

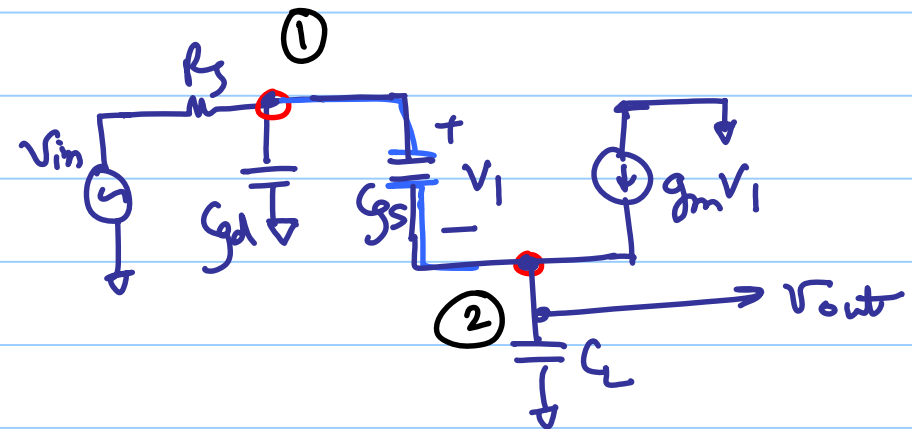
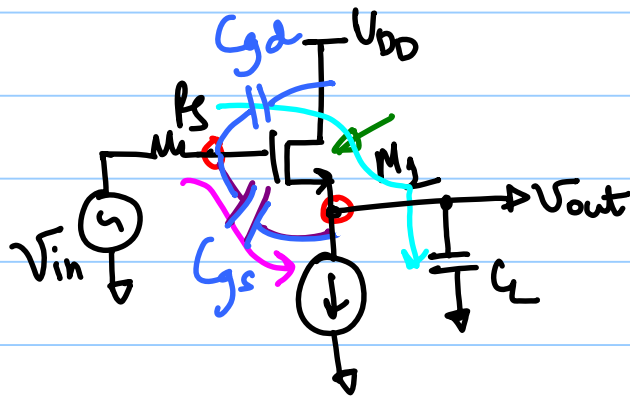
ECE 511- Lecture 18

Note Title

4/1/2014

Source followers frequency response

$\gamma \rightarrow \infty$



feed forward current is adding
to the output with same polarity
→ adding to the phase
→ LHP zero

2 nodes coupled to
each other thru
 C_{gs}
⇒ 2 poles

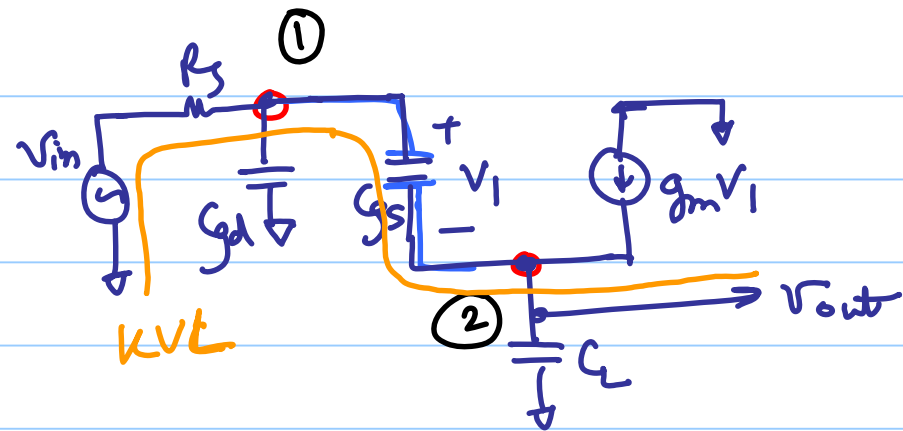
@ node 2

$$V_1 C_{gs} s + g_m V_1 = V_{out} \cdot C_L s$$

$$\Rightarrow V_1 = \frac{s C_L}{g_m + s C_{gs}} \cdot V_{out} \rightarrow \text{①}$$

KVL

$$V_{in} = R_s [V_1 C_{gs} s + (V_1 + V_{out}) s C_{gd}] + V_1 + V_{out} \rightarrow \text{②}$$



$$\frac{V_{out}}{V_{in}}(s) = \frac{(g_m + C_{gs} s)}{R_s [C_{gs} C_L + C_{gs} C_{gd} + C_{gd} C_L] s^2 + [g_m R_s C_{gd} + C_L + C_{gs}] s + g_m}$$

$\frac{1}{\omega_{p1}} + \cancel{\frac{1}{\omega_{p2}}}$

$$\omega_z = -\frac{g_m}{C_S}$$

LHP zero

Assuming $|\omega_{p1}| \ll |\omega_{p2}|$

→ Dominant pole

$$\omega_{p1} \approx \frac{g_m}{g_m R_S C_S + C_L + C_S}$$

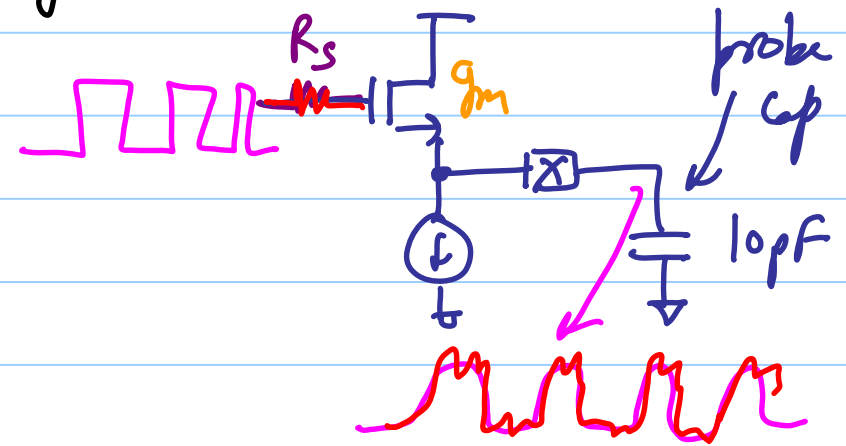
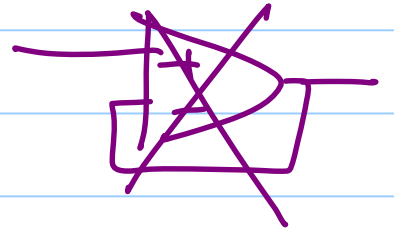
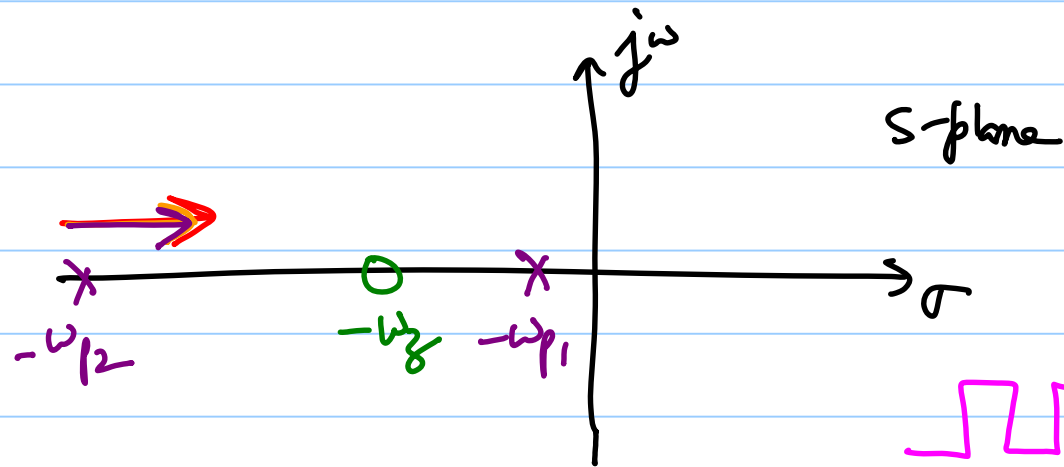
(using same method as C_S freq. response)

