

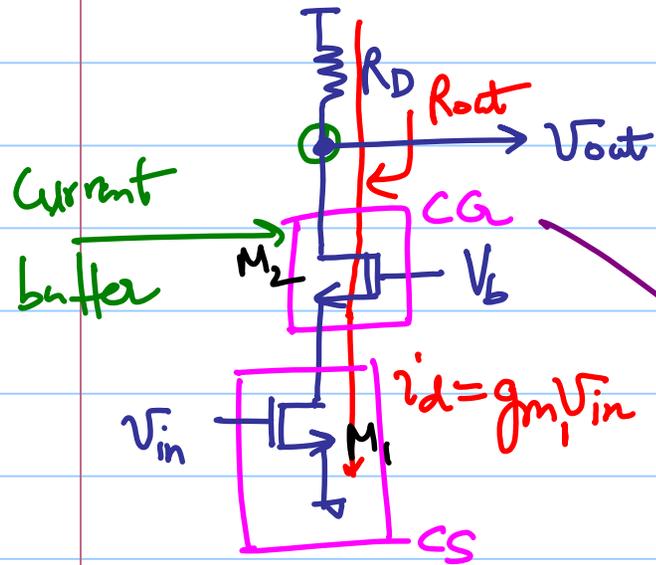
ECE 511 - Lecture 16

Note Title

3/18/2014

HW#6 due
April 1st

Cascode Amplifier.



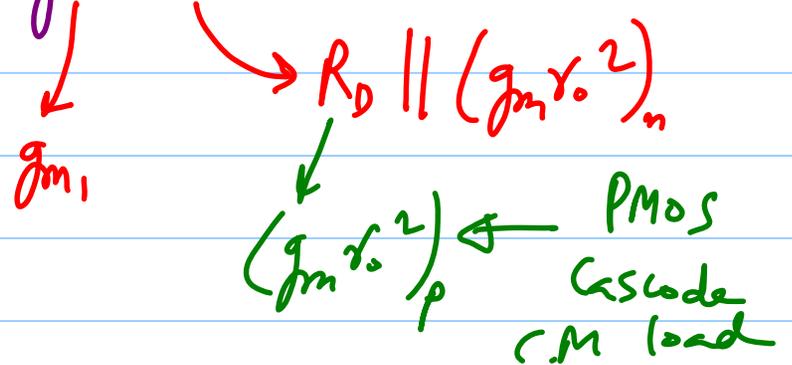
transconductance shoring by
the o/p to ground

Lemma:

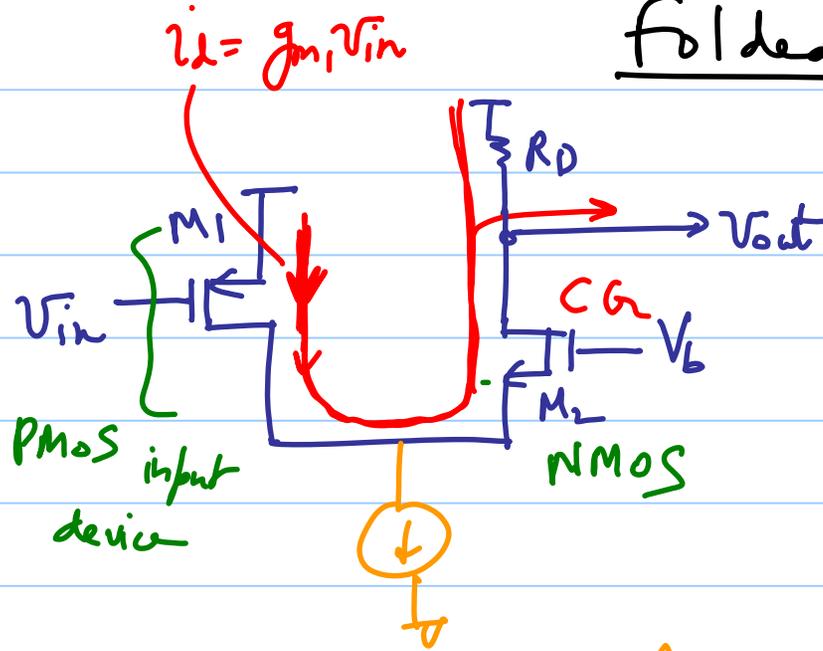
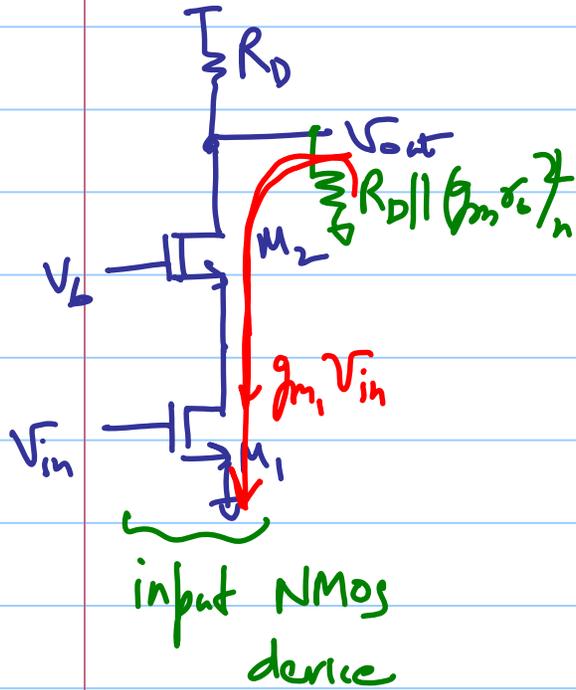
$$A_v = -g_{m1} \cdot R_{out}$$

