

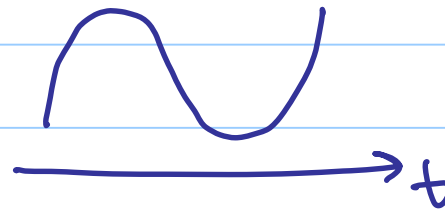
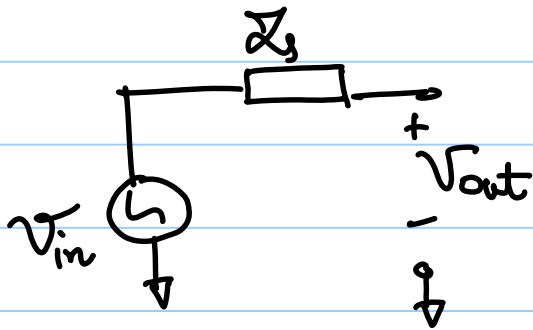
ECE 511 - Lecture 19

Note Title

4/3/2014

Differential Amplifiers

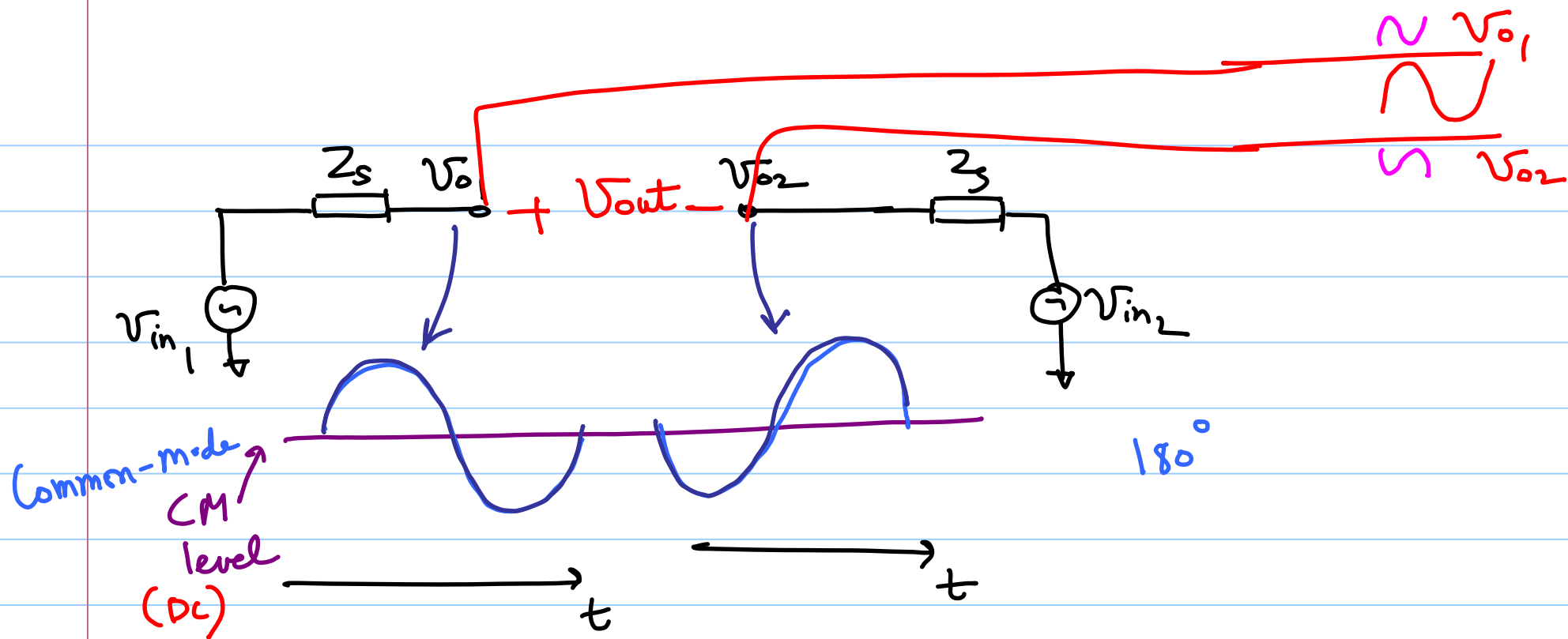
"single-ended signaling"