$$= \frac{1}{R_S C_S + \left(\frac{C_L + C_S}{g_m} \right)}$$

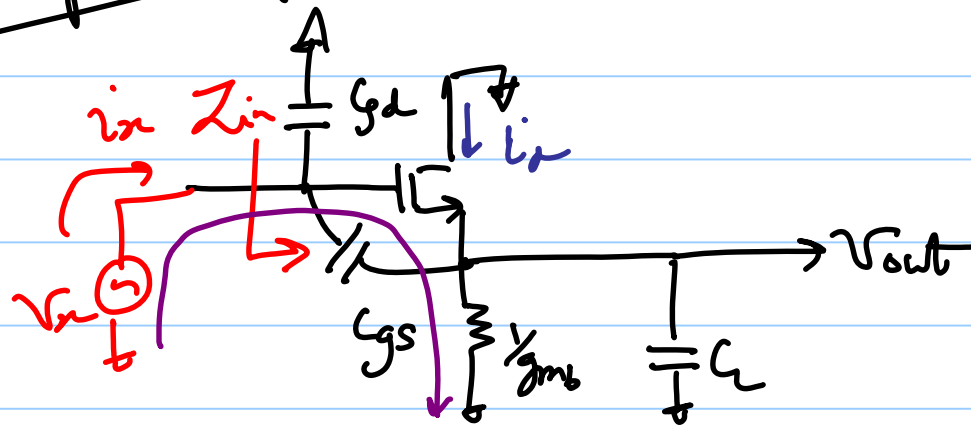
$$R_S = 0$$

$$\boxed{\omega_{p1} \approx \frac{g_m}{C_S + C_L}}$$

Large $C_L \Rightarrow g_{m1} \uparrow \Rightarrow \frac{W}{L} \propto V_{ov}$



Input Impedance



$$v_{gs} = \frac{i_x}{sC_{gs}}$$

$$\Rightarrow i_d = g_m v_{gs} = \frac{g_m i_x}{sC_{gs}} \rightarrow \textcircled{1}$$

$$v_x = \frac{i_x}{sC_{gs}} + \left(i_x + \frac{g_m i_x}{sC_{gs}} \right) \left(\frac{1}{g_{mb}} \parallel \frac{1}{sC_L} \right) \rightarrow \textcircled{2}$$

$$Z_{in} = \frac{1}{sC_{gs}} \left(1 + \frac{g_m}{g_{mb}} \right) + \frac{1}{g_{mb}}$$

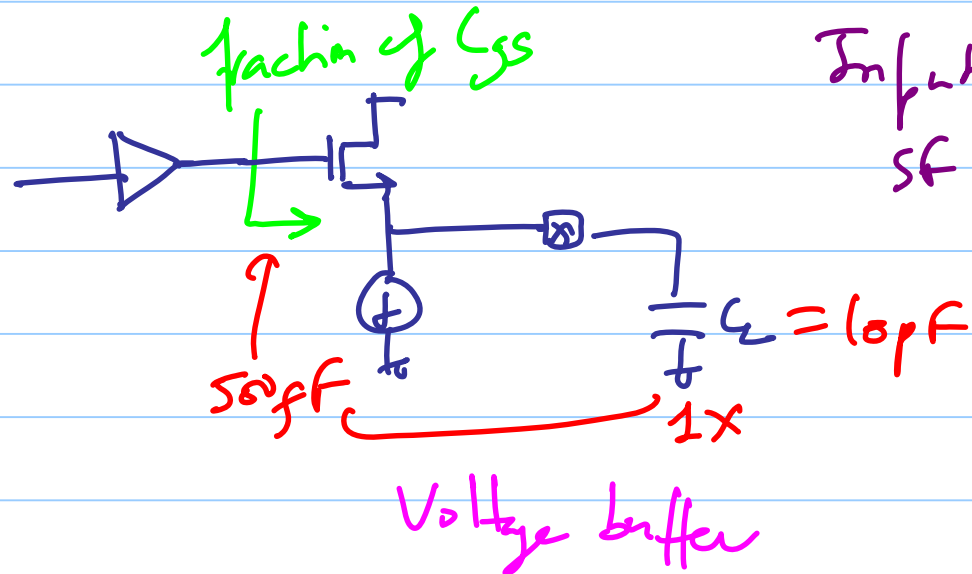
$$Z_{in} = \frac{1}{\frac{sC_{gs}}{(1 + g_m/g_{mb})}} + \frac{1}{g_{mb}}$$