o/p impedance
when $V_{in} > 0$

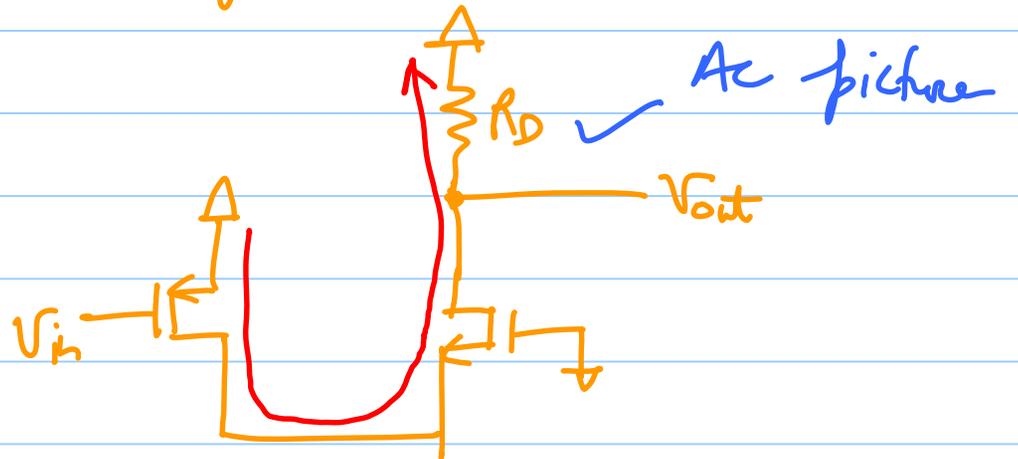
$$A_v = -g_{m1} \cdot R_{out}$$

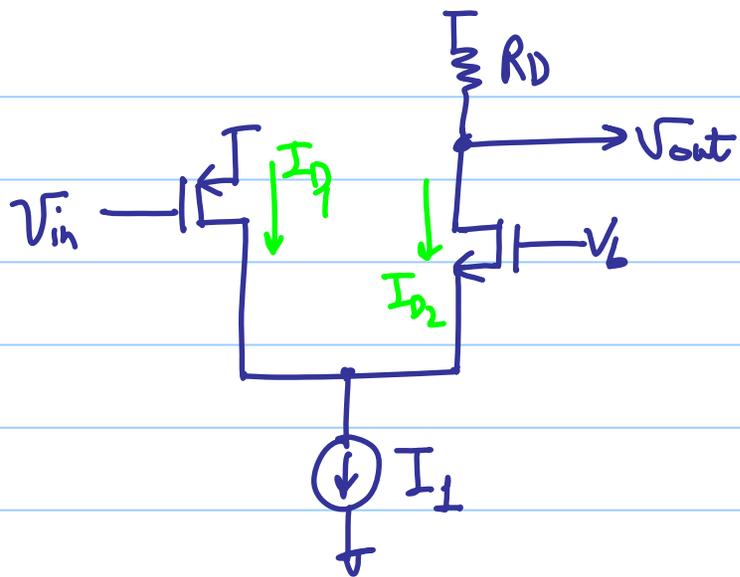


Folded Cascode Amplifier



Small signal current is folded up

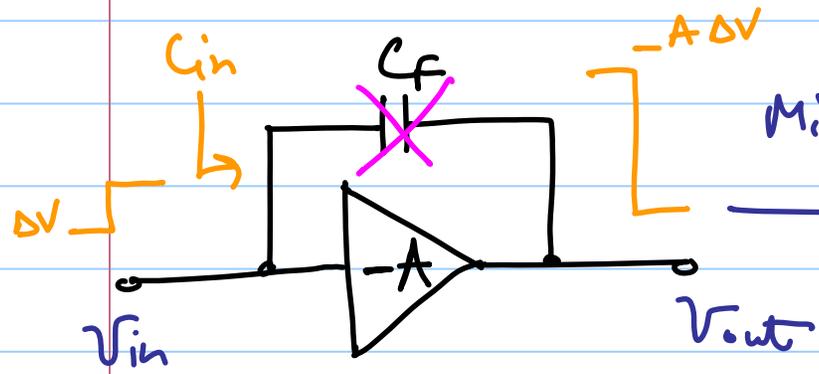




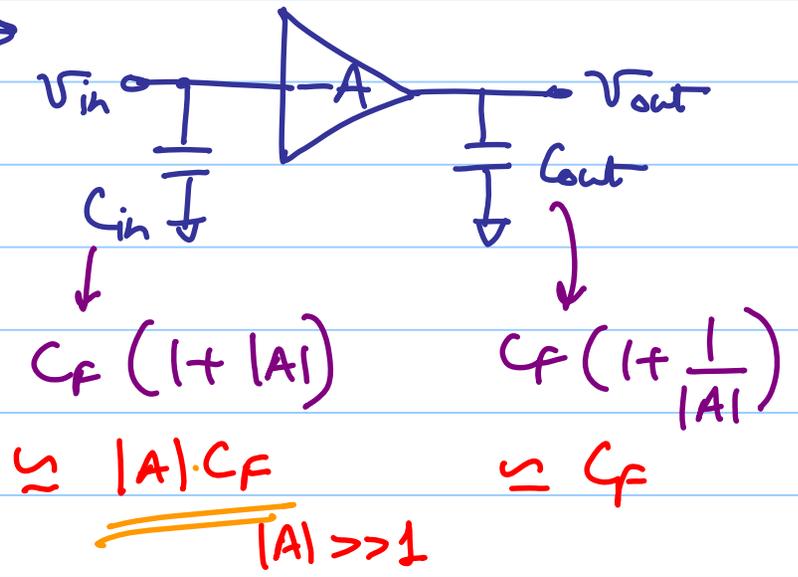
* 2x bias current
↓
($I_{D1} + I_{D2}$)

