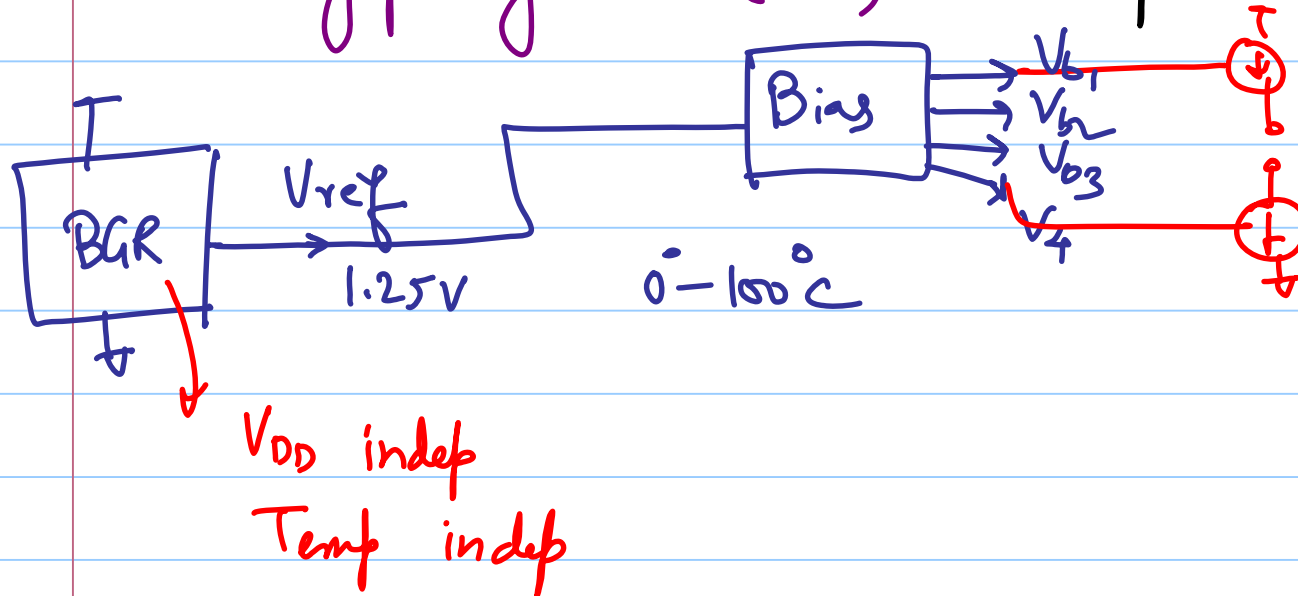


ECE 511 - Lecture 27

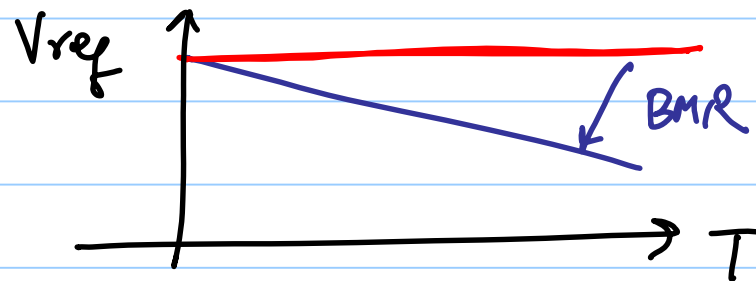
Note Title

5/6/2014

Bandgap Reference (BGR) $\rightarrow$ Temp Independent reference



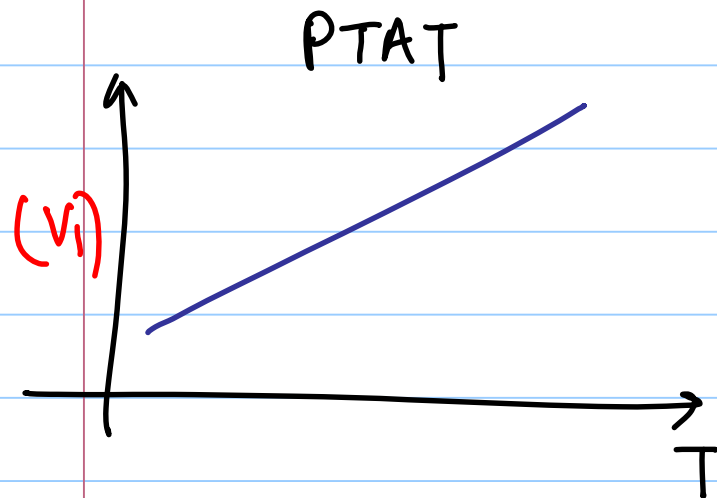
Temperature Coefficient (TempCo)