Input Cap $\Rightarrow \frac{C_{gs}}{\left(1 + \frac{g_m}{g_{mb}}\right)}$

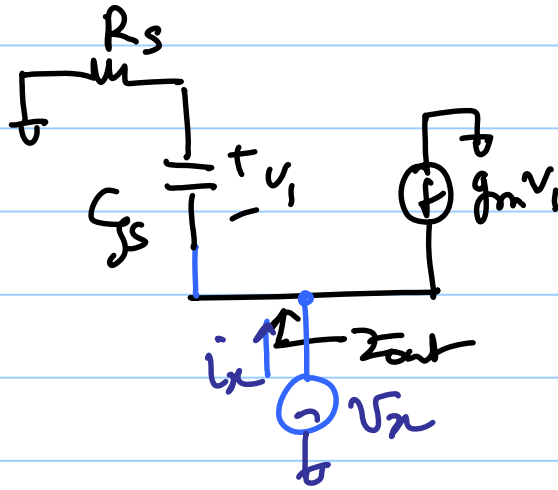
fraction of C_{gs}

Refer to Razavi

post nks online



output impedance of $\sim$ SF

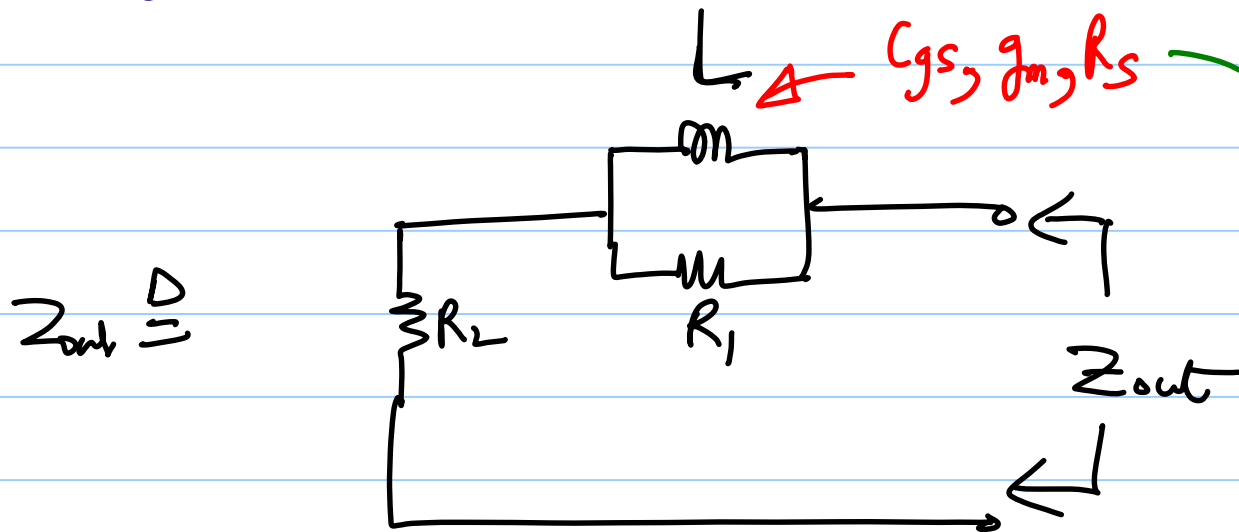
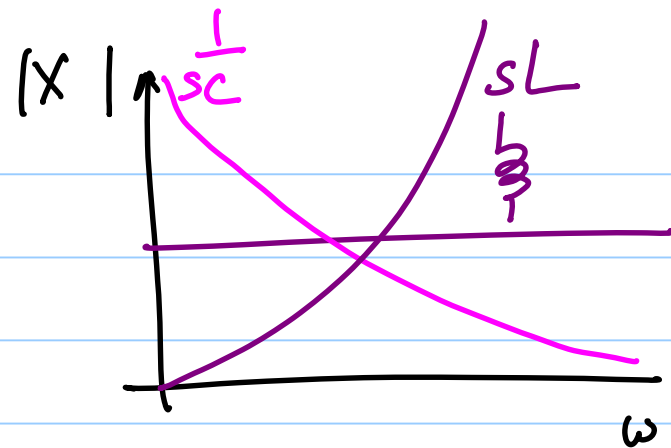
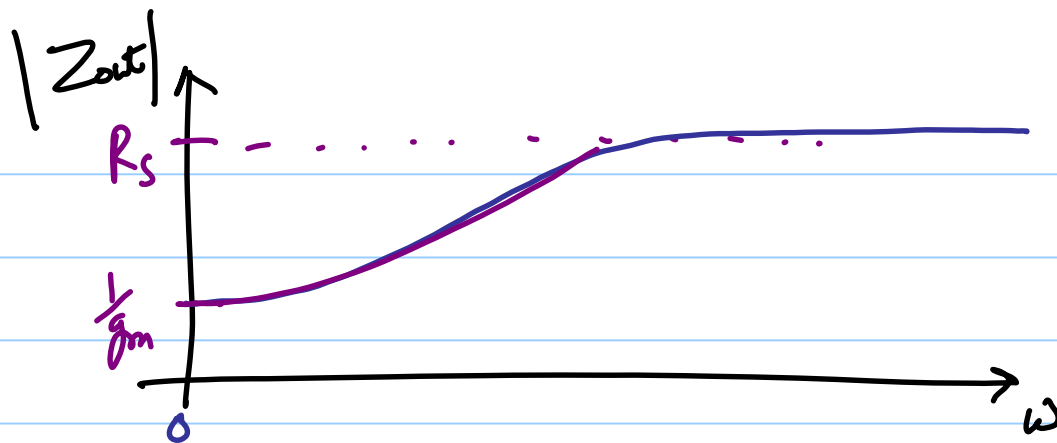


$$Z_{out} = \frac{R_s C_s s + 1}{g_m + s C_s}$$

* at low frequencies $j\omega \rightarrow 0 \Rightarrow s \rightarrow 0$

$$Z_{out} \approx \frac{1}{g_m}$$

* at high frequencies $j\omega \rightarrow \infty \Rightarrow Z_{out} \approx R_s$

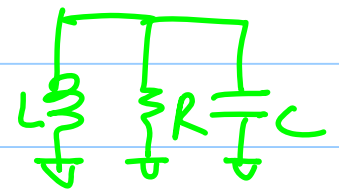
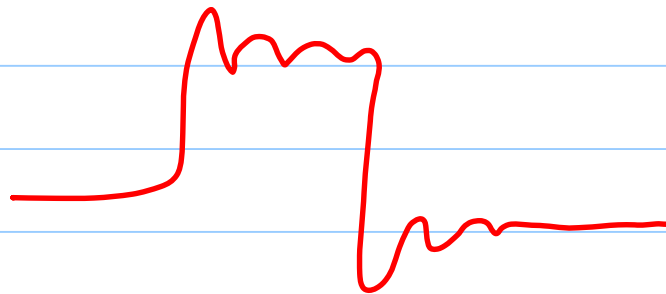
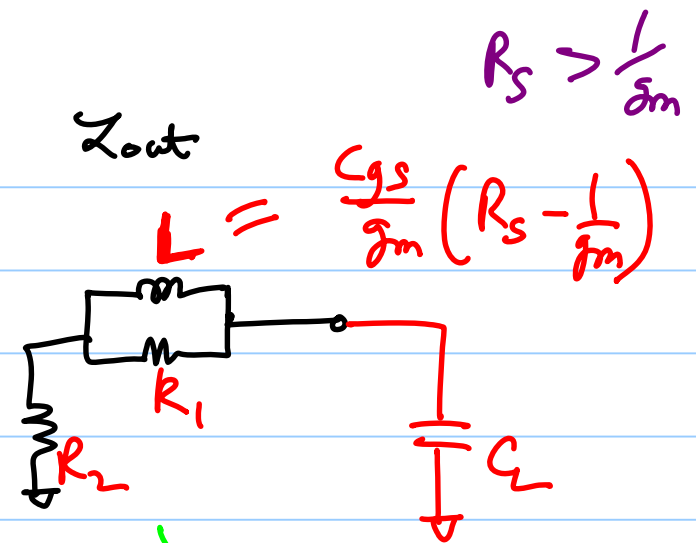
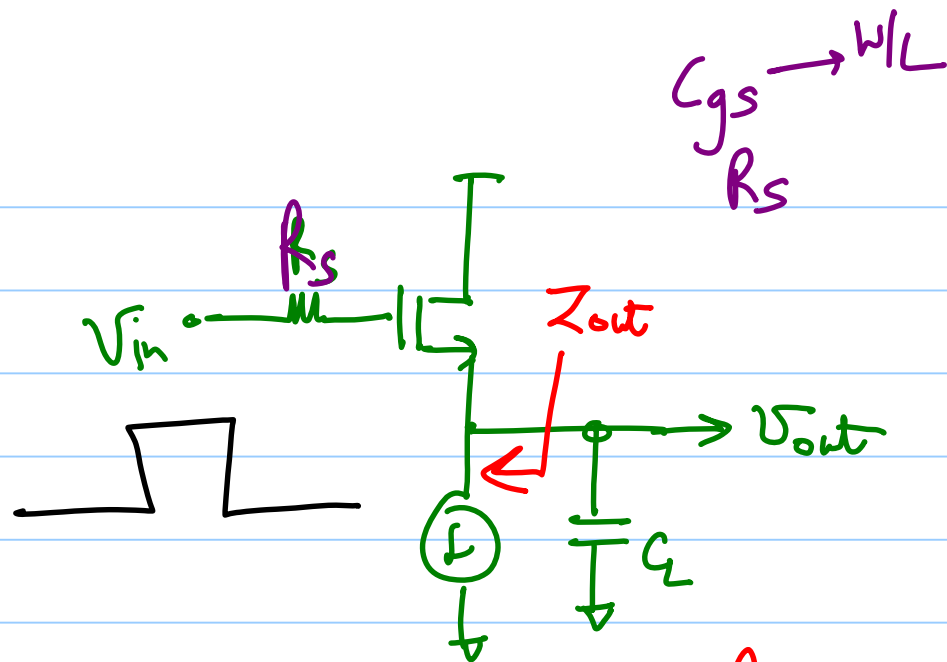


