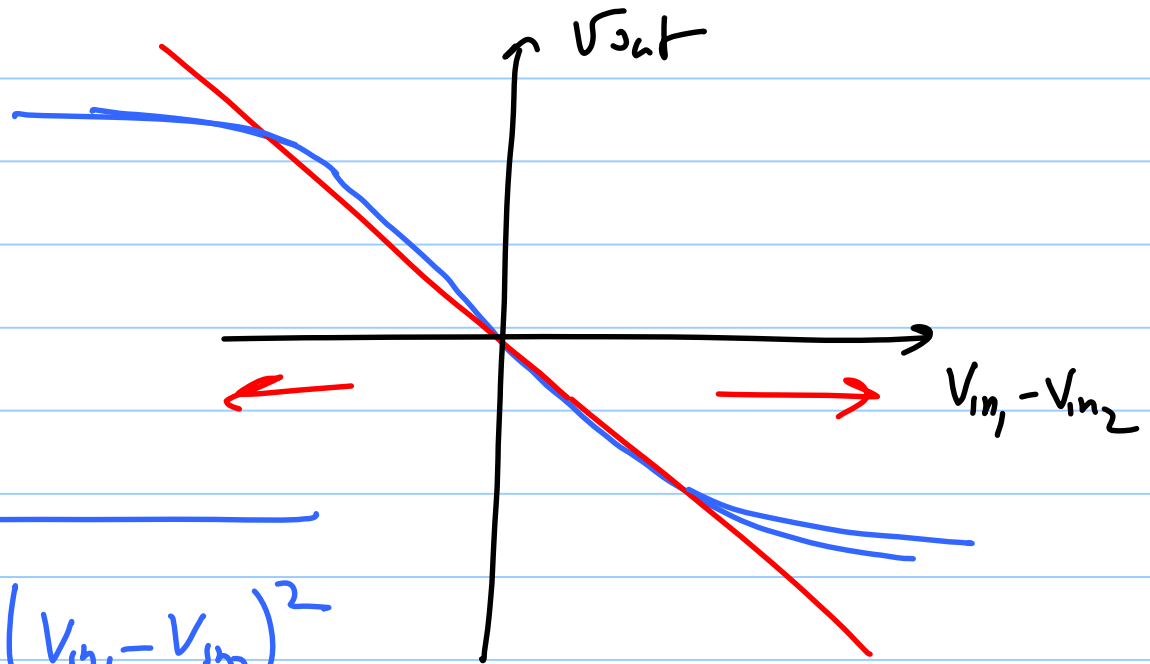


ECE 511 - Lecture 21

Note Title

4/7/2015



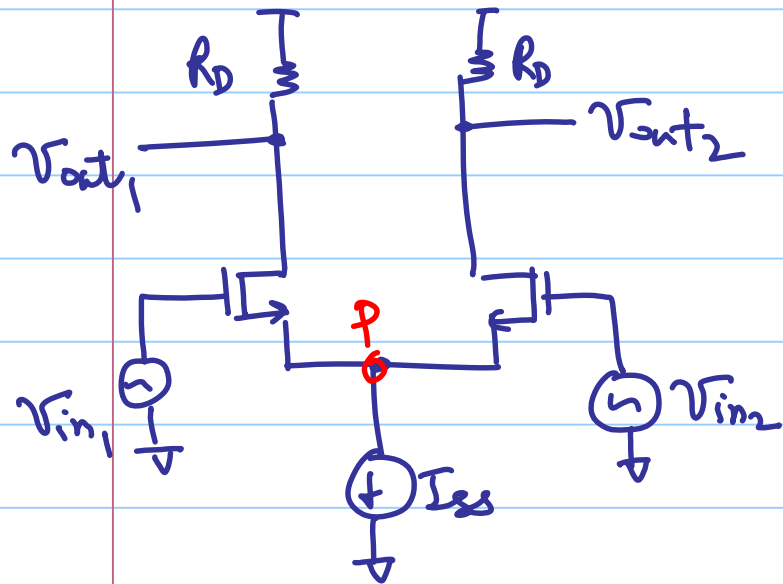
$$I_{D1} - I_{D2} = \frac{\beta}{2} \underbrace{(V_{in1} - V_{in2})}_{V_{in}} \sqrt{\frac{4I_{SS}}{\beta} - \underbrace{(V_{in1} - V_{in2})^2}_{V_{in}^2}}$$