$$TempCo = \left(\frac{\partial V_{ref}}{\partial T} \right) \cdot \frac{1}{V_{ref}}$$

↓
zero

Zero Temp Coeff (ZTC)

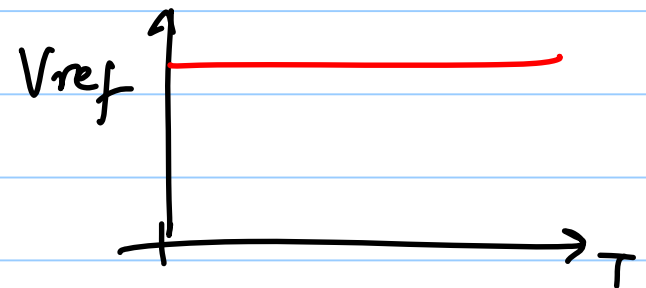
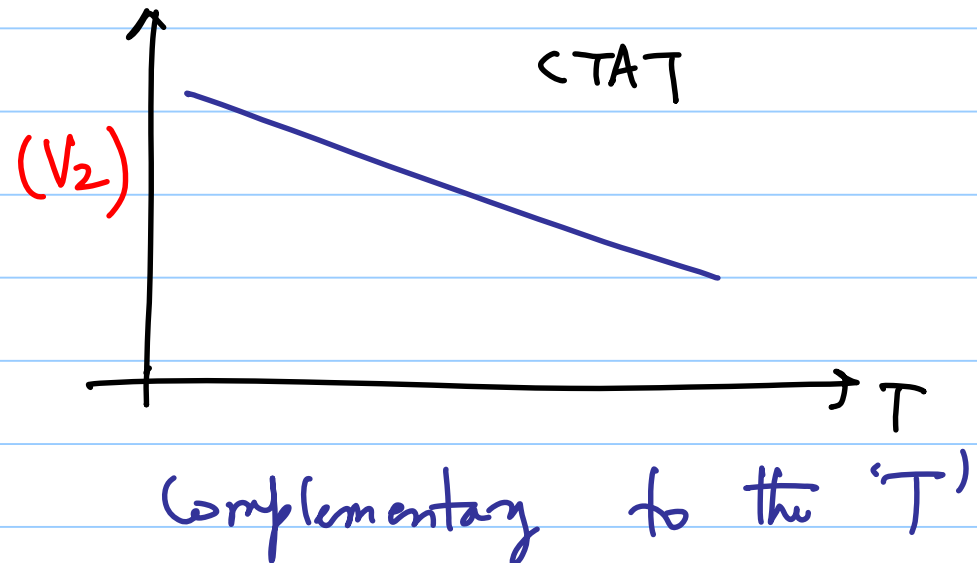


proportional to absolute
Temp.

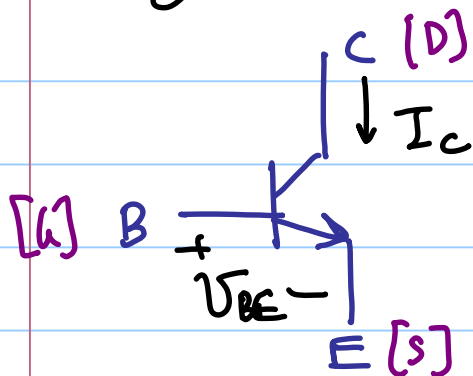
Combine PTAT & CTAT

$$V_{ref} = \alpha_1 V_1 + \alpha_2 V_2$$

$$\frac{\partial V_{ref}}{\partial T} = \alpha_1 \left(\frac{\partial V_1}{\partial T} \right) + \alpha_2 \left(\frac{\partial V_2}{\partial T} \right) = 0 \quad \text{"ZTC"}$$