$\Delta C_{gs}, g_m, R_s$

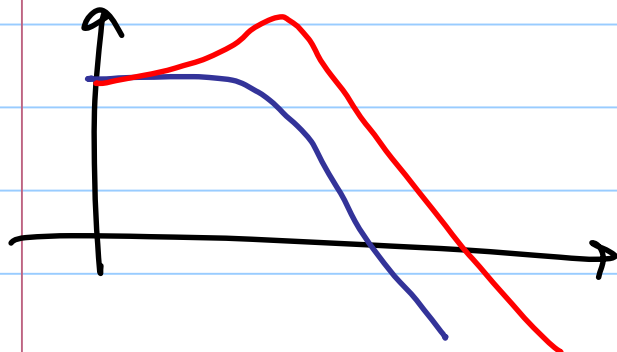
$$L = \frac{C_{gs}}{g_m} \left(R_s - \frac{1}{g_m} \right)$$

$$R_1 = R_s - \frac{1}{g_m}$$

$$R_2 = \frac{1}{g_m}$$

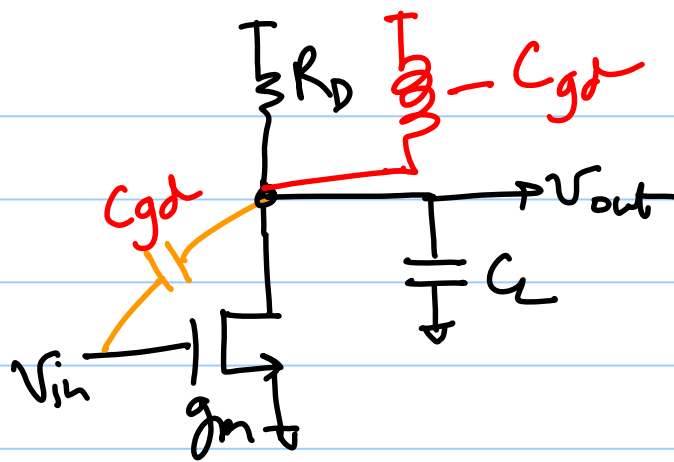


105Hz

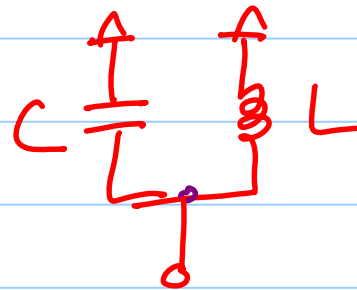


Idea is used to realize Active-L

$\rightarrow$ wide band amplifiers
 BW peaking



$$\omega_p = \frac{1}{R_D(C_L + C_{gd})}$$



$$Y = \frac{1}{Z} = j\omega C + \frac{1}{j\omega L}$$

$$= j\omega \left(-\frac{j}{\omega L} \right)$$

Cascode Amplifier frequency Response

$$A_v = -g_{m1} \cdot R_{out}$$

↓

$$R_D \parallel \underbrace{g_{m2} r_{o2} r_{o1}}_{g_{m1} r_{o1}^2}$$

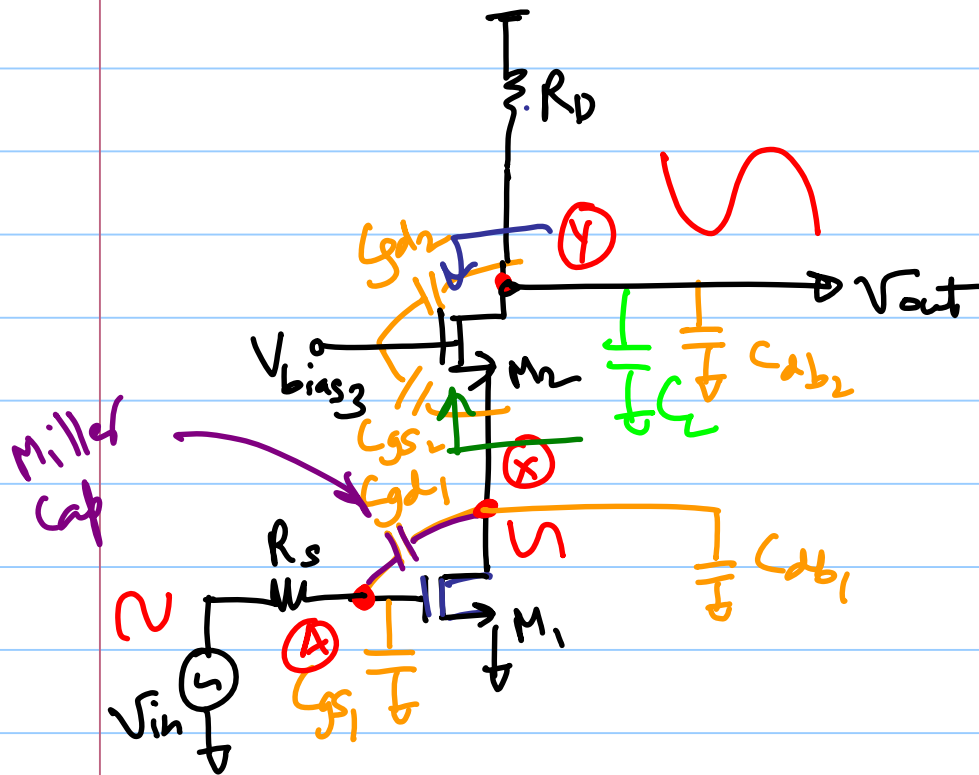
3 nodes
 $\Rightarrow$ 3 poles

Gain from node A to X

assume R_D is small

$$A_{A \rightarrow X} = -g_{m1} \cdot R_X$$

$$\begin{aligned} & \downarrow \\ & r_{o1} \parallel \frac{1}{(g_{m2} + g_{m3})} \\ & \approx -\frac{g_{m1}}{g_{m2}} \approx -1 \end{aligned}$$



gain across Miller
 Cap $C_{gd1} \Rightarrow -1$

$\Rightarrow$ Miller Effect at input
 is reduced

Pole at node (A)

$$\omega_{pA} \approx \frac{1}{R_S \left[C_{gs1} + \left(1 + \frac{g_{m1}}{g_{m2} + g_{m2b}} \right) C_{gd1} \right]}$$

Pole at node (X)

$$C_X = 2C_{gd1} + C_{db1} + C_{gs2} + C_{sb1}$$

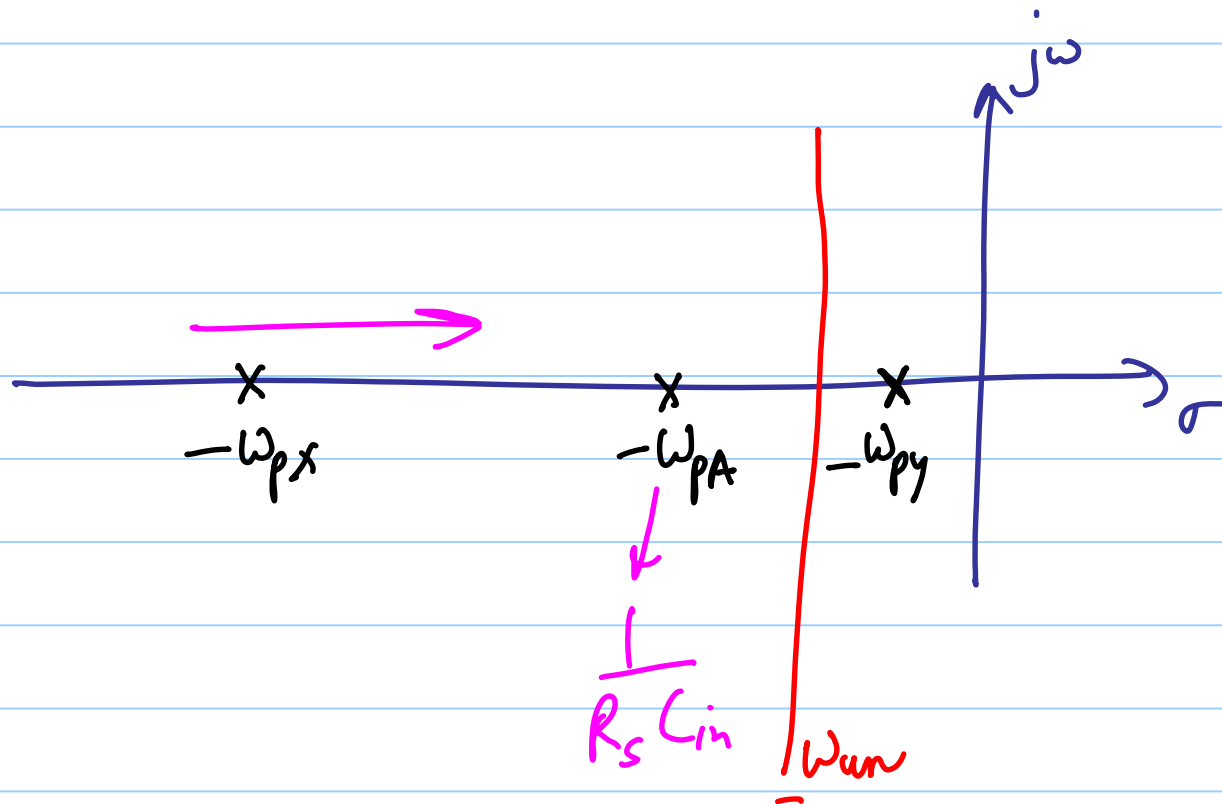
$$R_X \approx \frac{1}{g_{m2} + g_{m2b}}$$