referred to ground

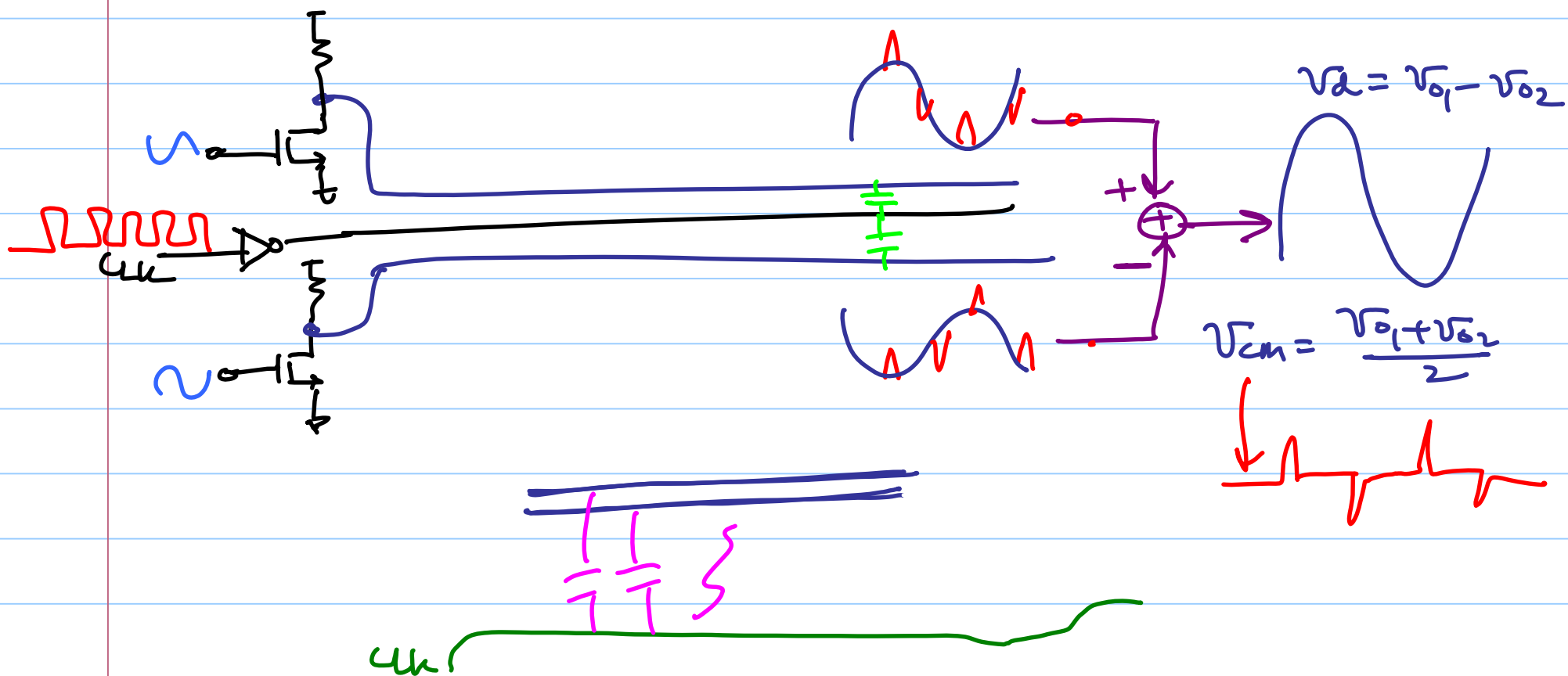
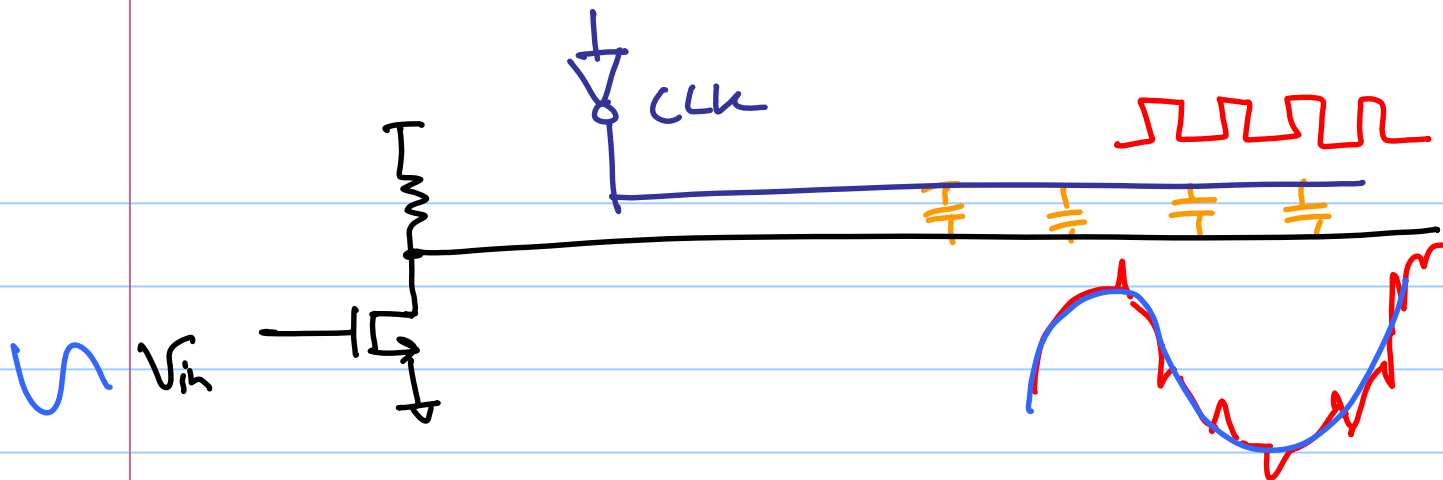
① Monday Apr/7, 3PM
SUB Barnsworth