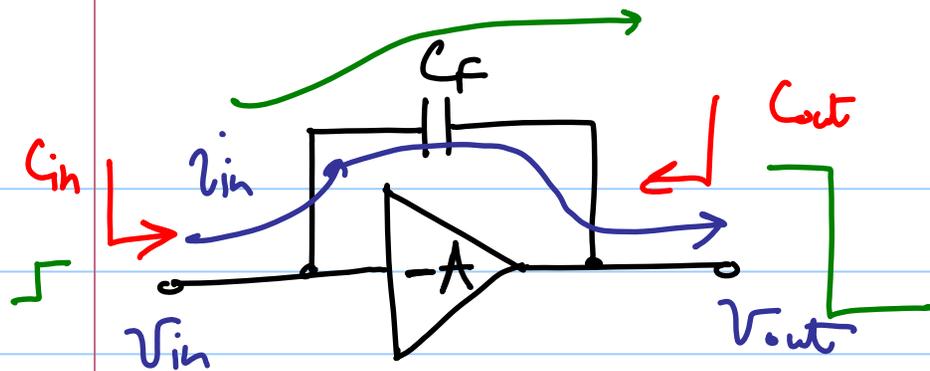
* better headroom

Miller Effect:



Miller Theorem





ξ . input capacitance is multiplied by $|A|$

$$\begin{aligned}
 i_{in} &= \frac{V_{in} - V_{out}}{1/sC_f} = sC_f (V_{in} - V_{out}) \\
 &= sC_f (V_{in} + |A|V_{in}) \\
 &= \underbrace{sC_f (1 + |A|)}_{C_{in}} \cdot V_{in} \\
 &= (sC_{in}) V_{in}
 \end{aligned}$$