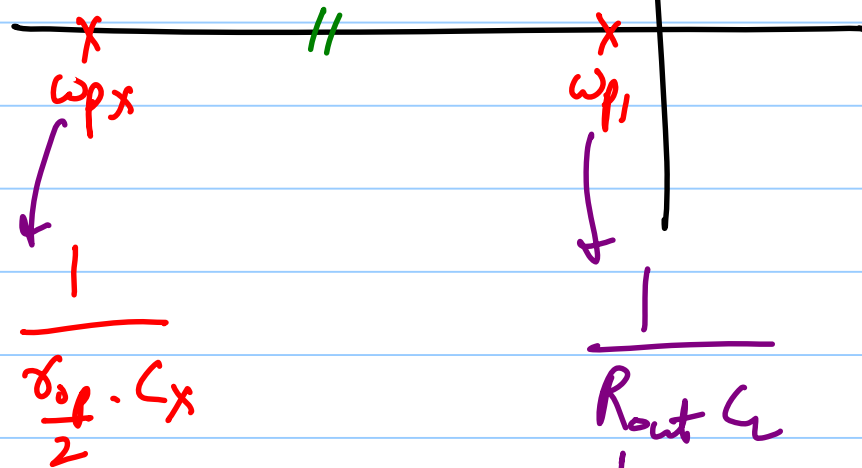
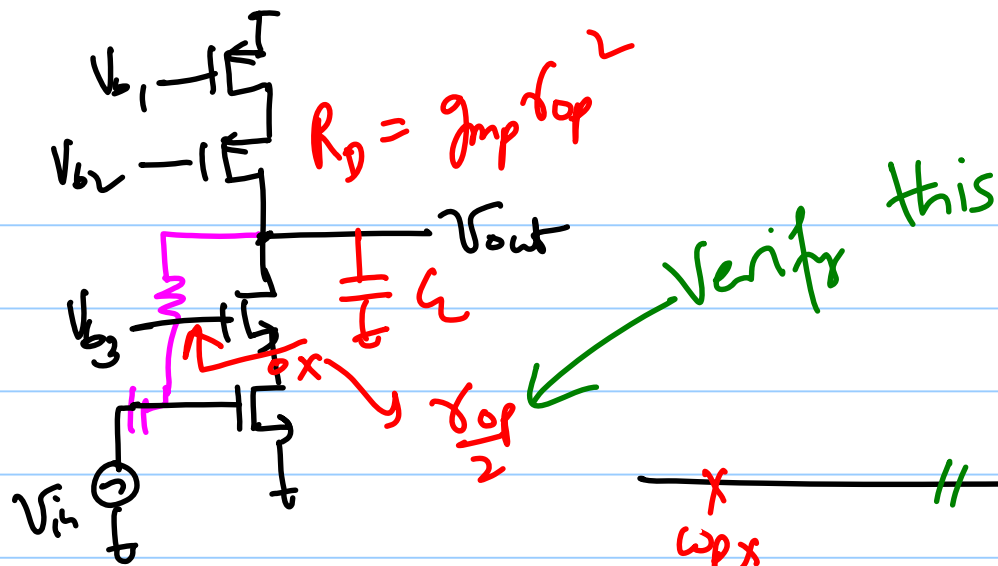
Assuming R_D is small
 $\rightarrow g_{mp} \delta_{op}^2$

$$\omega_{pX} = \frac{1}{R_X C_X} = \frac{g_{m2} + g_{m2b}}{2C_{gd1} + C_{db1} + C_{sb2} + C_{gs2}}$$

* Assuming R_D is small

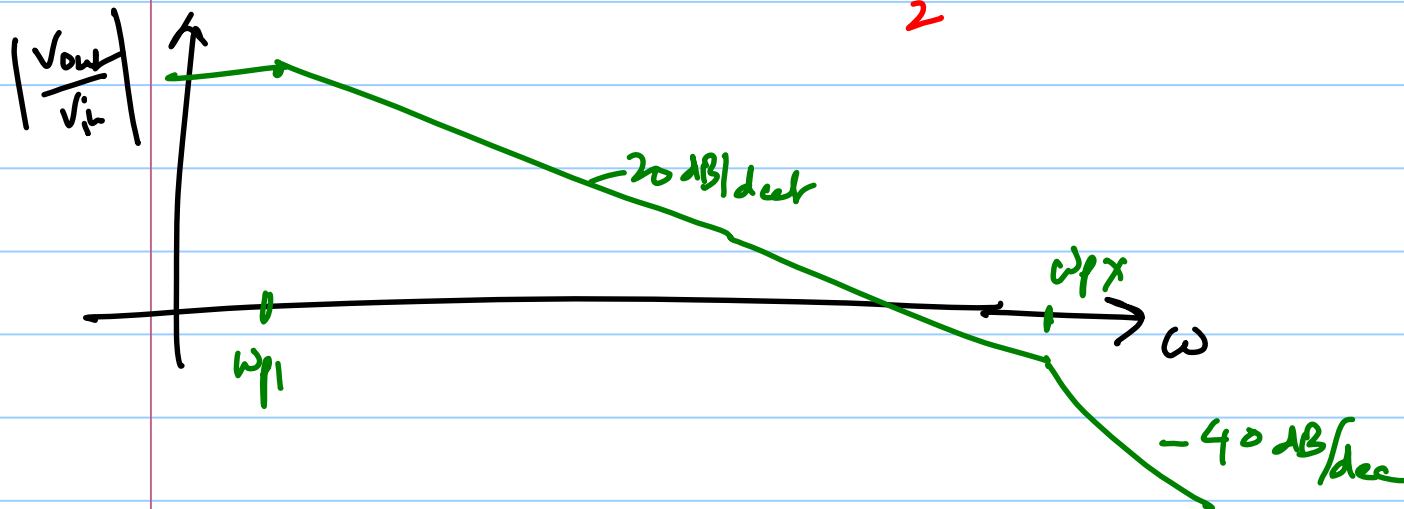
$$\omega_{py} \approx \frac{1}{R_D (C_{db2} + C_L + C_{gd2})} \quad \text{large } C_L$$