① Negative Temp Co (CTAT)



$$I_C = I_S e^{\frac{V_{BE}}{V_T}} \quad \text{--- ①}$$

$$V_T = \frac{kT}{q}$$

26 mV @ 27°C

$$I_S \propto \mu k T \cdot n_i^2 \rightarrow n_i^2 \propto T^3 \cdot e^{-\frac{E_g}{kT}} \rightarrow E_g \text{ is the Bandgap energy}$$

Si → 1.12 eV

$$\mu \propto T^m, m = -\frac{3}{2}$$

$$I_S = b \cdot T^{(4+m)} \cdot e^{-E_g/kT} \quad \text{--- ②}$$

from ①:

$$V_{BE} = V_T \ln \left(\frac{I_C}{I_S} \right)$$

Compute Temp Co V_{BE} for fixed I_C

$$\downarrow \frac{\partial V_{BE}}{\partial T} = \frac{\partial V_T}{\partial T} \times \ln\left(\frac{I_c}{I_s}\right) - \underbrace{\frac{V_T}{I_s} \cdot \frac{\partial I_s}{\partial T}}_{\text{}} \longrightarrow (3)$$

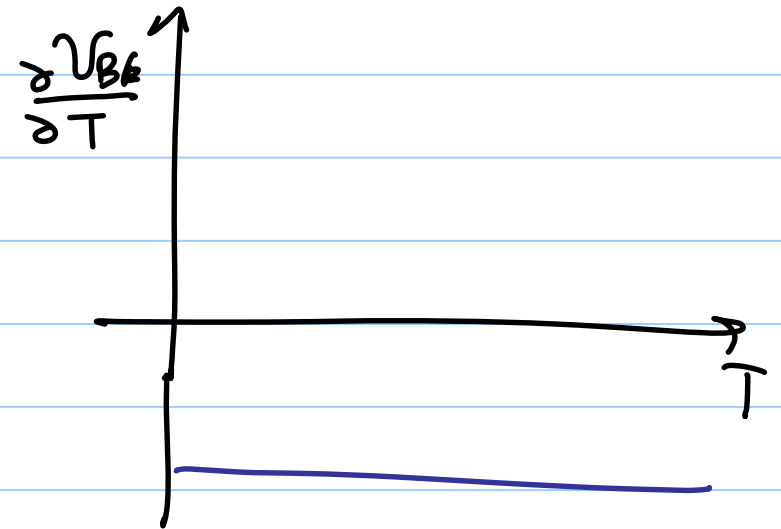
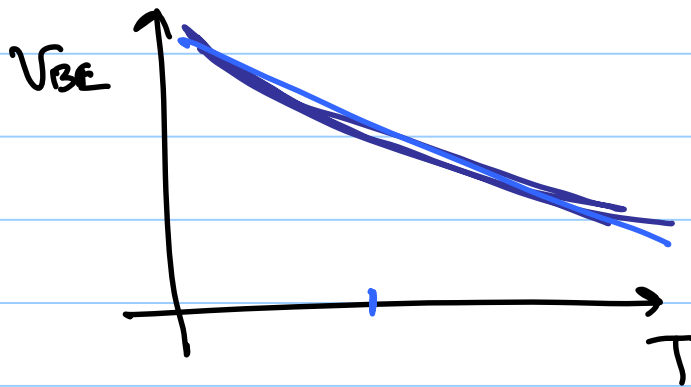
from (2)

$$\begin{aligned} \frac{\partial I_s}{\partial T} &= b(4+m) T^{3+m} e^{-E_g/kT} + b T^{4+m} e^{-E_g/kT} \cdot \frac{E_g}{kT^2} \\ &= \frac{(4+m)}{T} \underbrace{b T^{4+m} e^{-E_g/kT}}_{I_s} + \underbrace{b T^{4+m} e^{-E_g/kT}}_{I_s} \cdot \frac{E_g}{kT^2} \\ &= \frac{(4+m)}{T} I_s + I_s \cdot \frac{E_g}{kT^2} \end{aligned}$$

$$\Rightarrow \frac{V_T}{I_s} \cdot \frac{\partial I_s}{\partial T} = (4+m) \frac{V_T}{T} + \frac{E_g}{kT^2} V_T \longrightarrow (4)$$

plug (4) into (3)