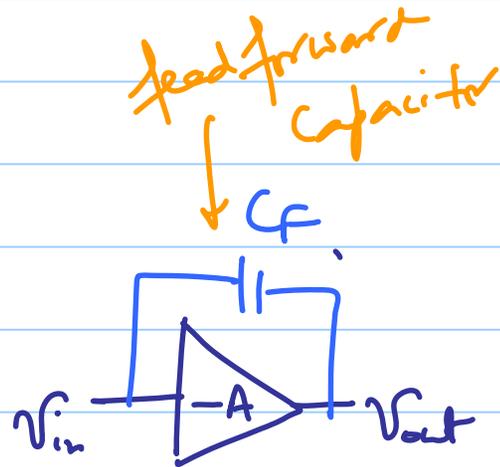
$\leftarrow -AV_{in}$

$$C_{in} = (1 + |A|) C_f$$

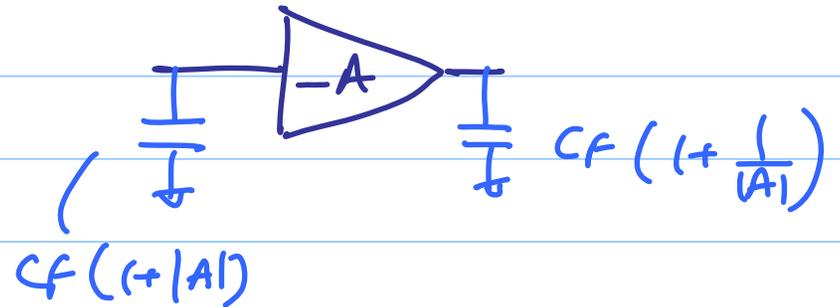
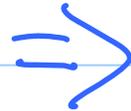
$$\begin{aligned}
 i_{out} &= -i_{in} = -sC_f (V_{in} - V_{out}) \\
 &= -sC_f \left(\frac{-V_{out}}{|A|} - V_{out} \right)
 \end{aligned}$$

$$i_{out} = \underbrace{sC_f \left(1 + \frac{1}{|A|} \right)}_{C_{out}} V_{out}$$

$$C_{out} = \left(1 + \frac{1}{|A|}\right) C_f \approx C_f$$



approximation



* What happen at $\omega \rightarrow \infty$

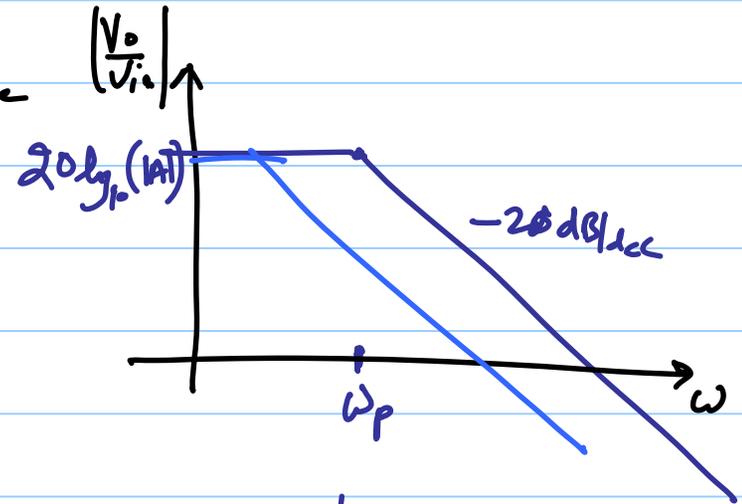
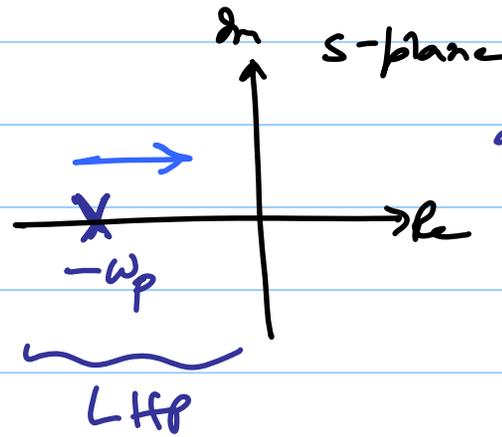
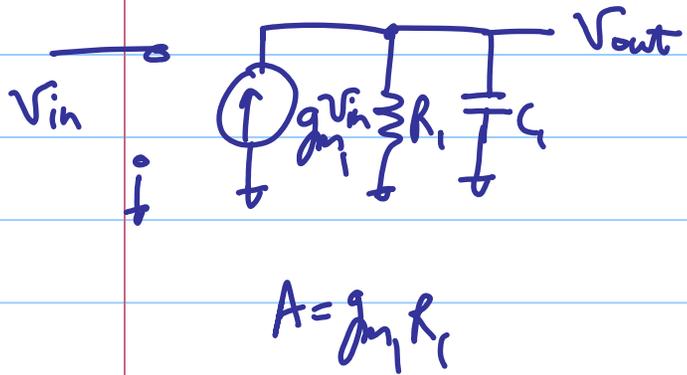
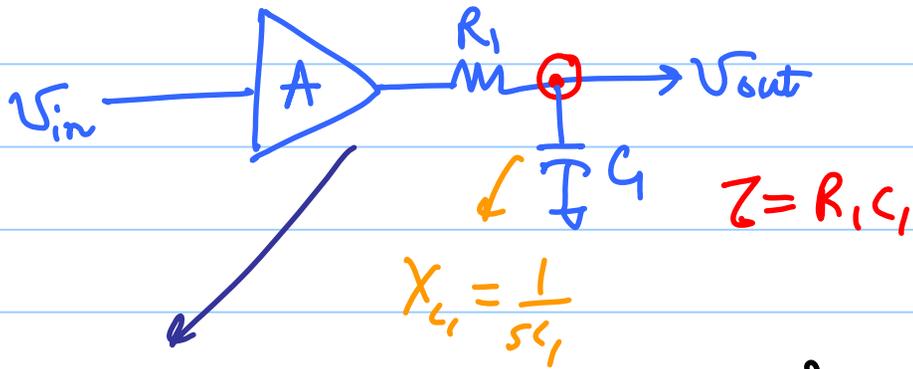
useful in analysis