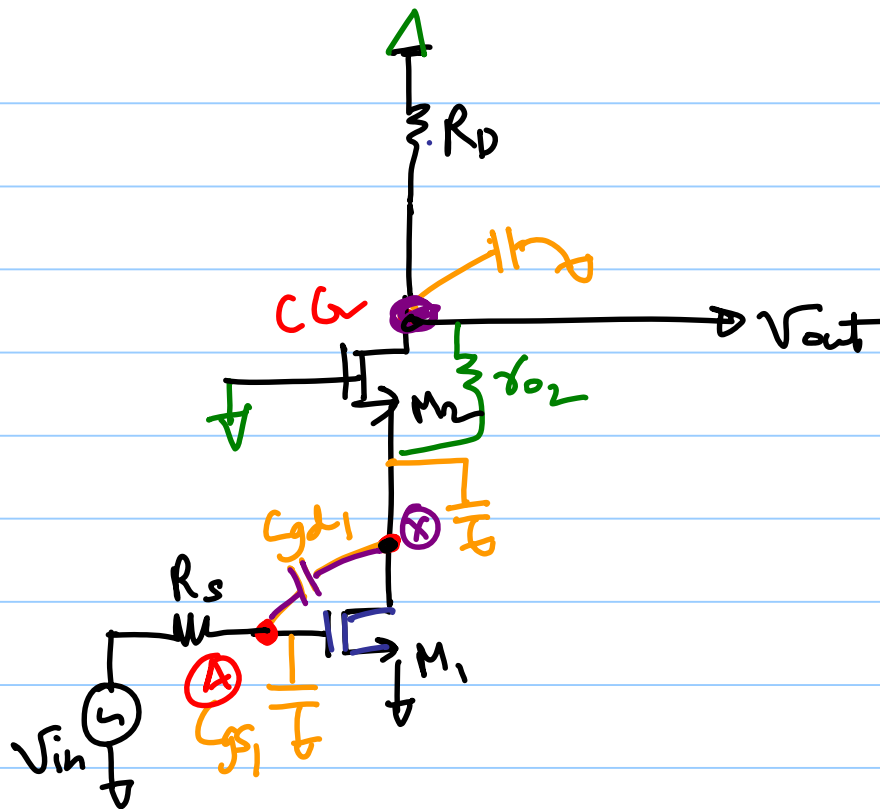




$$\frac{1}{\frac{\delta_{op}}{2} \cdot C_x}$$

$$\frac{1}{R_{out} C_L} \downarrow (g_{m p} \delta_{op}^2) \parallel (g_{m n} \delta_{on}^2)$$



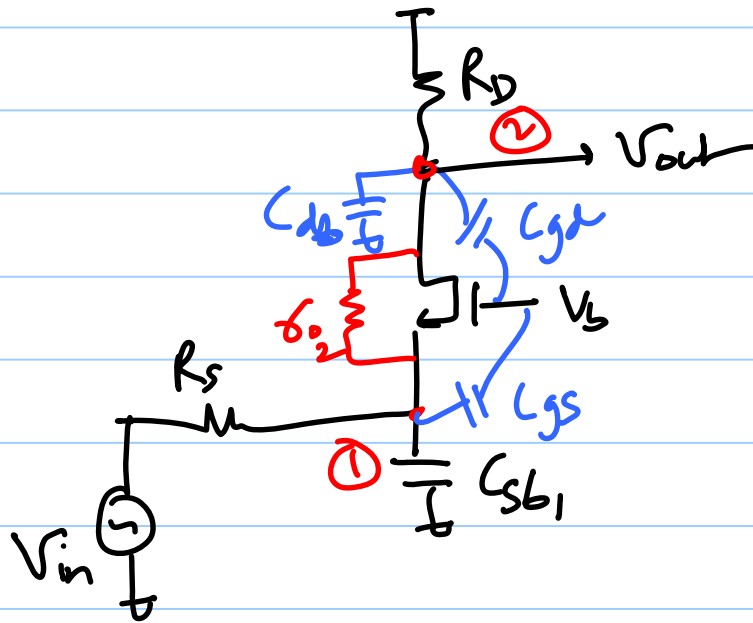


No zeros

↳ isolation due to M_2

⇒ Miller effect is reduced

Common Gate

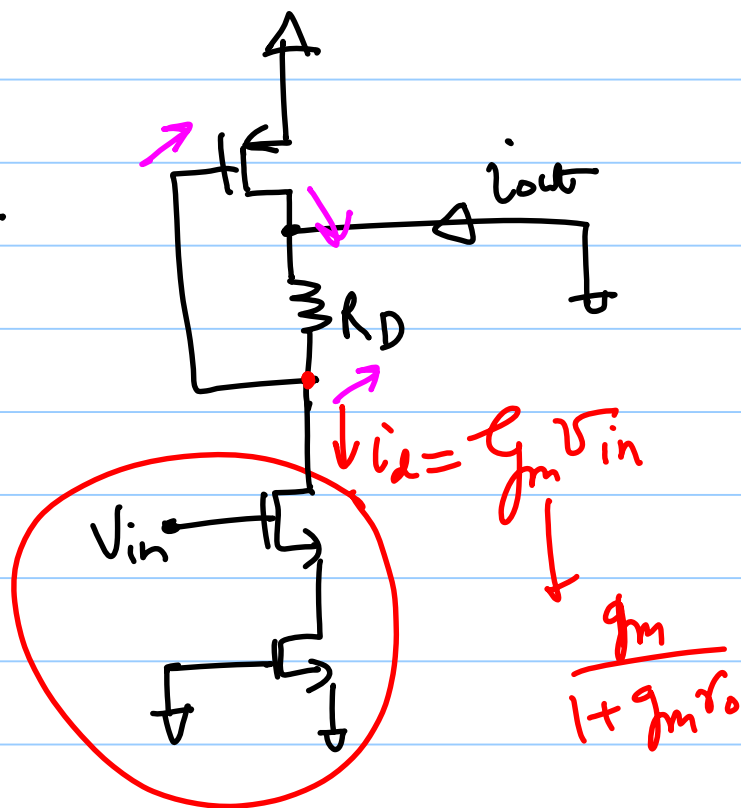
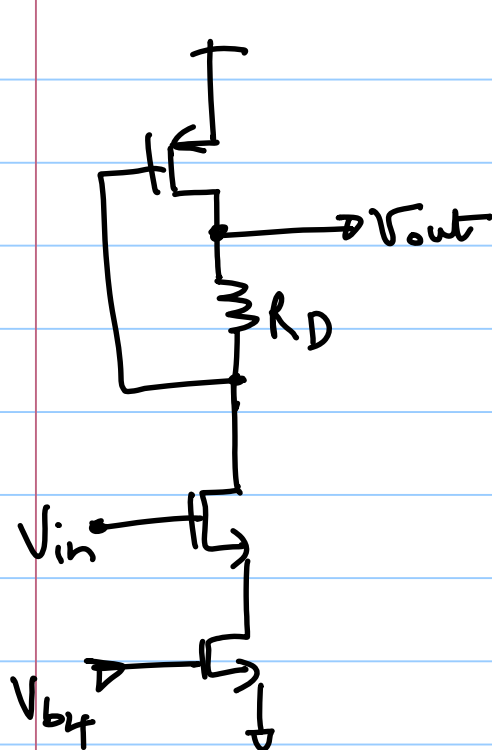


$$\omega_{in} \approx \frac{1}{\left(R_s \parallel \frac{1}{g_m + g_{mb}}\right) C_{in}}$$

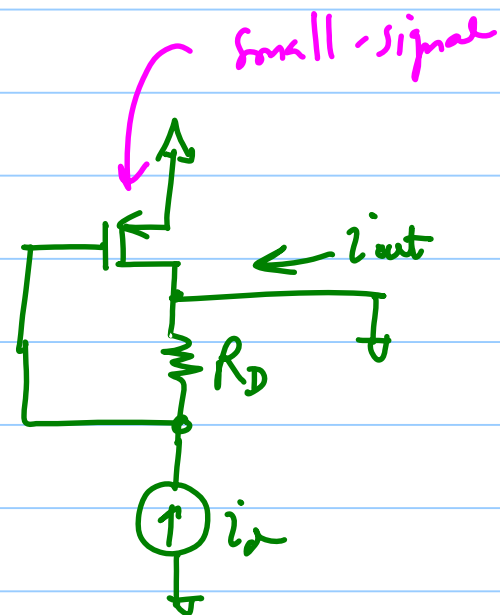
$$\omega_{out} \approx \frac{1}{R_D C_2}$$

No zero.