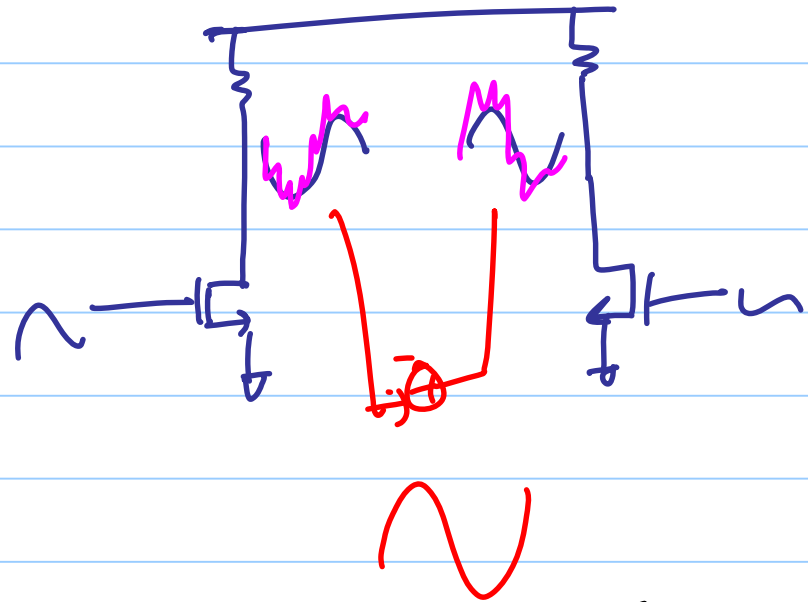
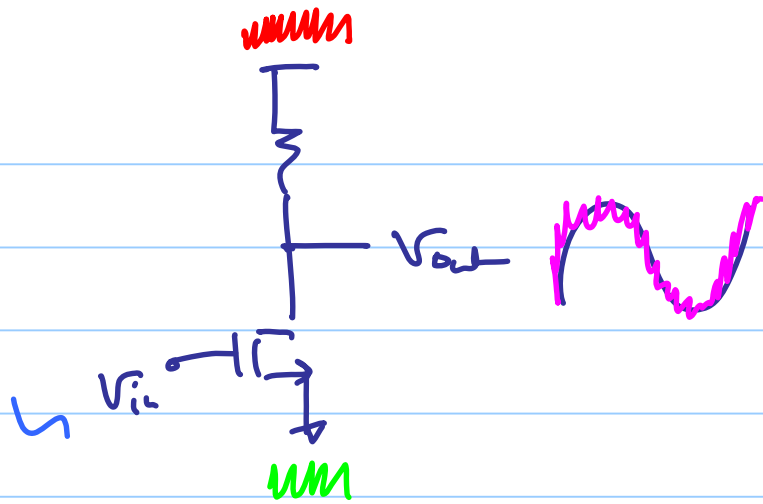
② Wednesday Apr/9, 4:30PM
Talk on Power Management Circuits
Dr. Paul Firth 



Differential signal $\Rightarrow V_d = V_{o1} - V_{o2}$

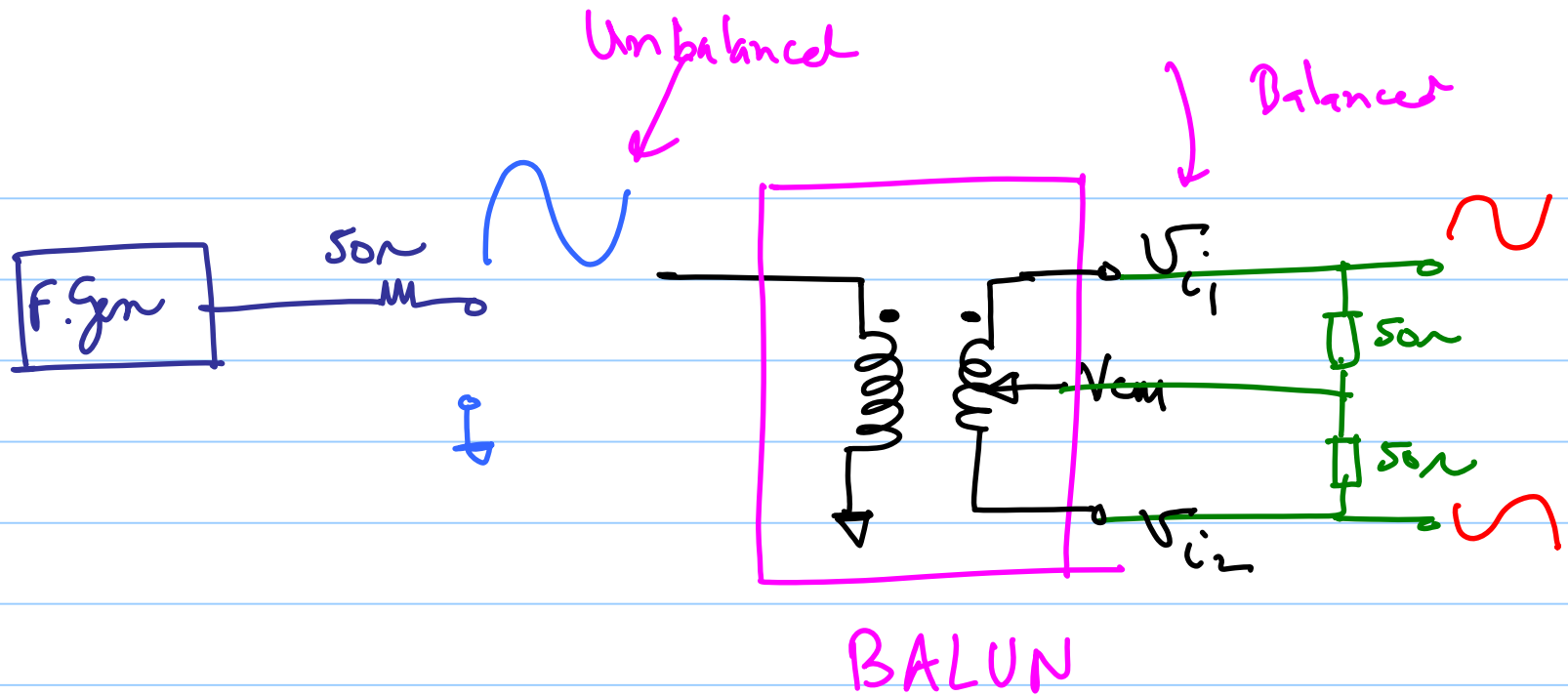
$$V_{cm} = \frac{V_{o1} + V_{o2}}{2} \leftarrow \text{DC value (Ideally)}$$