for linearity

$\frac{I_{SS}}{\beta} \uparrow$

compressive
non linearity

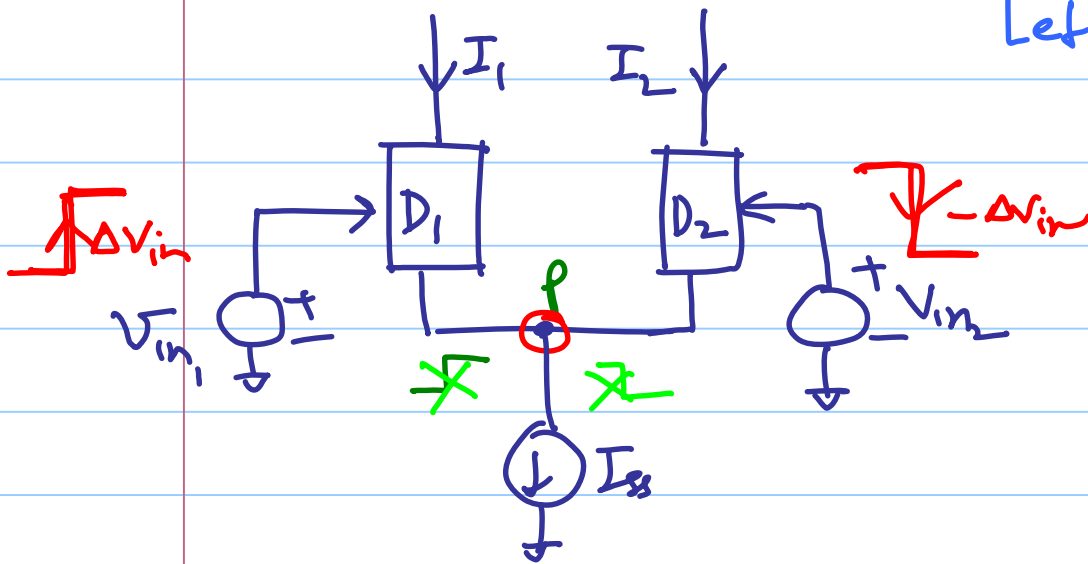
Small-signal Analysis



Lemma:

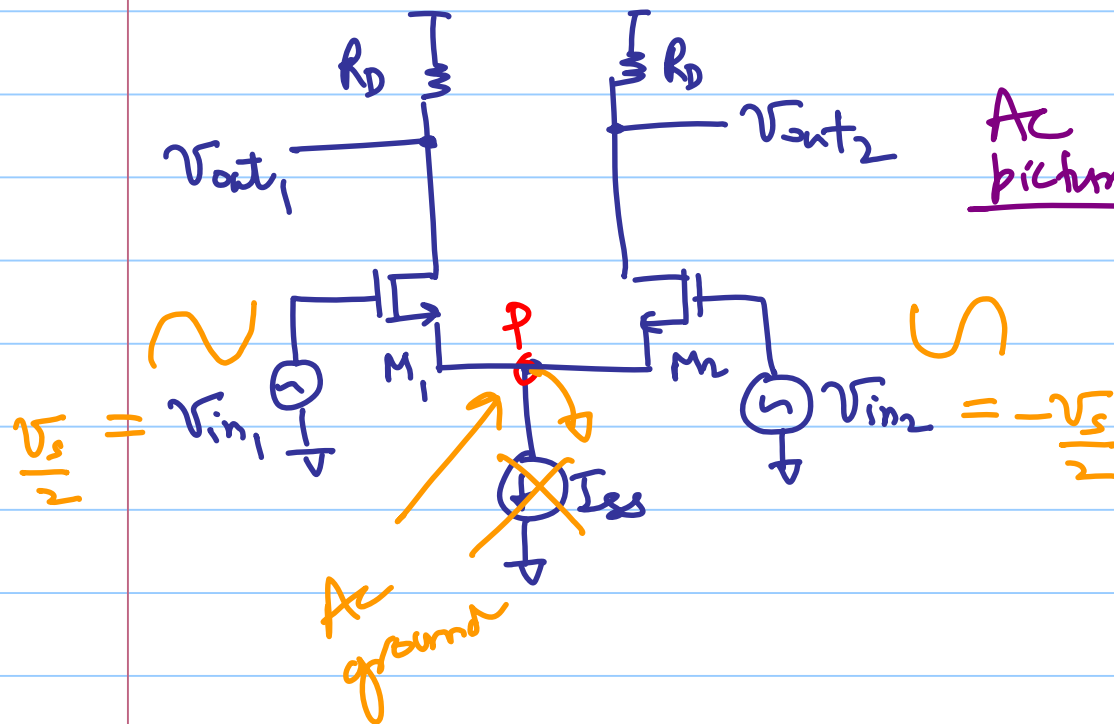
Consider the "symmetric circuit" shown below where D_1 and D_2 are any 3-terminal devices

Let V_{in_1} change from V_0 to $V_0 + \Delta V_{in}$
 V_{in_2} " " " V_0 to $V_0 - \Delta V_{in}$