(e)

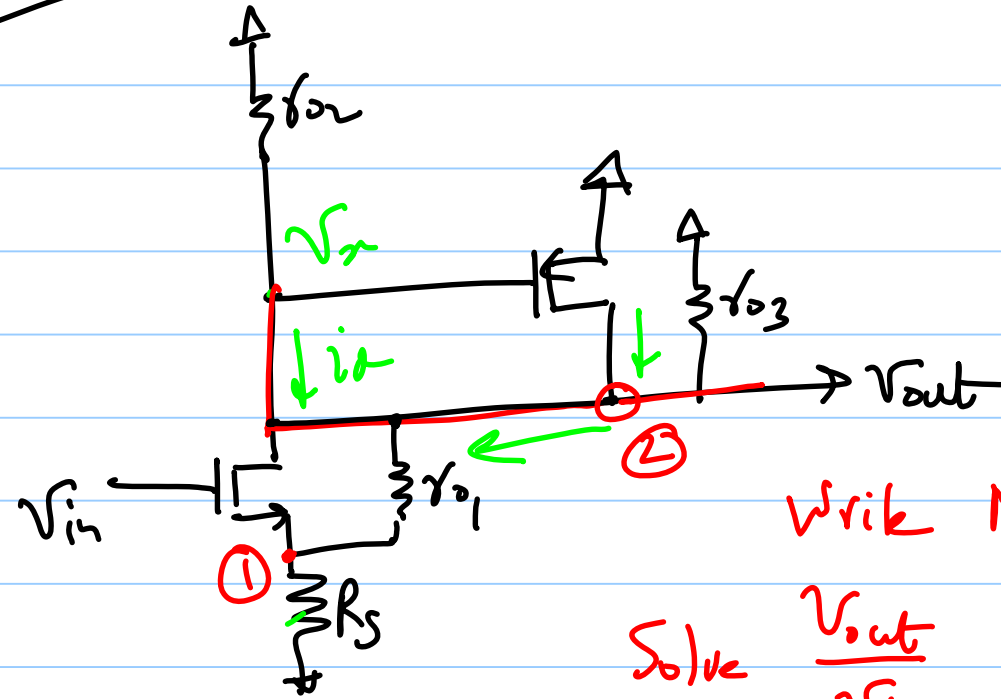


g_m, R_{out}



Problem ③

$\lambda = 0$

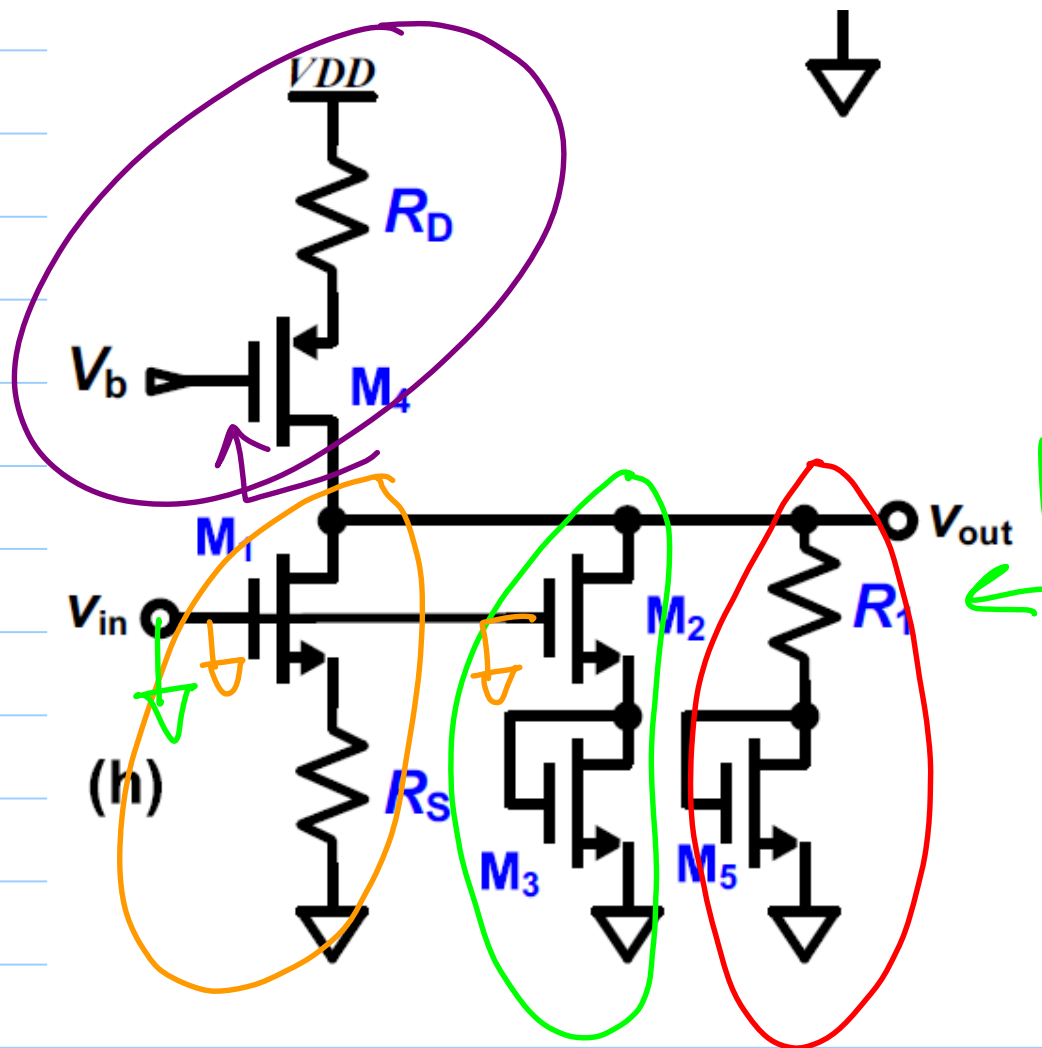


Write Nodal equations

Solve $\frac{V_{out}}{V_{in}}$

Algebra

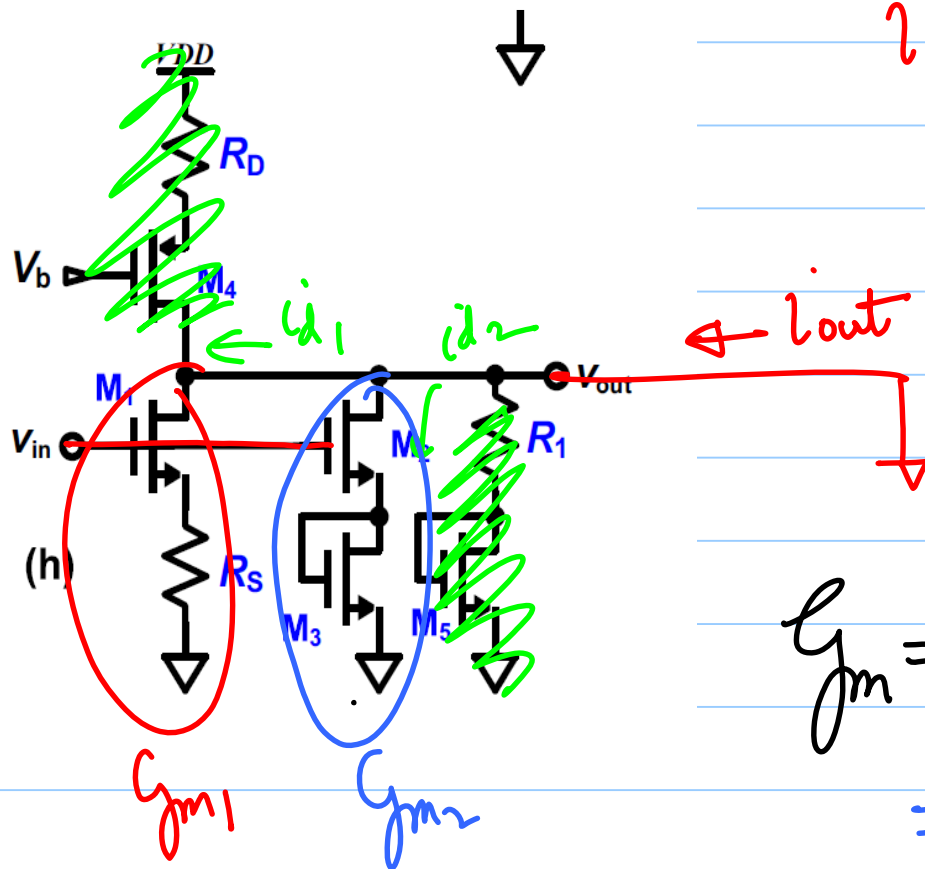
1 (h)