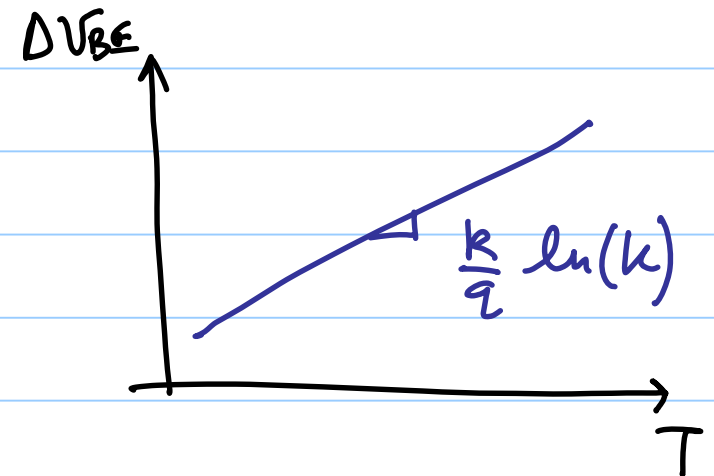
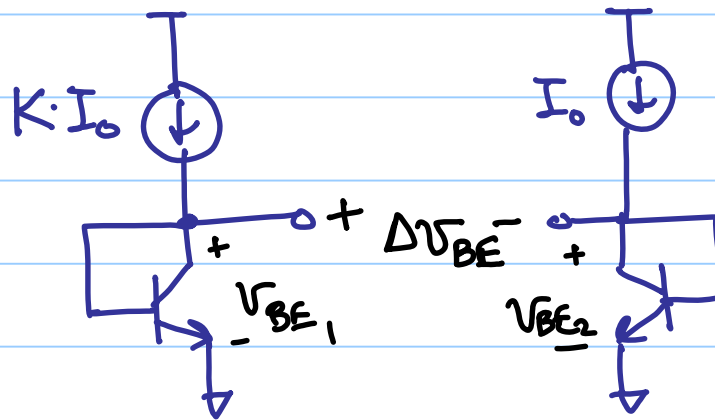
$$\frac{\partial V_{BE}}{\partial T} = \frac{V_{BE} - (4+m) V_T - E_g/2}{T}$$



' V_{BE} itself is a CTAT'

* Since $\frac{\partial V_{BE}}{\partial T}$ itself depends on V_{BE} & T
 $\rightarrow$ not a linear CTAT

② Positive TempCo (PTAT)