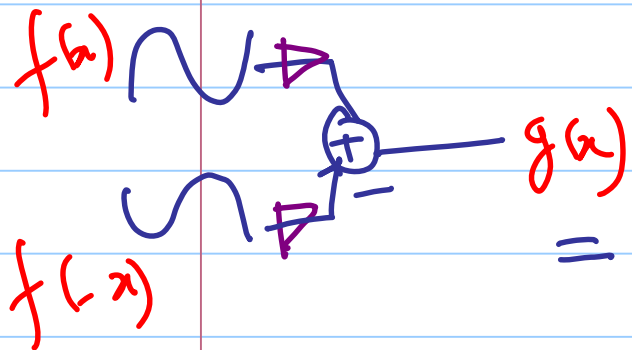
Diff. circuits reject any CM noise / disturbance

* Also cancel any even-order non-linearity



$$g(x) = \frac{f(x) - f(-x)}{2}$$

Odd function

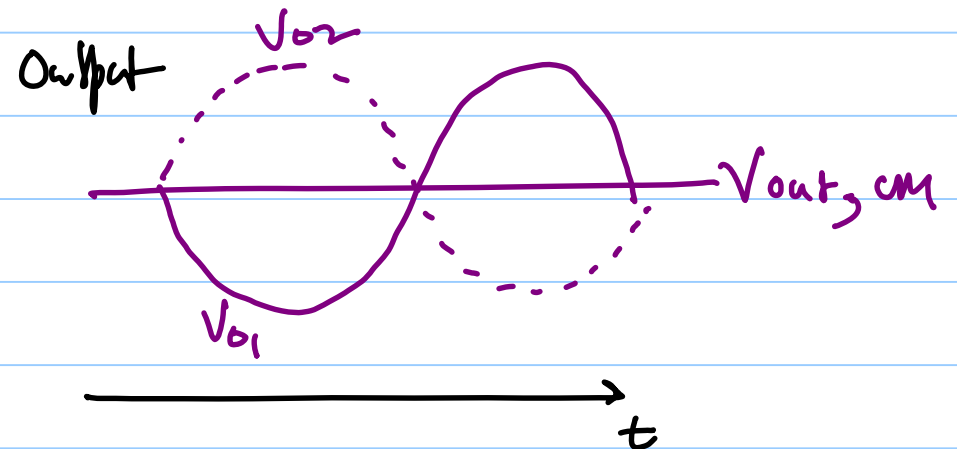
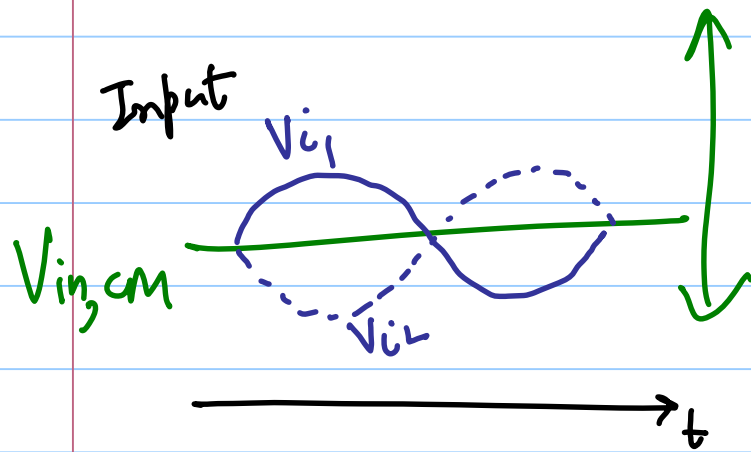
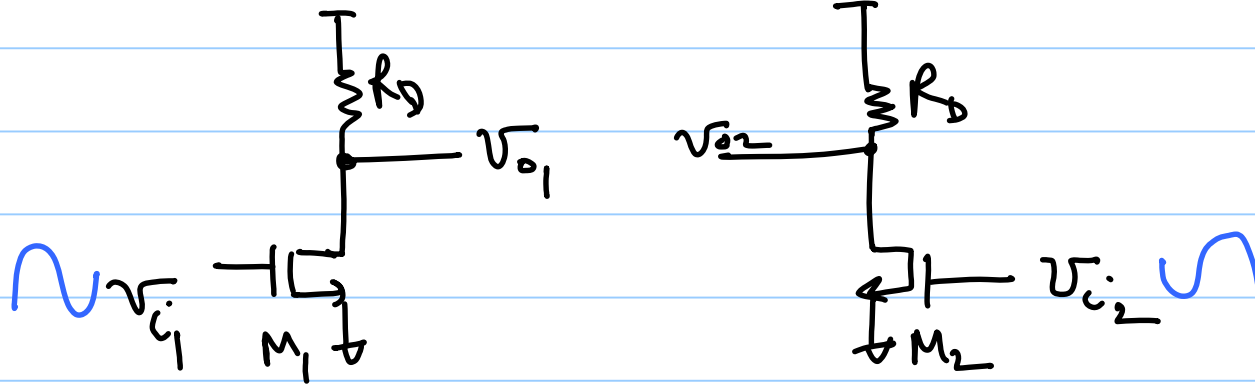