$$R_{out} = g_{m4} r_{o4} R_D \parallel g_{m1} r_{o1} R_S \parallel g_{m2} r_{o2} \cdot \frac{1}{g_{m3}}$$

$$R_1 + \frac{1}{g_{m5}}$$

5

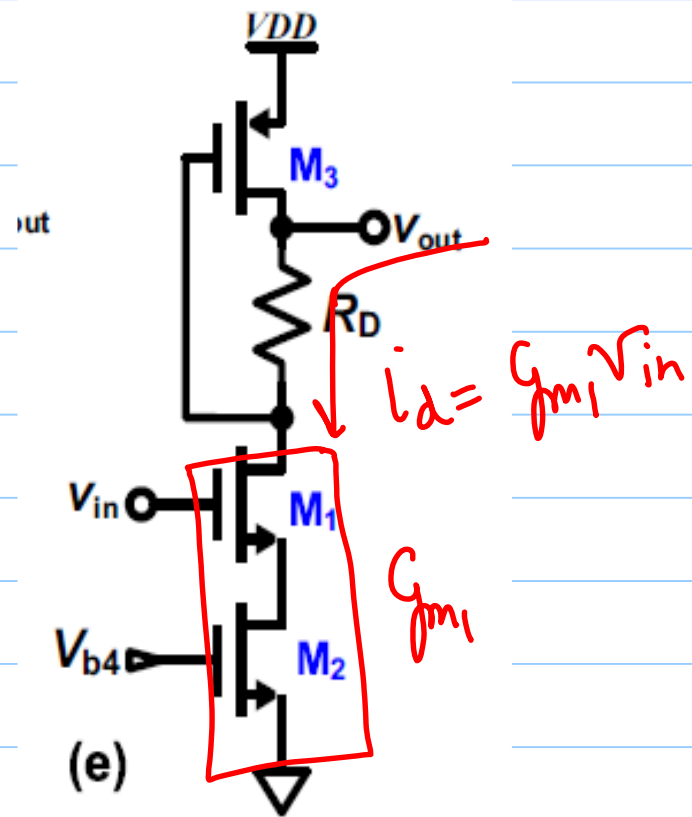


$$i_{out} = i_{d1} + i_{d2}$$

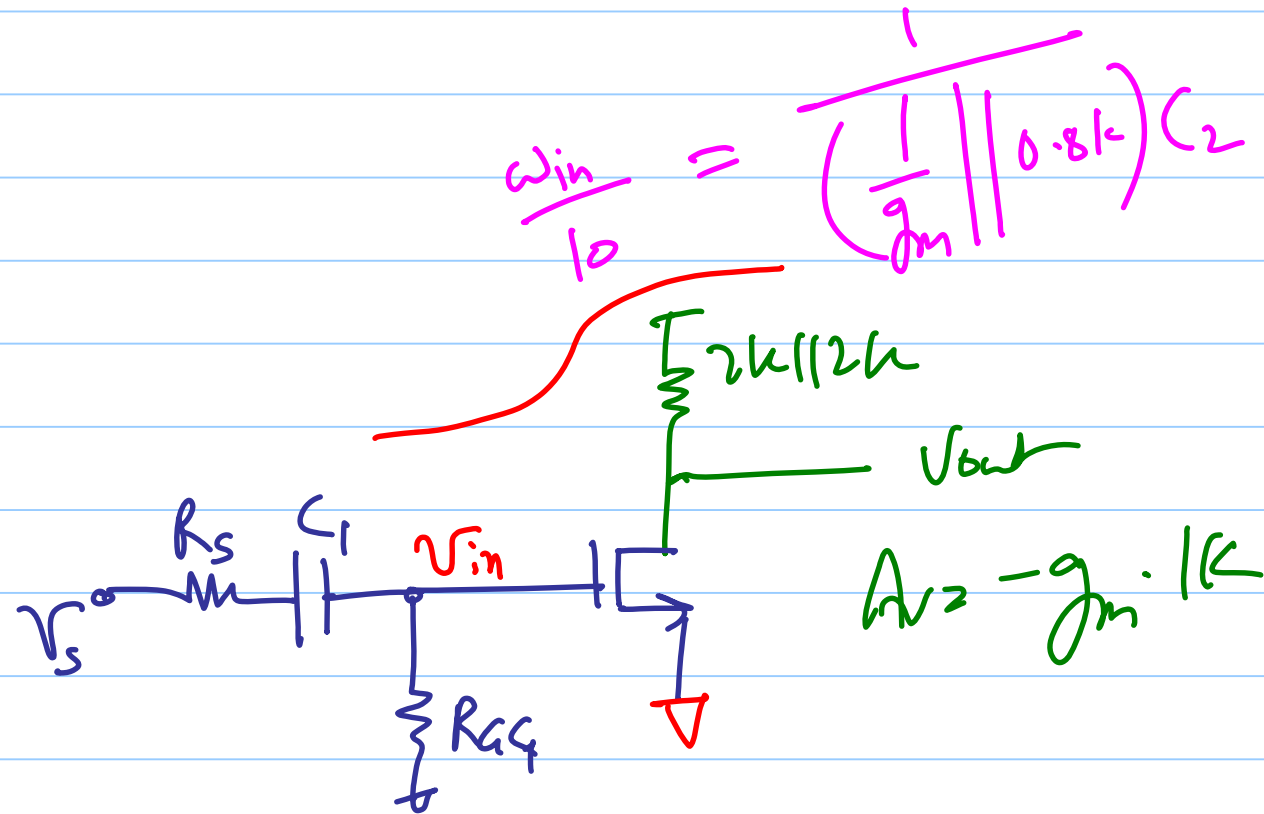
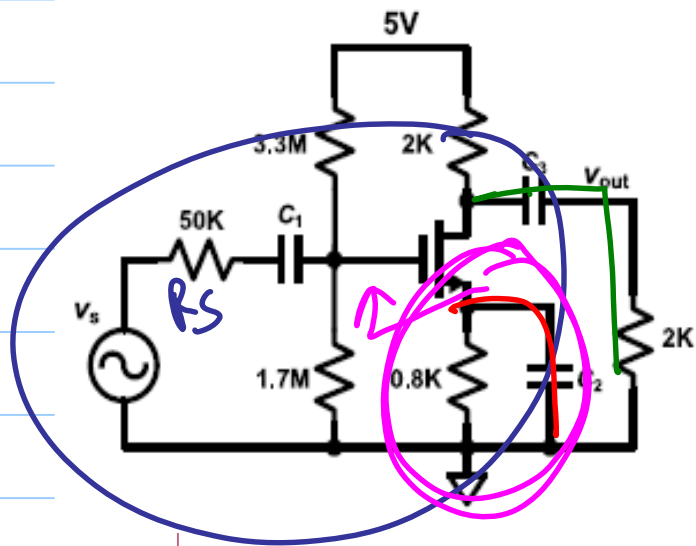
$$=$$

$$g_m = g_{m1} + g_{m2}$$

$$= \left(\frac{g_{m1}}{1 + g_{m1}R_S} \right) + \left(\frac{g_{m2}}{1 + \frac{g_{m2}}{g_{m3}}} \right)$$



Problem 2



$$\frac{V_{in}}{V_s} \Rightarrow \text{time-constant} \quad (R_s + R_{gs}) C_1$$

$$\frac{1}{(R_s + R_{gs}) C_1} < \frac{\omega_{in}}{10}$$