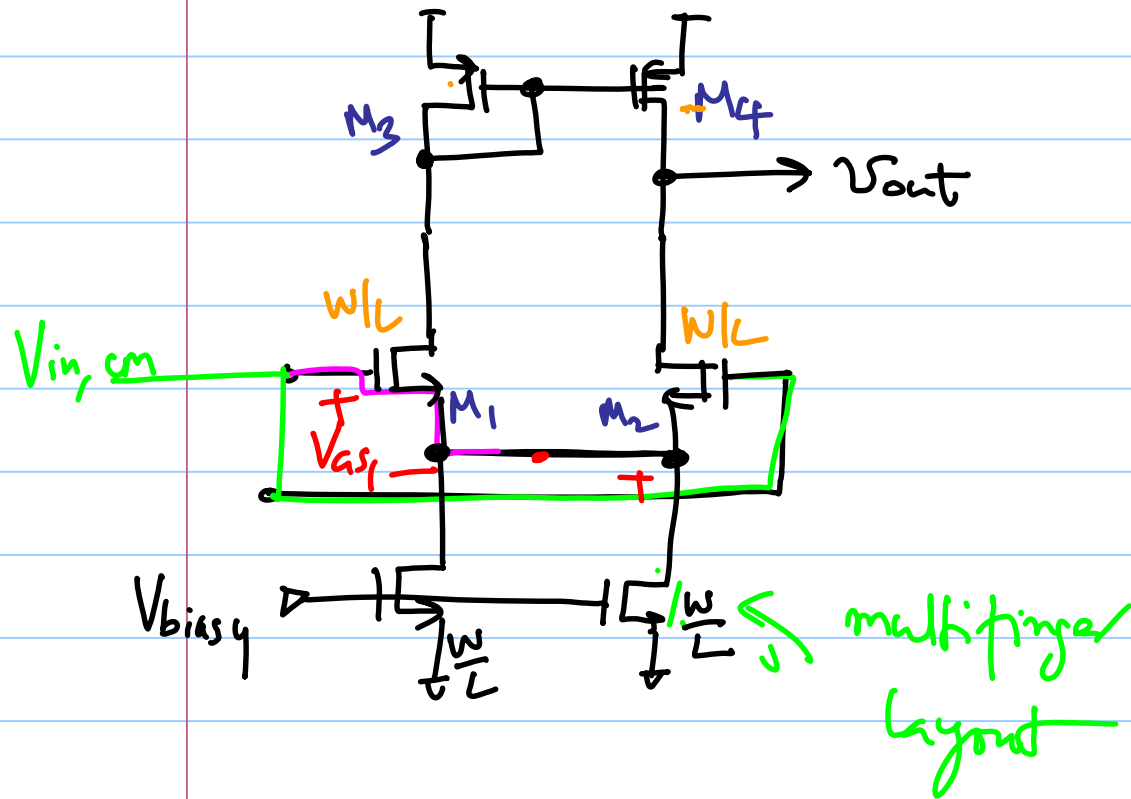
$I_{D2} \downarrow$

$\rightarrow$ drives M_4 into triode

$\hookrightarrow$ finally M_2 shuts off & M_4
operates in deep triode with

$$V_{out} = V_{DD}$$

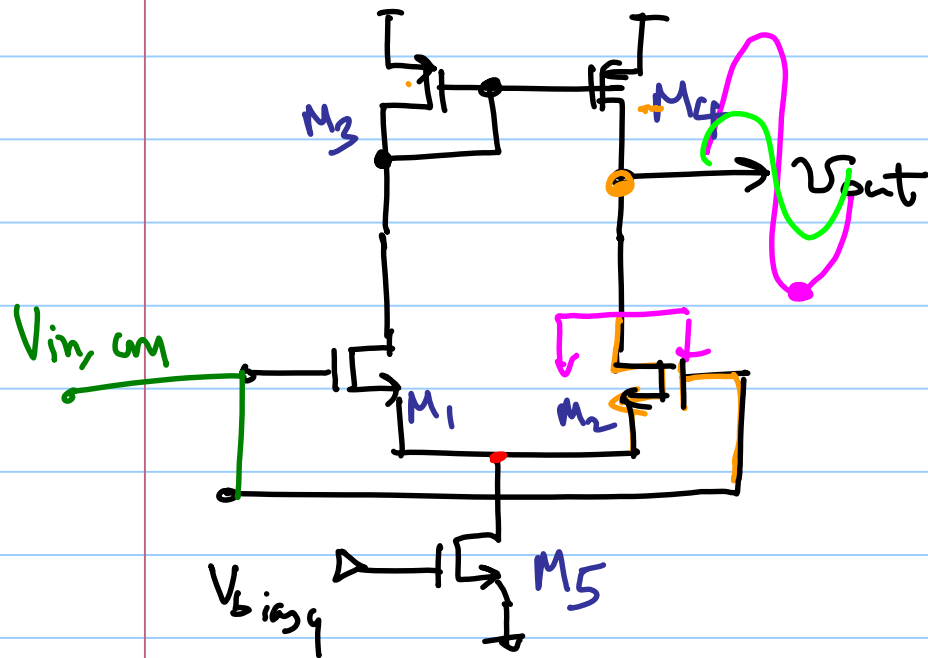
Input common-mode range



$$V_{in,cm} \geq V_{GS1,2} + V_{DS,sat5}$$

to keep $M_{1,2}$ & M_5 in SAT.