only has odd-order Taylor series

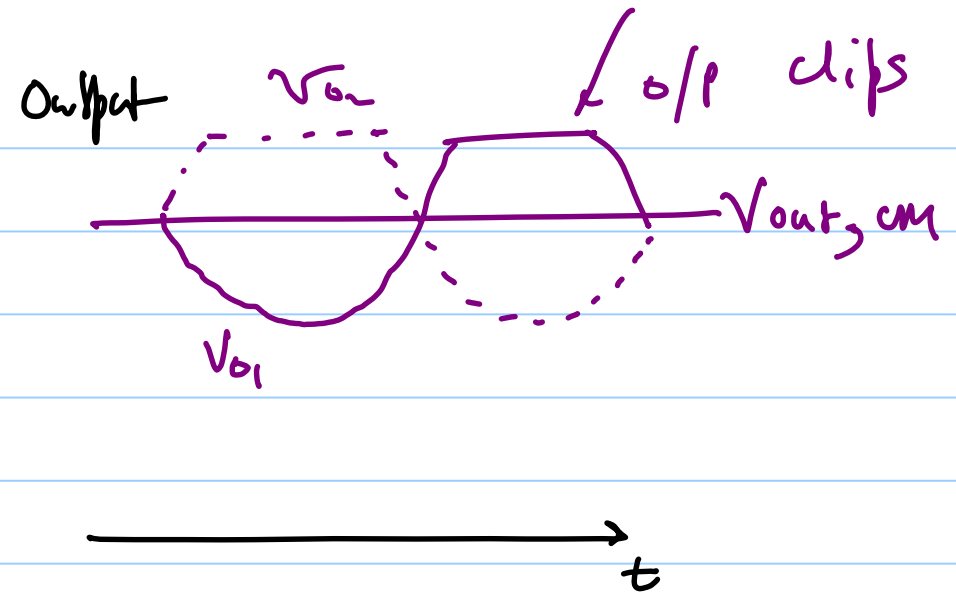
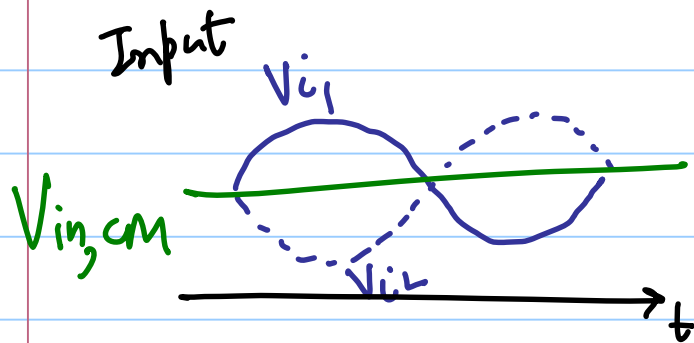
$$g_1 x + g_3 x^3 + g_5 x^5$$

* gets rid of Even-order
nonlinearity terms

CS Amplifier

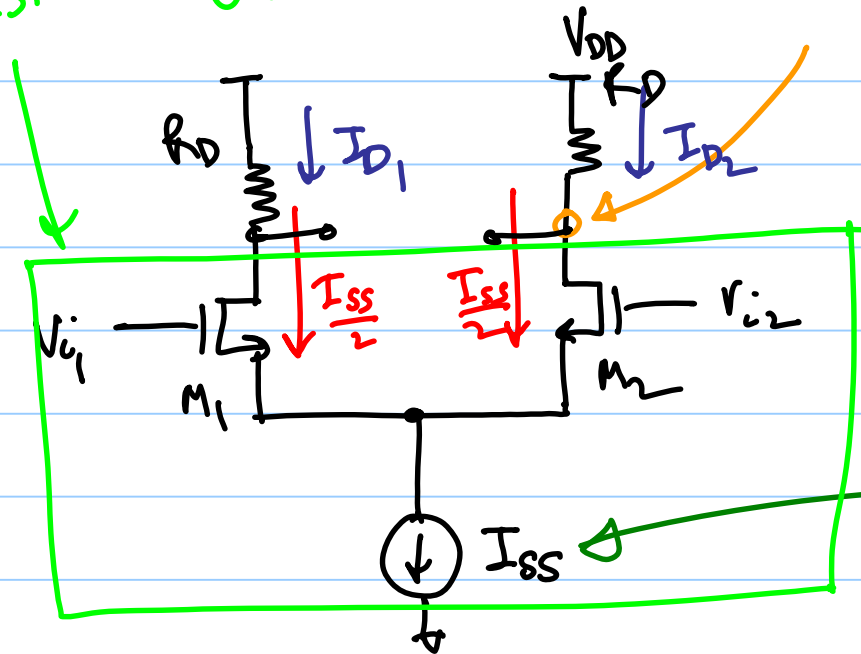


What happens if $V_{in,cm}$ is not well-defined



What we want is that DC biasing should be indep.
of the $V_{in,cm}$ (input cm-level)