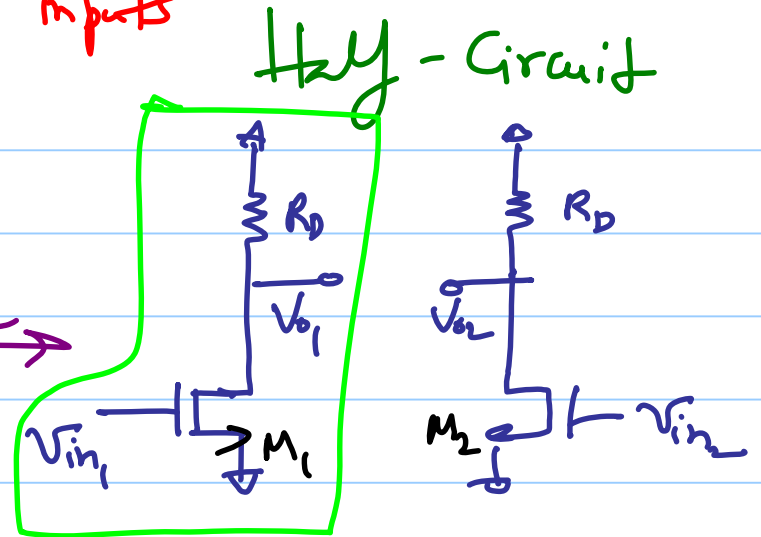


Then if, circuit remains "linear", " V_p doesn't change".

V_{in1} & V_{in2} are differential inputs

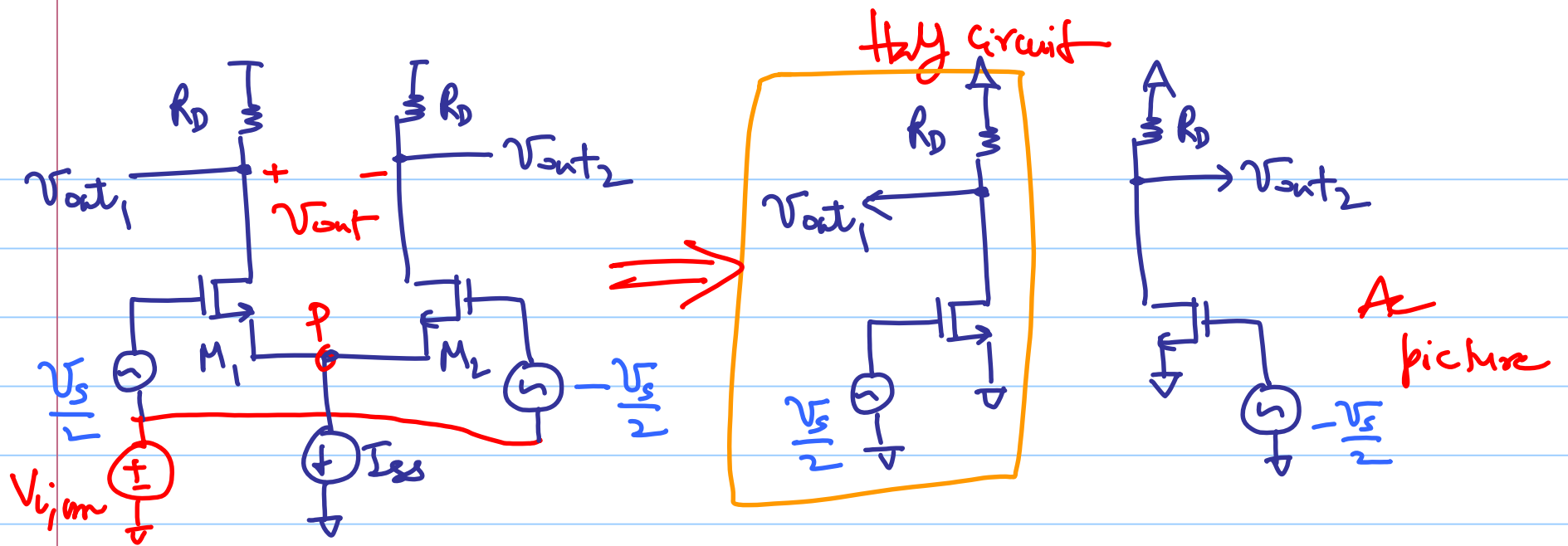


AC picture →



Linearity $\Rightarrow$ signals are "small"

* Half Circuit (small-signal) Analysis



$$v_{out1} = -g_m (r_o \parallel R_D) \cdot \frac{v_s}{2}$$

$$v_{out2} = +g_m (r_o \parallel R_D) \cdot \left(\frac{+v_s}{2}\right)$$

Diff.
o/p $\Rightarrow$

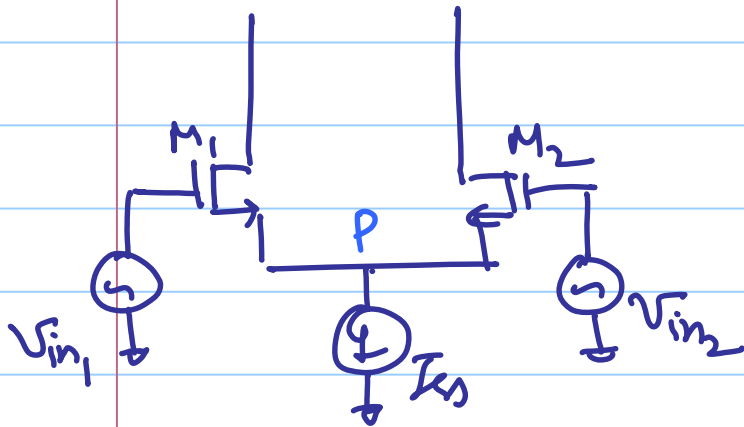
$$(v_{out1} - v_{out2}) = \frac{-g_m (r_o \parallel R_D) \cdot v_s}{2} - \frac{g_m (r_o \parallel R_D) \cdot v_s}{2}$$