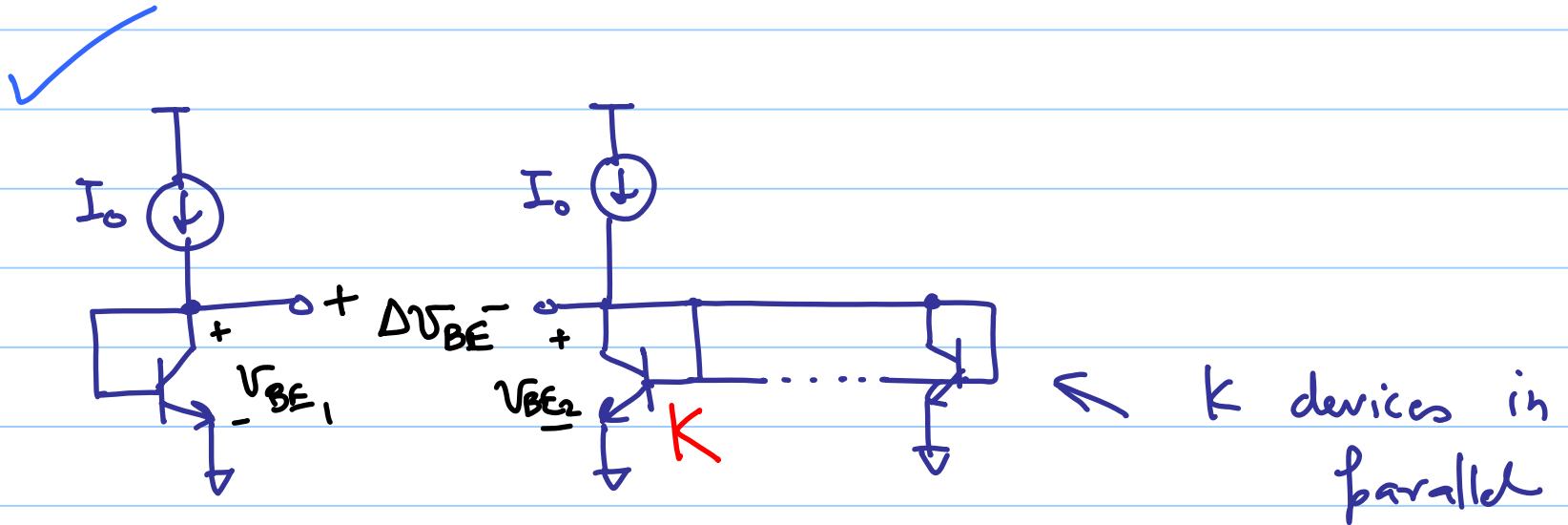
$$\Delta V_{BE} = V_{BE1} - V_{BE2}$$

$$= V_T \ln\left(\frac{K I_0}{I_S}\right) - V_T \ln\left(\frac{I_0}{I_S}\right) \quad , \quad \underbrace{I_{S1} = I_{S2}}$$

$$= V_T \ln\left(\frac{K I_0}{I_S} \cdot \frac{I_S}{I_0}\right)$$

$$= V_T \ln K$$

$$\frac{\partial \Delta V_{BE}}{\partial T} = \left(\frac{k}{q}\right) \ln(k) > 0$$



$$\begin{aligned} \Delta V_{BE} &= V_T \ln\left(\frac{I_0}{I_S}\right) - V_T \ln\left(\frac{I_0/k}{I_S}\right) \\ &= V_T \ln k \end{aligned}$$

Need to design this

$$V_{ref} = \alpha_1 V_{BE} + \alpha_2 \Delta V_{BE} \rightarrow kT \ln(K)$$

CTAT PTAT

$$ZTC \Rightarrow \frac{\partial V_{ref}}{\partial T} = 0$$

$$\alpha_1 \cdot \left(\frac{\partial V_{BE}}{\partial T} \right) + \alpha_2 \left(\frac{k}{T} \ln K \right) = 0$$

$$\alpha_2 \ln(K) = - \frac{\alpha_1 \cdot \left(\frac{\partial V_{BE}}{\partial T} \right)}{(k/q)}$$

$-1.5 \text{ mV}/^\circ\text{K}$
 CTAT

$\frac{k}{T} = +0.087 \text{ mV}/^\circ\text{K}$
 PTAT

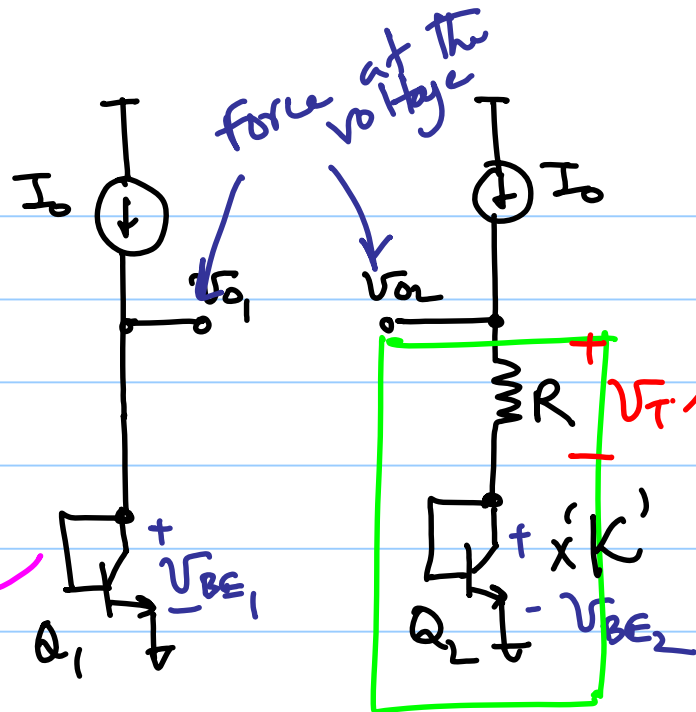
$$\alpha_2 \cdot \ln(K) = 17.2 \times \alpha_1$$