Basic Diff - Pair

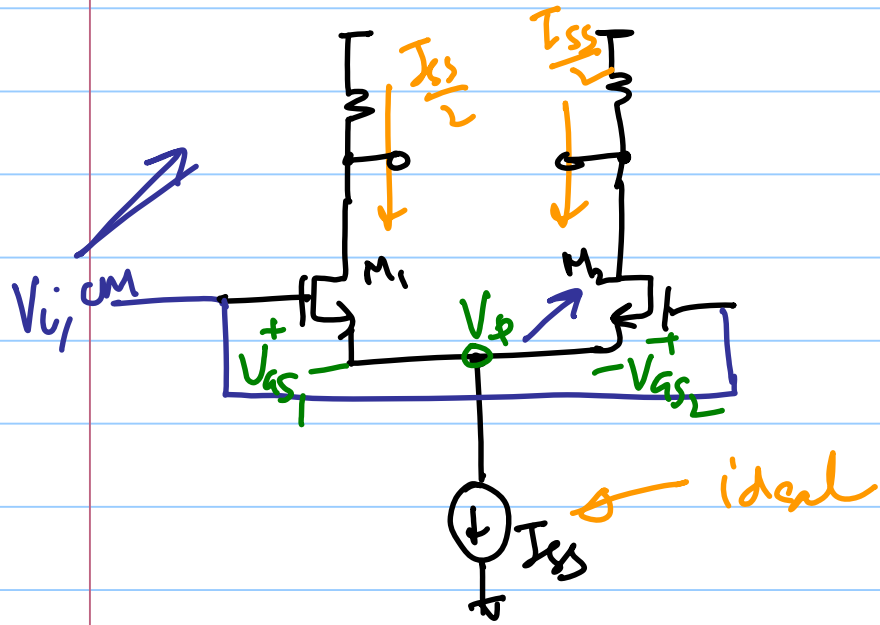


$$I_{D1} + I_{D2} = I_{SS}$$

tail current source

Output
CM-level : $V_{out, cm} = V_{DD} - \frac{I_{SS}}{2} \cdot R_D$

Basic Diff amp

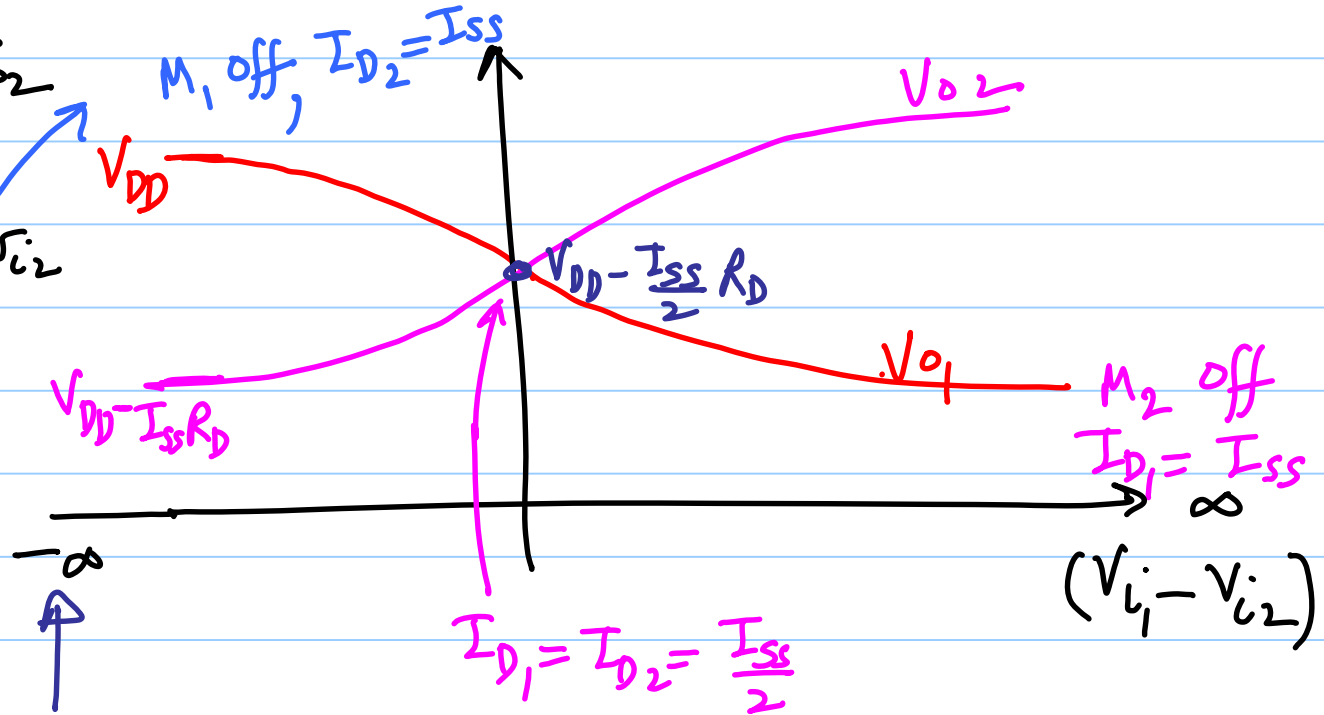
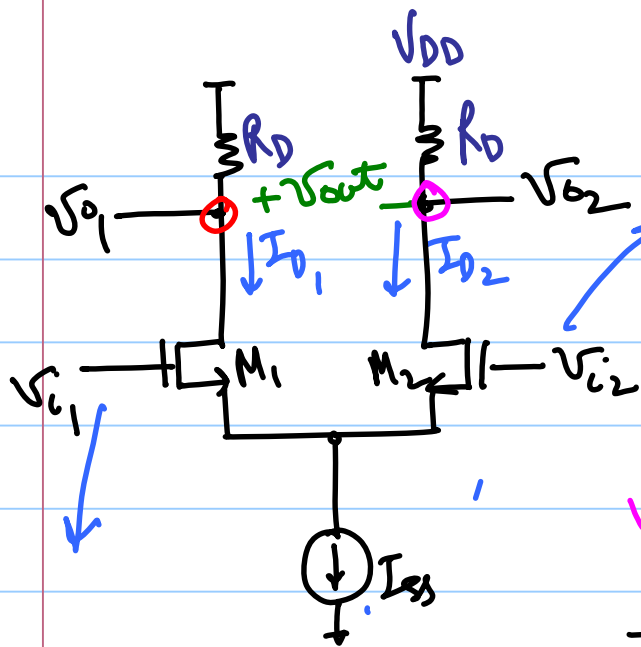