$$= -g_m (r_o \parallel R_D) \cdot v_s$$

$$\Rightarrow \frac{v_{out1} - v_{out2}}{v_s} = -g_m (r_o \parallel R_D)$$

$$v_s \triangleq v_{in1} - v_{in2}$$

* What if the inputs are not fully-differential, but
Single-ended

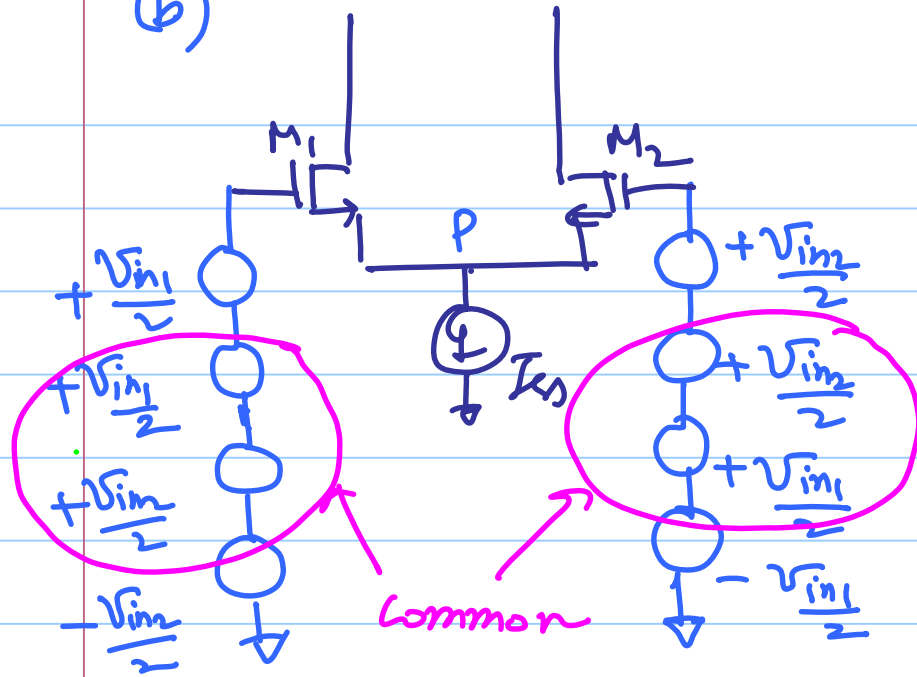


$$V_{in1} = \underbrace{\left(\frac{V_{in1} - V_{in2}}{2} \right)}_{v_{s/2}} + \left(\frac{V_{in1} + V_{in2}}{2} \right)$$

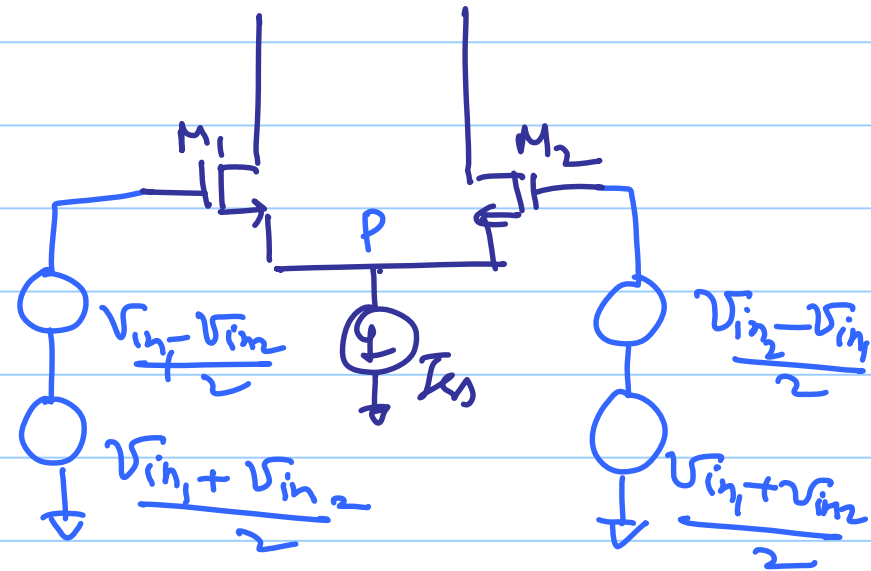
$$V_{in2} = \underbrace{\left(\frac{V_{in2} - V_{in1}}{2} \right)}_{-v_{s/2}} + \left(\frac{V_{in1} + V_{in2}}{2} \right)$$