* misses a zero in the T.F.

Poles \leftrightarrow Nodes

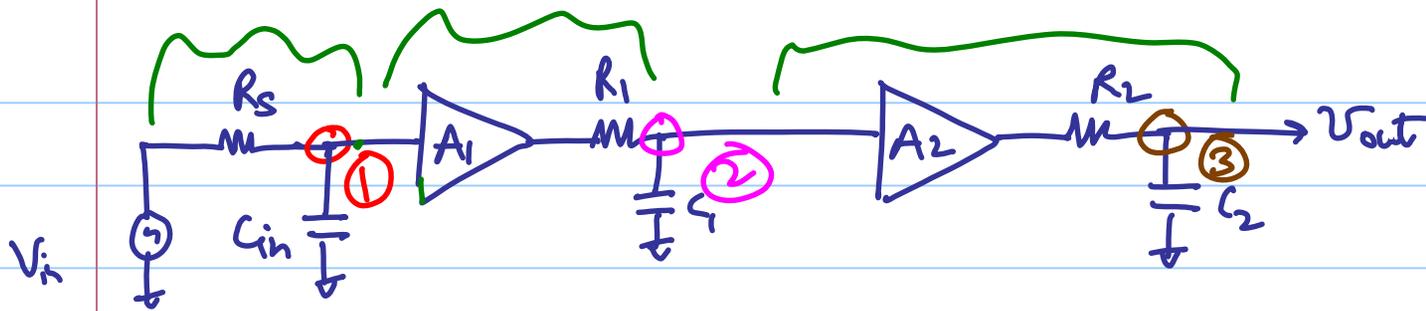
$$\frac{V_{out}}{V_{in}}(s) = \frac{A}{1 + sR_1C_1}$$