What about the output



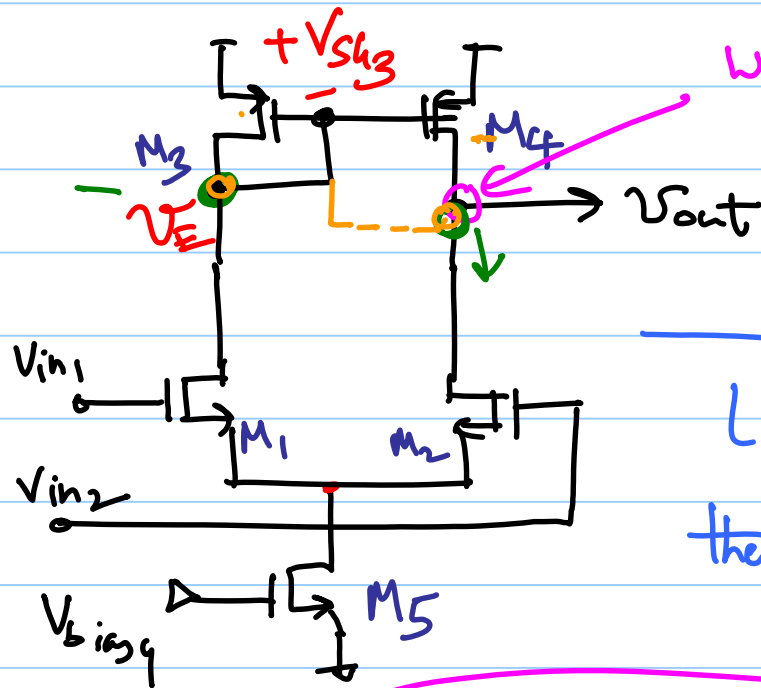
to keep M_2 in SAT

$$V_{DS} \geq V_{GS} - V_{THN}$$

$$V_D - V_S \geq V_G - V_S - V_{THN}$$

$$V_{out} \geq V_{in,cm} - V_{THN}$$

$$V_{in,cm} \leq V_{out} + V_{THN}$$



What is the DC level here?? $\approx V_{bias4}$

With perfect symmetry

$$V_{out} = V_E = V_{DD} - V_{SG3}$$

Let $V_{out} < V_E$

then M_1 must carry higher current than $M_2 \Rightarrow (I_{D1} > I_{D2})$

Should also be true that

$$(I_{D4} > I_{D3}) \rightarrow \textcircled{2}$$

But

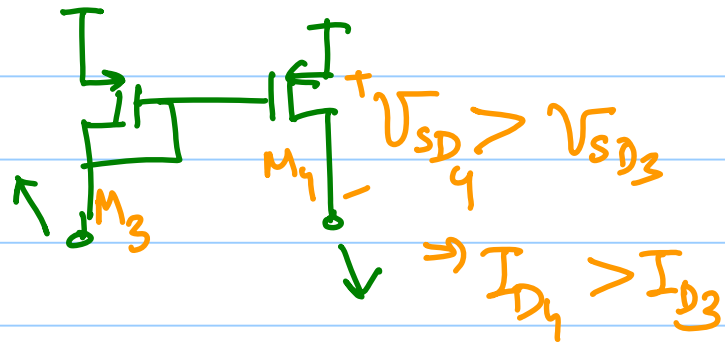
$$I_{D1} > \frac{I_{SS}}{2} \Rightarrow I_{D3} > \frac{I_{SS}}{2}$$

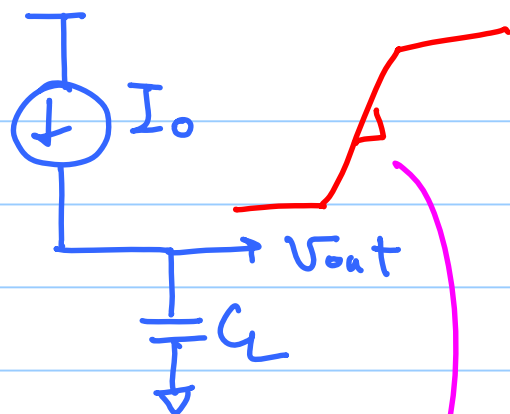
$$\Rightarrow I_{D4} < \frac{I_{SS}}{2}$$