Common v_c
Many Not bc DC

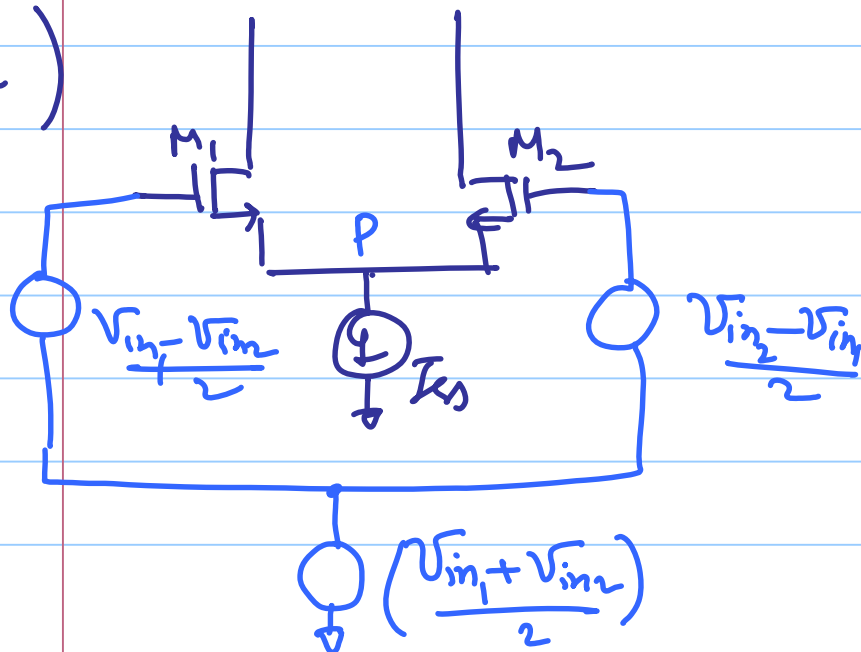
(b)

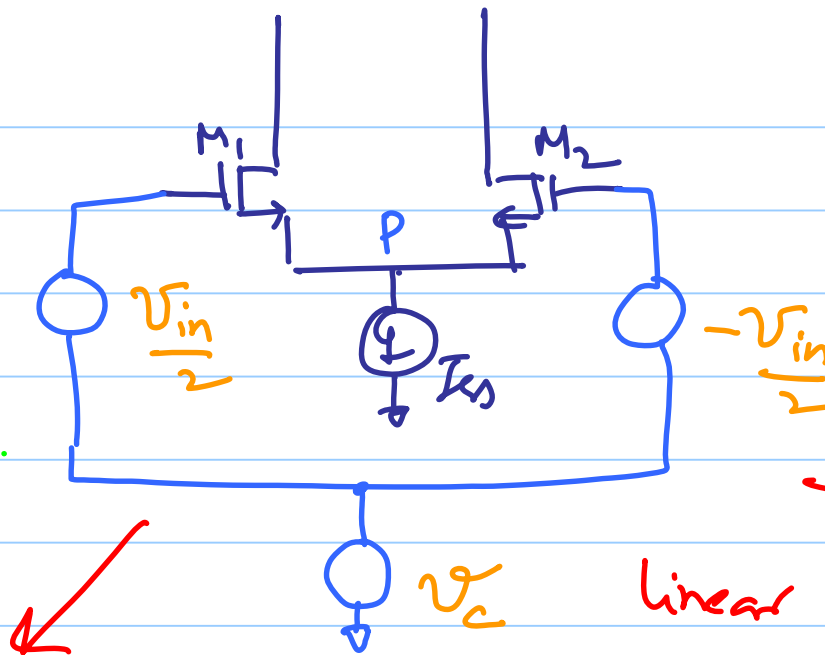


(c)



(d)