$$V_{GS1} = \sqrt{\frac{I_{SS}}{\beta}} + V_{THN}$$

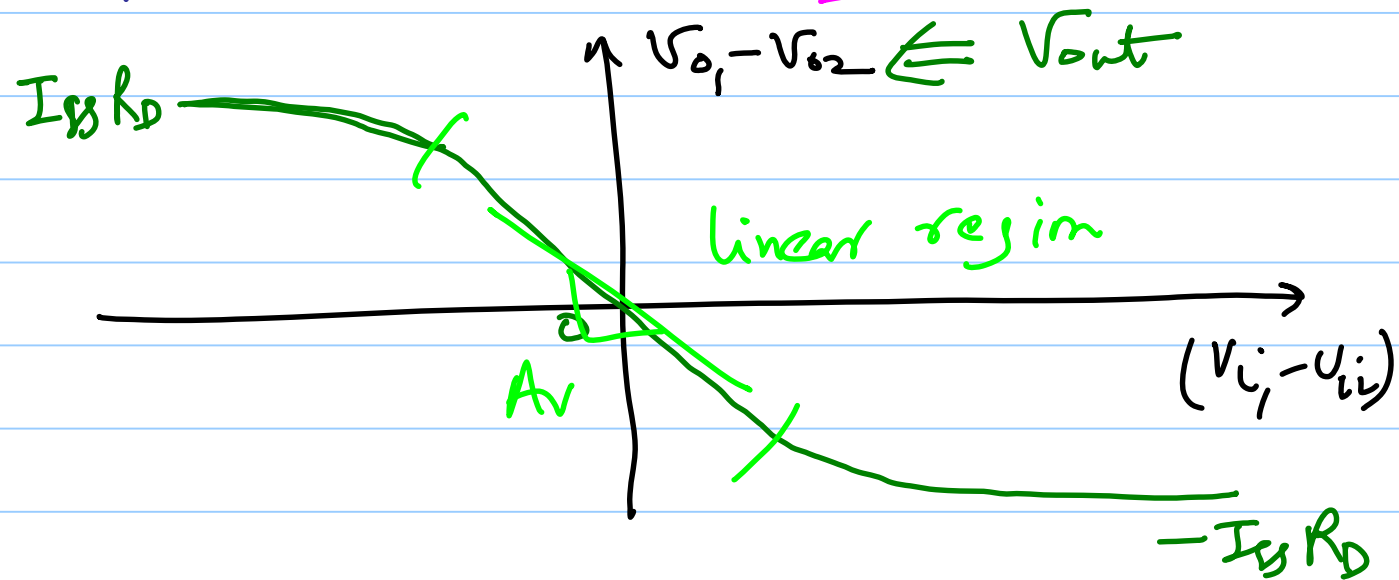
As long as $M_{1/2}$ & I_{ss} are in saturation

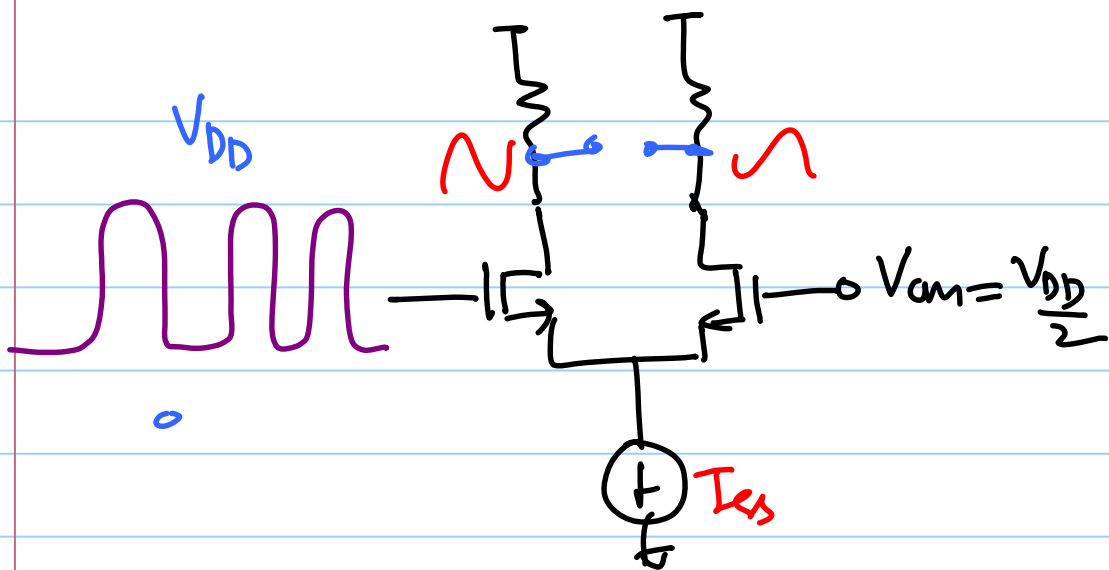
→ Biasing (V_{GS}, I_D, V_{DS}) is indep of V_{in}, ω .

greatly simplifies Biasing!