$$= \frac{A}{1 + \frac{s}{\omega_p}} \quad \text{pole}$$



$$\omega_p = \frac{1}{R_1 C_1} \quad \checkmark$$

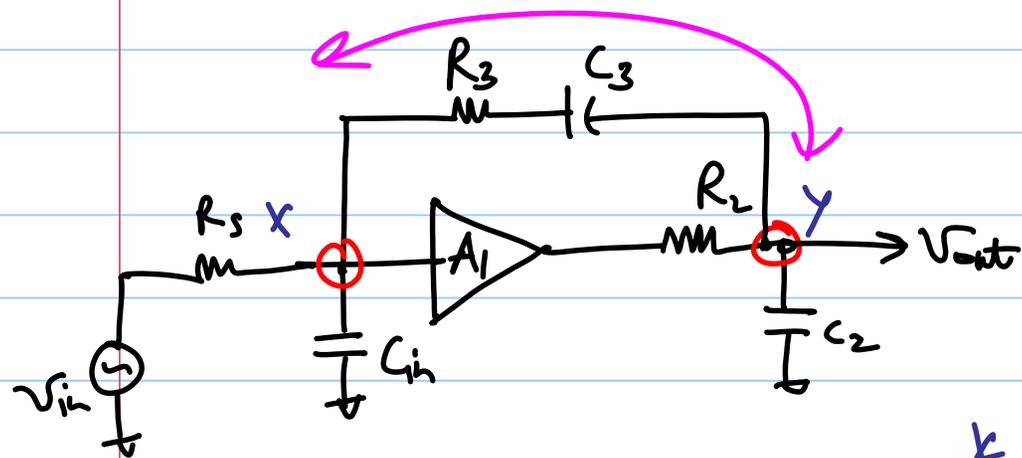
$$f_p = \frac{1}{2\pi R_1 C_1}$$



$$H(s) = \frac{V_{out}}{V_{in}}(s) = \frac{1}{(1 + sR_sC_{in})} \cdot \frac{A_1}{(1 + sR_1C_1)} \cdot \frac{A_2}{(1 + sR_2C_2)}$$

3 poles

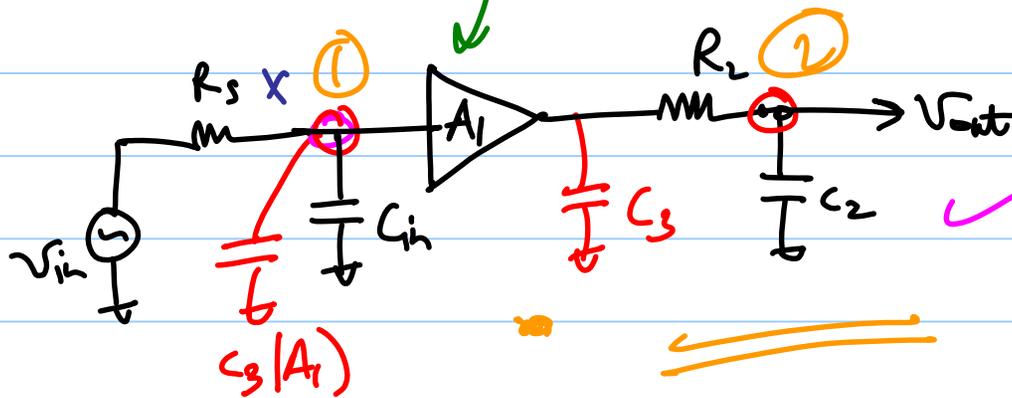
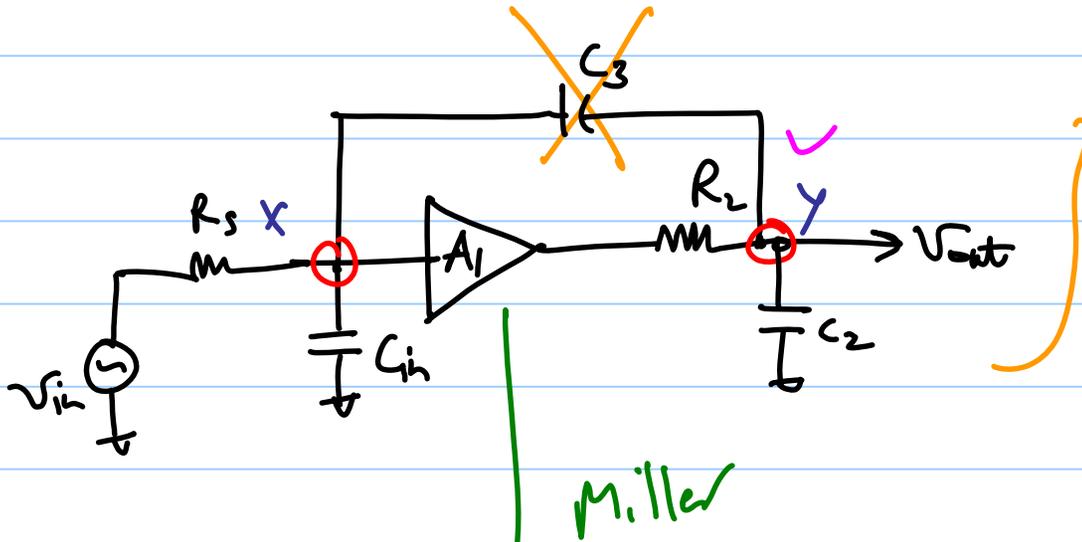
each node contributes n pole to the transfer function