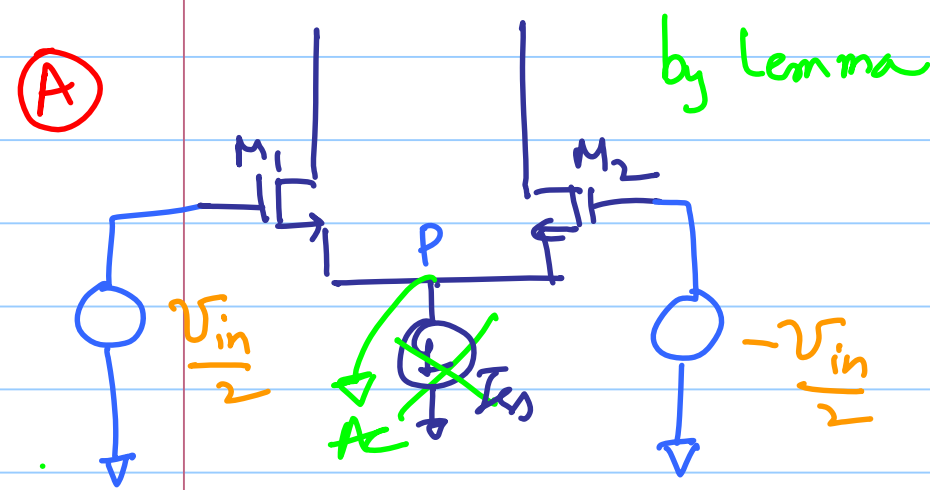


$$v_{in} = v_{in1} - v_{in2}$$

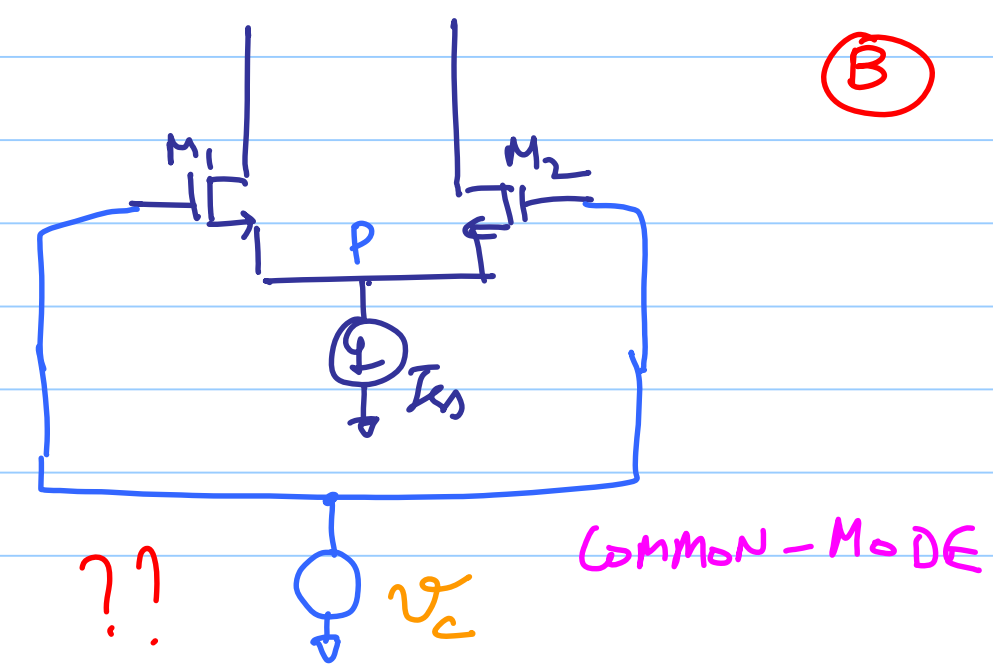
$$v_c = \left(\frac{v_{in1} + v_{in2}}{2} \right)$$

average of the 2 inputs $\Rightarrow$ Common-mode signal

Linear Superposition

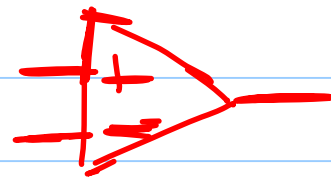
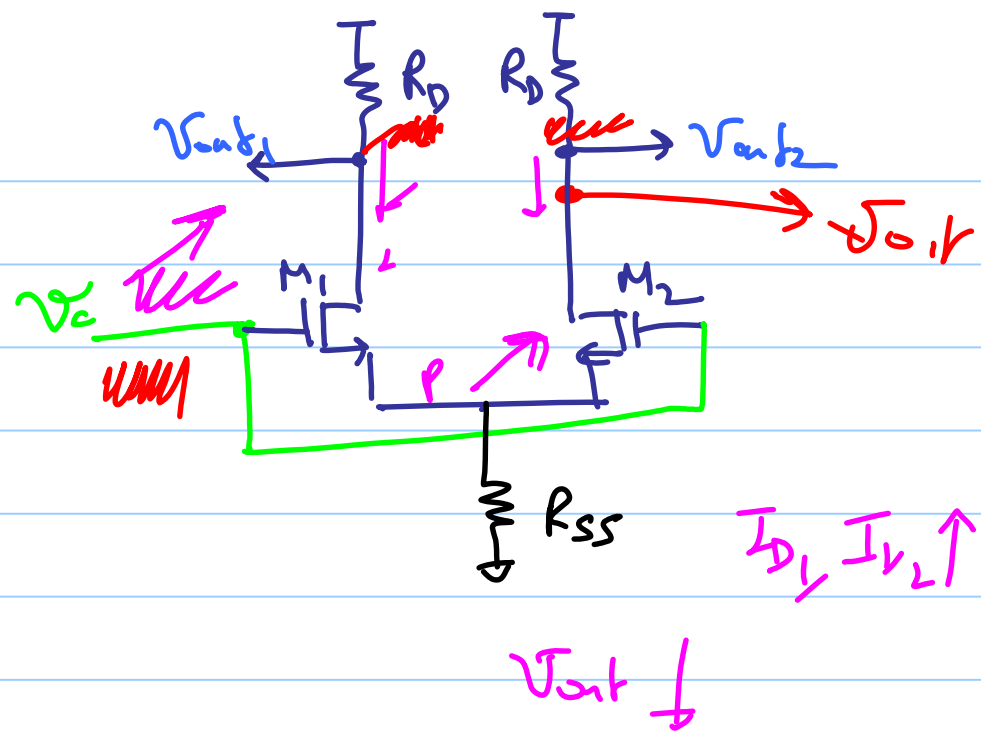
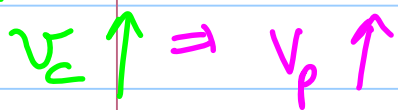