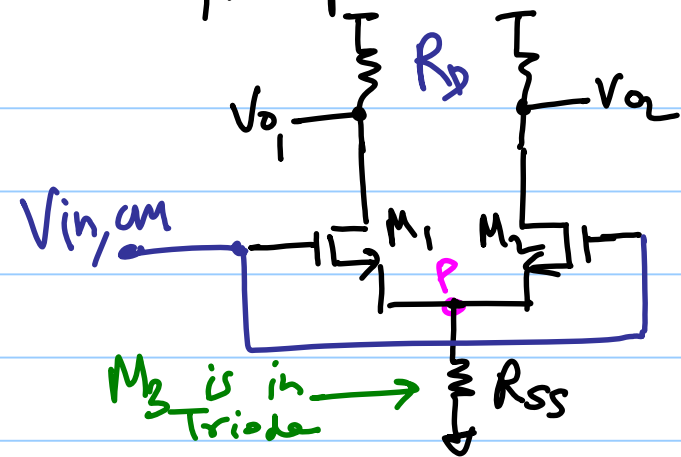
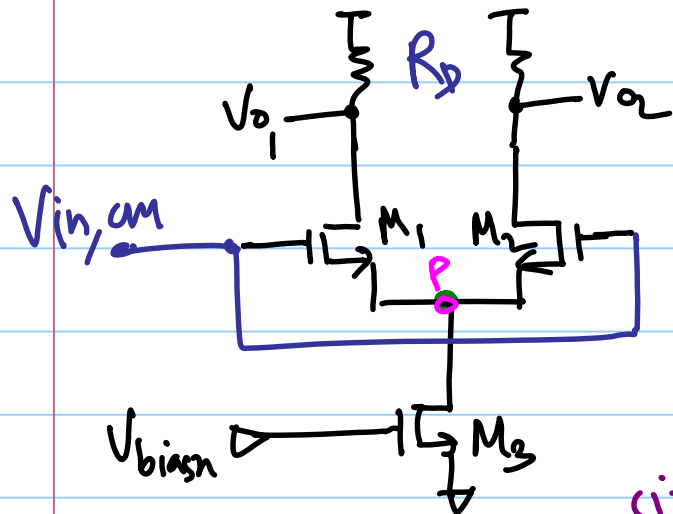
indep of
input
cm-level



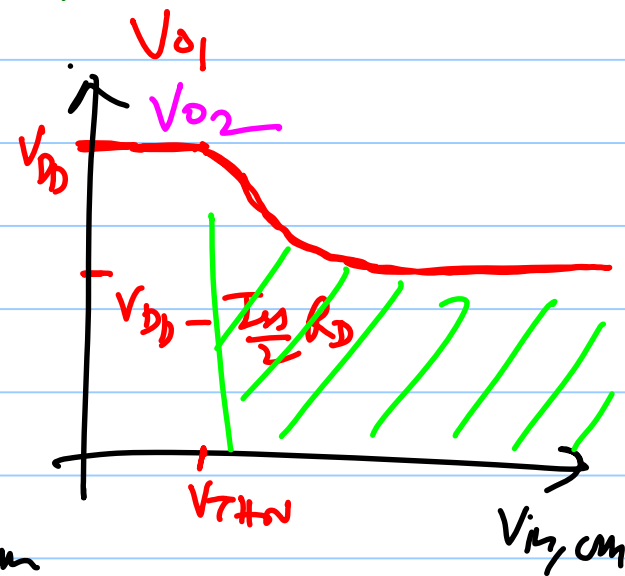
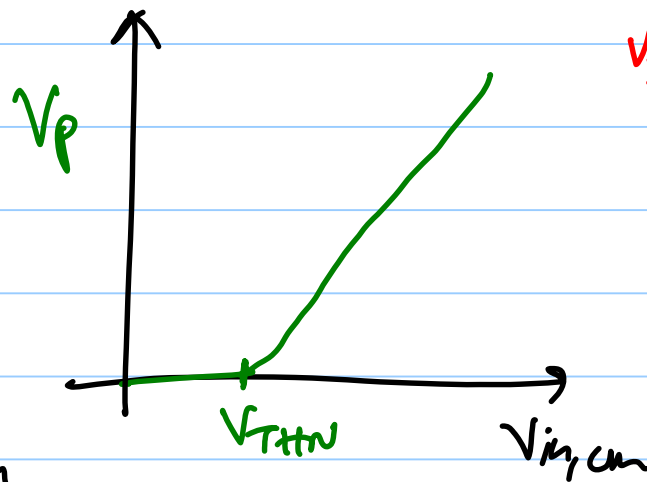
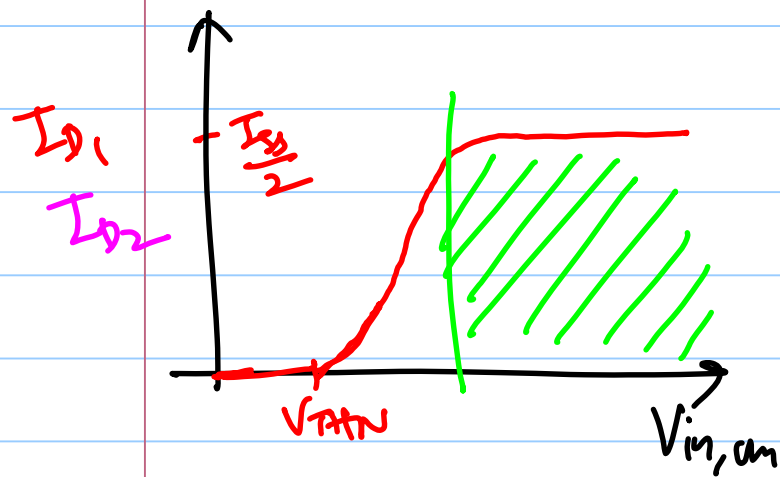


4 with
(aveats)

Common-Mode Behavior of a Diff-pair



(i) $V_{in,cm} = 0$ (ii) $V_{in,cm} > V_{THN}$



INPUT

CMR

Common-mode range