choose $\alpha_1 = 1$

$\alpha_2 \ln K = 17.2$

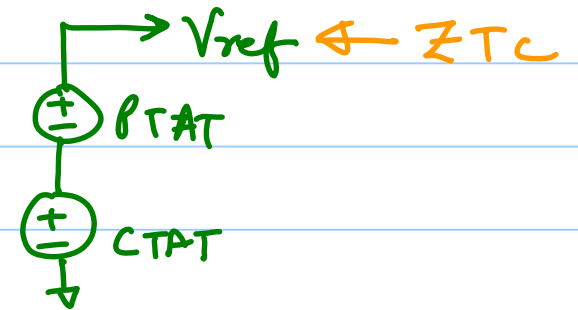
$V_{ref} = V_{BE} + 17.2 \times V_T$

Typical value
1.25 V



When $V_{O1} = V_{O2}$

$$IR = V_{BE1} - V_{BE2} = V_T \ln K$$



$V_T \ln K$ PTAT

CTAT

$$V_{O2} = IR + V_{BE2}$$

$$= V_{BE2} + V_T \ln K$$

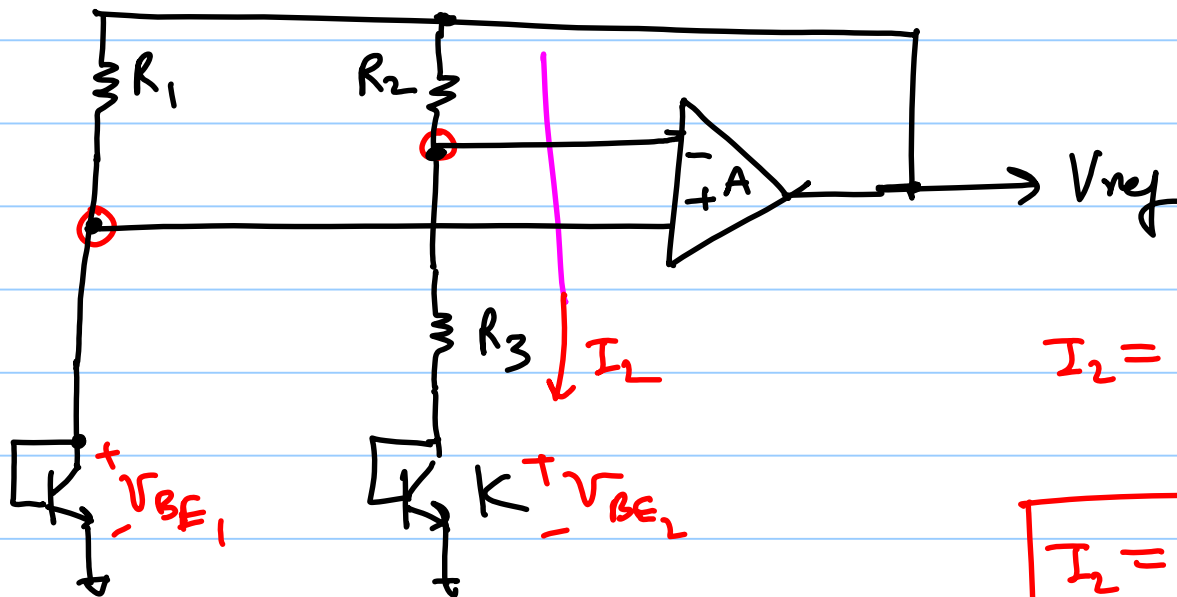
Note that $\alpha_1 = \alpha_2 = 1$

$$\frac{\partial V_{O2}}{\partial T} = 0 \Rightarrow$$

$$\ln K = 17.2 \Rightarrow K = e^{17.2}$$

$\Rightarrow$ We need a large $\alpha_2 > 1$

Example BGR:



$$I_2 = \frac{V_{BE1} - V_{BE2}}{R_3}$$

$$I_2 = \frac{V_T \ln K}{R_3}$$

$$V_{ref} = V_{BE2} + \left(\frac{V_T \ln K}{R_3} \right) (R_2 + R_3)$$

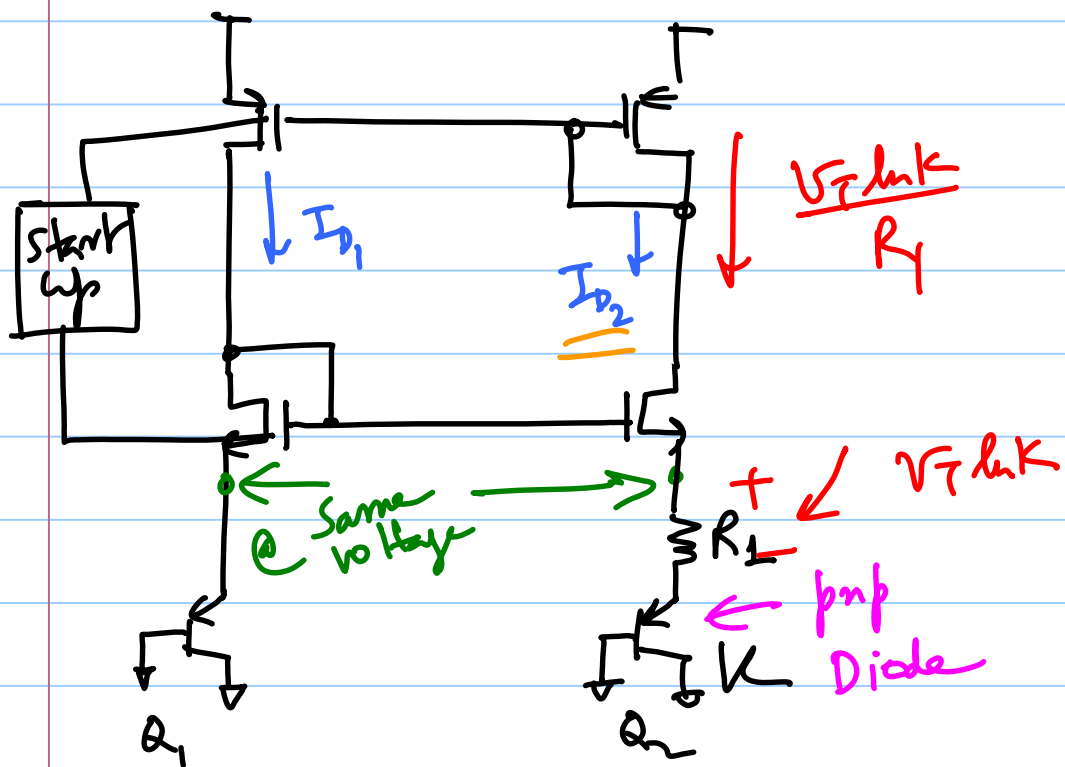
$$= \underbrace{V_{BE2}}_{CTAT} + \underbrace{\left(1 + \frac{R_2}{R_3} \right)}_{\alpha_2 > 1} \underbrace{V_T \ln K}_{PTAT}$$

Example

$$\alpha_2 \ln K = 17.2$$

$$\Rightarrow K = 31 \text{ \& } \frac{R_2}{R_3} = 4$$

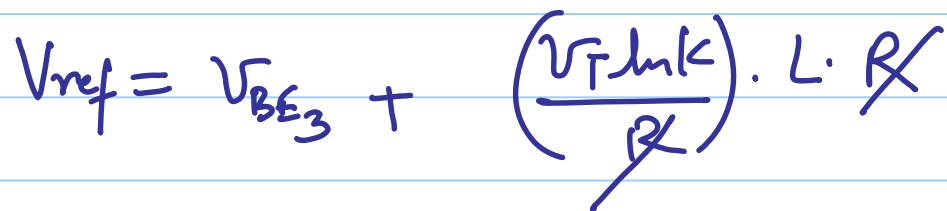
" ∞ solutions"



$$I_{D1} = I_{D2} = \frac{V_T \ln K}{R}$$

↓

$$\frac{PTAT}{R}$$



$$V_{ref} = \underbrace{V_{BE3}}_{CTAT} + \underbrace{L \cdot V_T \ln K}_{PTAT}$$

Σ .

$$K=8,$$

$$L = \frac{17.2}{\ln(8)} \supset 8.4834$$