DIFFERENTIAL
(Half Circuit Analysis)

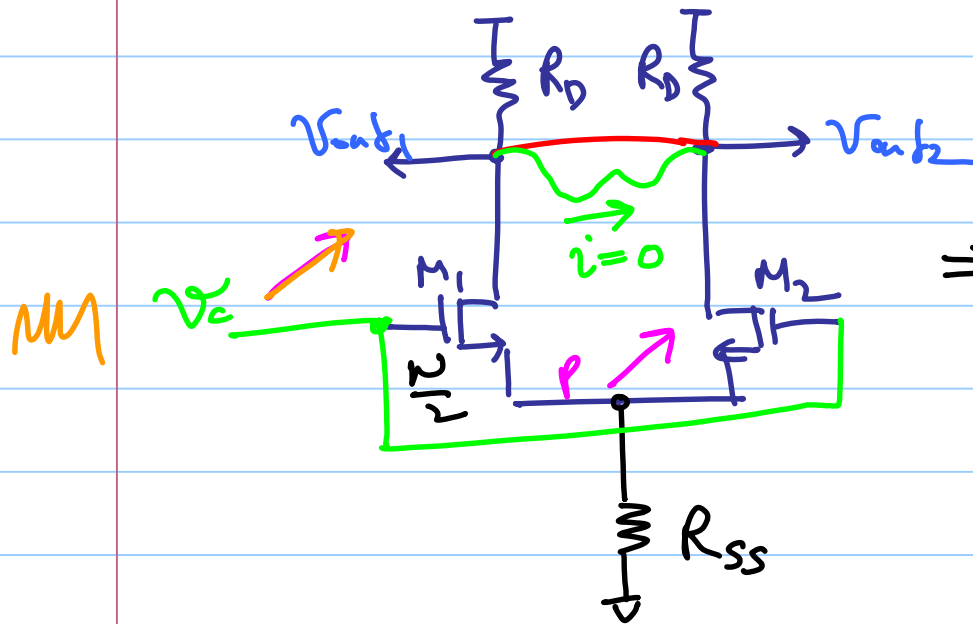


Common Mode Response of Diff-pair

- * Diffamp should ideally suppress the effect of CM disturbances, including a CM input (v_c)
- * In reality the tail current source is not ideal
 - ↳ finite output resistance
 - ↳ CM variations at the output