contradiction

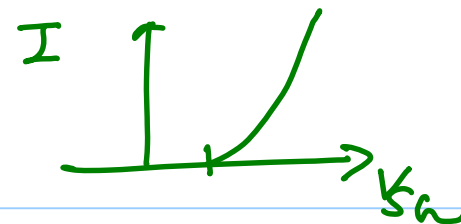
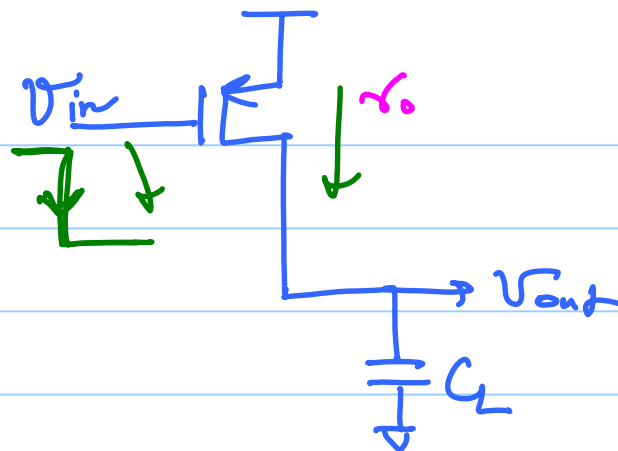
Contradicts with $\textcircled{2}$

$$I_{D1} = I_{D2} \quad + \quad V_{GS1} = V_{GS2} = V_{DD} - V_{SG3}$$

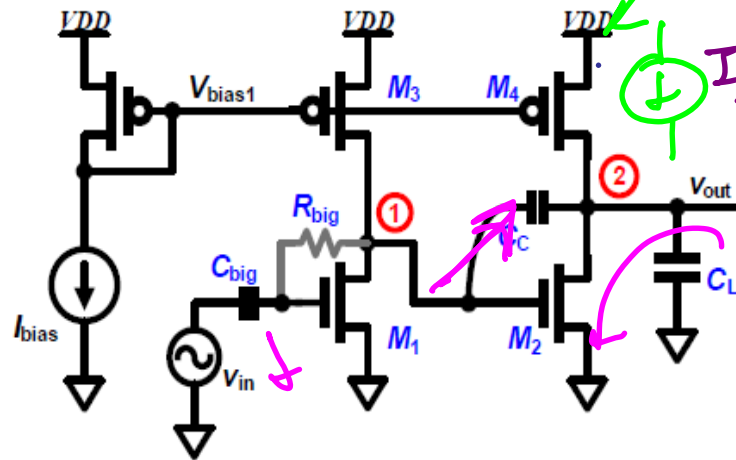




$$\frac{dV_{out}}{dt} = \frac{I_o}{C_L} \text{ "Slew"} "$$



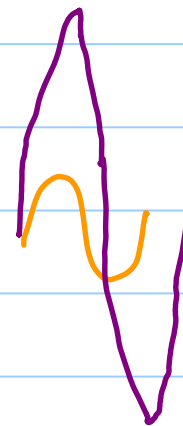
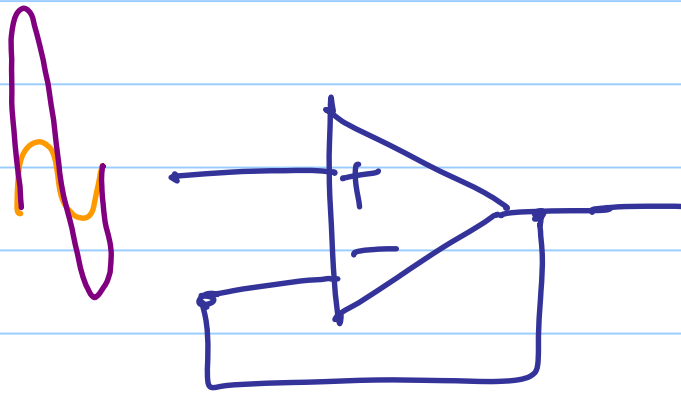
charging
 slew rate limited by
 M_4 current
 source

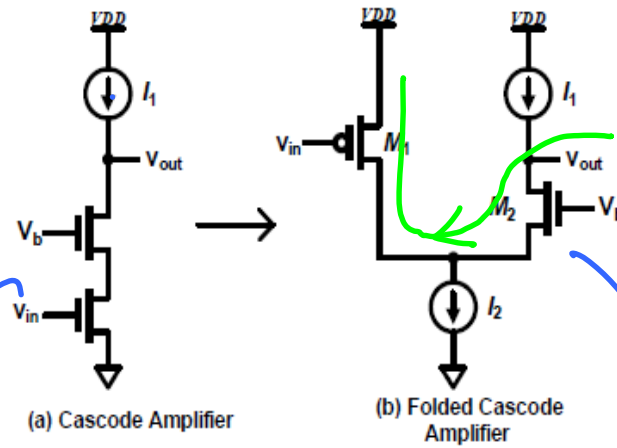


$$\frac{I_{D4}}{C_L}$$

no slew-rate
 limitation while
 discharging.

$$\frac{dV_{out}}{dt} > I_{D2}$$





$$g_m = g_{m1}$$

$$R_{out} = g_{m2} r_{o2} r_{o1}$$

$$= -g_{m1} (g_{m2} r_{o2} r_{o1})$$

(a) (10 points) Find the small-signal gain of the folded-cascode amplifier (b) shown above, and compare it with the gain of the cascode amplifier (a). Assume that the current sources are ideal.

$$A_v = -g_{m1} (g_{m2} r_{o2} r_{o1})$$