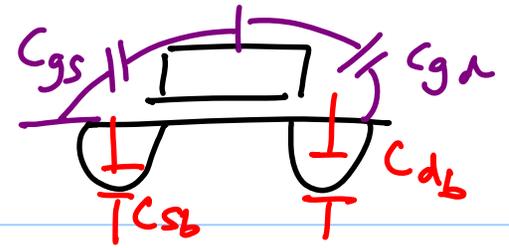
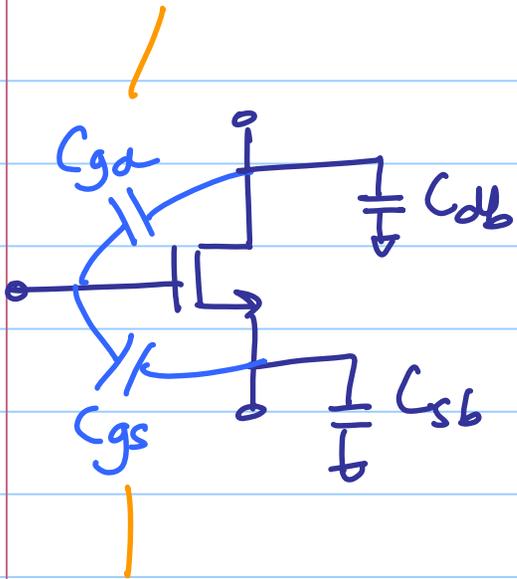
nodes X & Y are interacting through R_3 & C_3

↳ In general can't associate a pole to a node

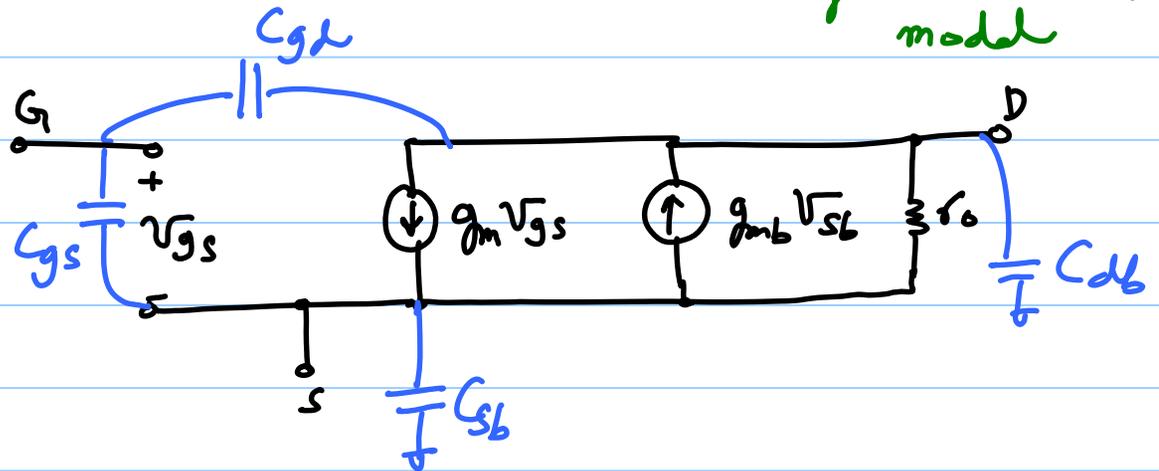
* All poles are contributed by all interacting nodes in the circuit



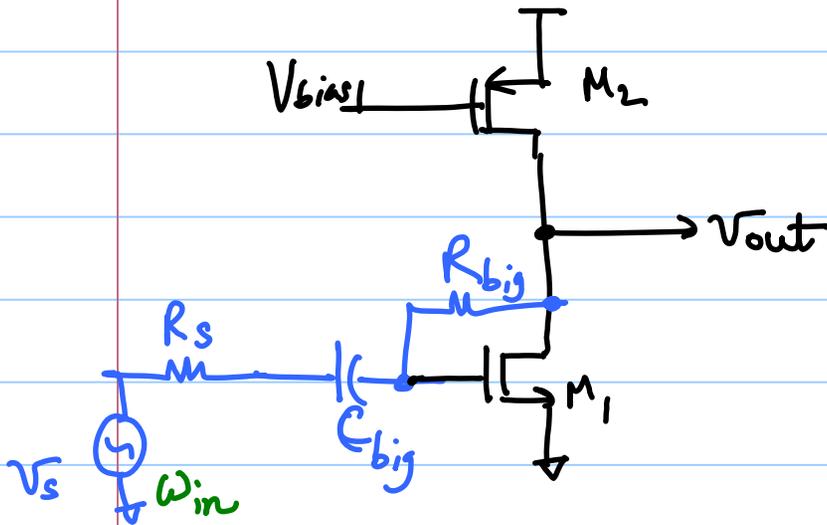
ok for intuition
 but may not
 always be accurate