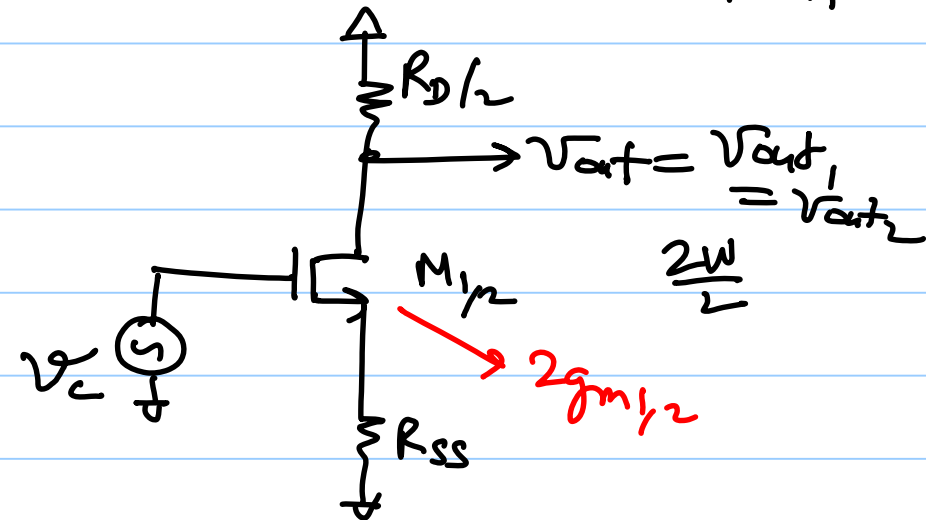


Common - Mode Equivalent Circuit



$\Rightarrow$

CM-Equivalent (Ac) circuit

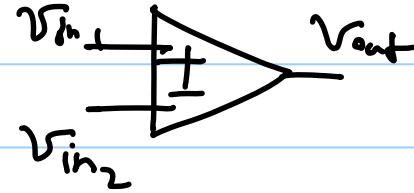
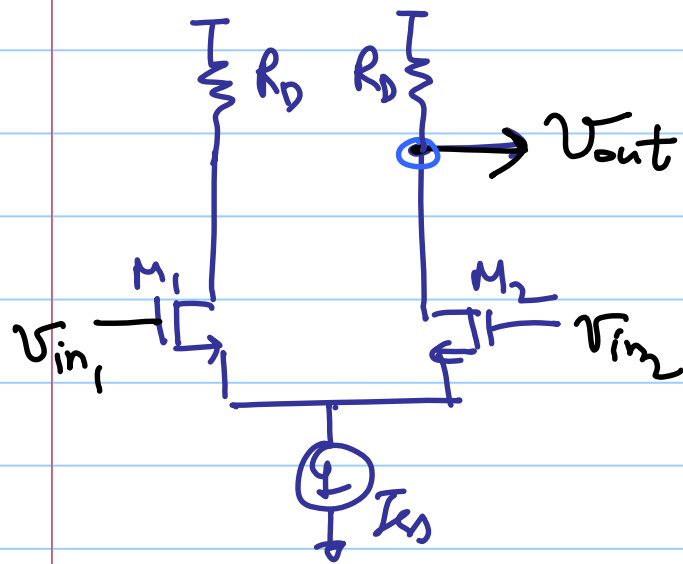


Common mode small-signal gain $= A_{cm} = \frac{V_{out}}{V_c} = - \frac{R_D/2}{\frac{1}{(2g_m)} + R_{ss}}$

We want $|A_{cm}| \rightarrow 0$
 $\Rightarrow R_{ss} \rightarrow \infty$

$\lambda=0, \delta=0$

Let's say we have single-ended output



$$V_{out} = V_{out2} = A_{v,DM} \cdot (V_{in1} - V_{in2}) + A_{v,CM} \cdot \left(\frac{V_{in1} + V_{in2}}{2} \right)$$

$$= A_{v,DM} \cdot V_{in} + A_{v,CM} \cdot V_c$$

$\nearrow$ DM gain
 $\nearrow$ CM gain

$$A_{v,DM} = -\frac{g_m R_D}{2}$$

$$A_{v,CM} = -\frac{R_D/2}{\left(\frac{1}{2g_m} \right) + R_{SS}}$$

We want $|A_{v,DM}| \uparrow$ & $|A_{v,cm}| \rightarrow 0$

Common-mode rejection ratio

$$C_{MRR} = \left| \frac{A_{v,DM}}{A_{v,cm}} \right|$$

ideally $C_{MRR} \rightarrow \infty$

Expressed in
dB

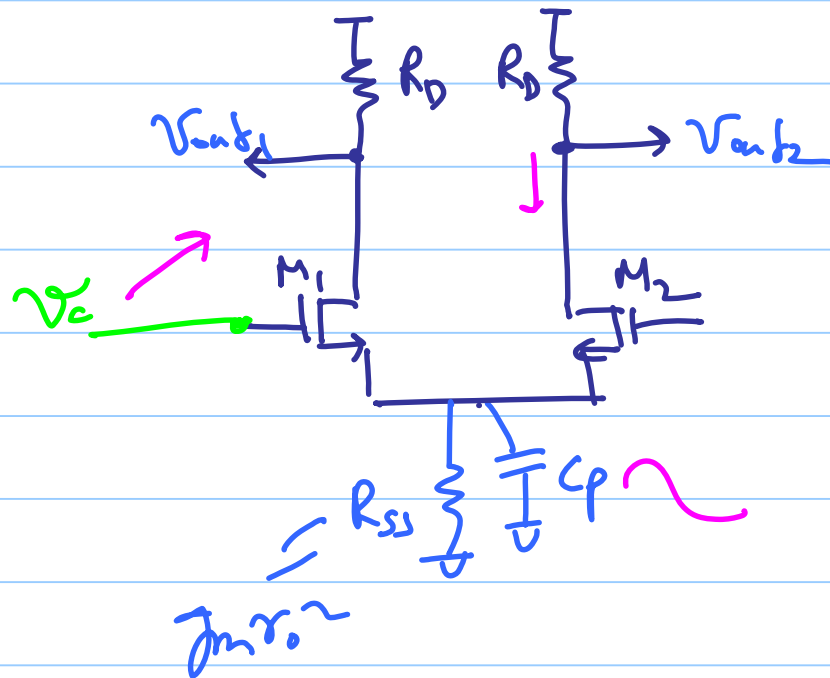
$$20 \log_{10} \left| \frac{A_{v,DM}}{A_{v,cm}} \right|$$

CMRR for the above diff pair

$$C_{MRR} = \frac{\frac{g_m R_D}{2}}{\frac{g_m R_D}{1 + 2 g_m R_{SS}}} = \frac{1}{2} + g_m R_{SS}$$

mismatch b/w M_1, M_2 limits CM reject

$$CMRR = \frac{g_m}{\Delta g_m} (1 + 2g_m R_{ss})$$



$$\left| \frac{1}{j\omega C_p} \right| \approx R_{ss}$$