high-frequency small-signal model



CS Stage

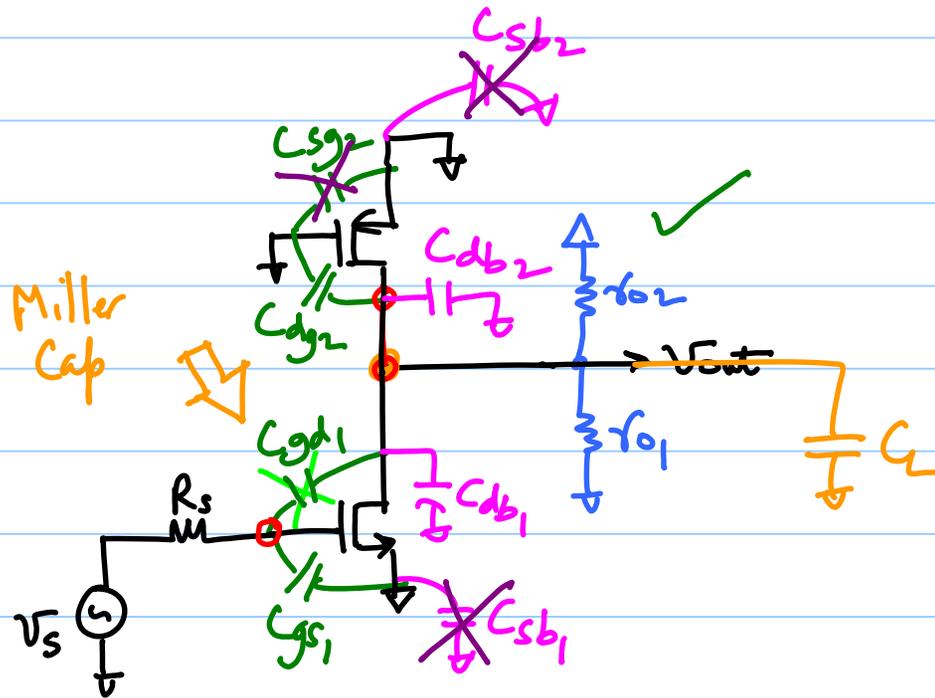


$$A_v = -g_{m1}(r_{o1} \parallel r_{o2})$$

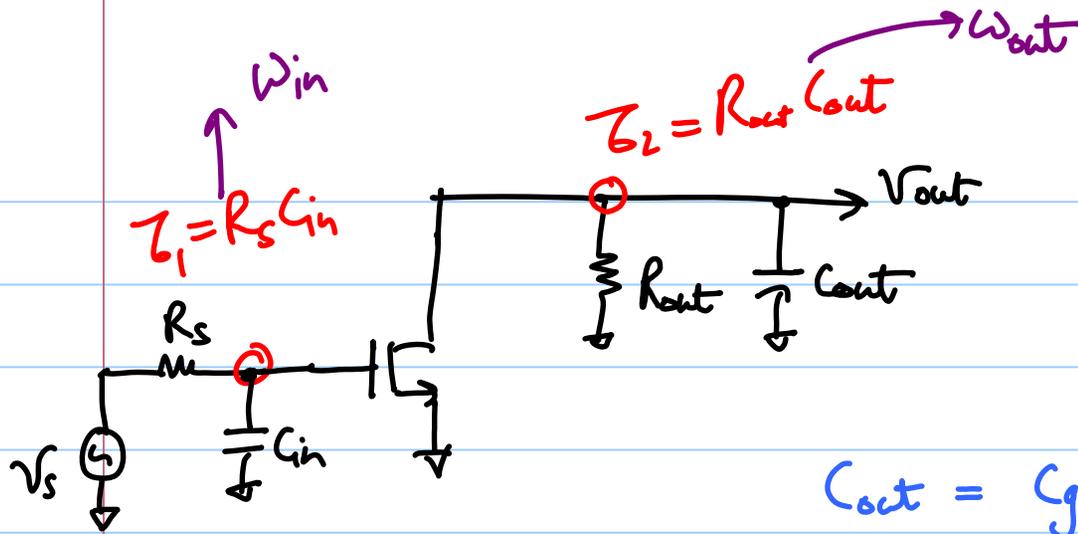
low-freq gain

$$\omega_0 = \frac{1}{R_{big} C_{big}} \ll \omega_{in}$$

Az picture with parasitic Caps



Let's use Miller appx.
and derive quick
results



$$R_{out} = r_{o1} \parallel r_{o2}$$

$$C_{in} = C_{gs1} + C_{gd1} (1 + |A|)$$

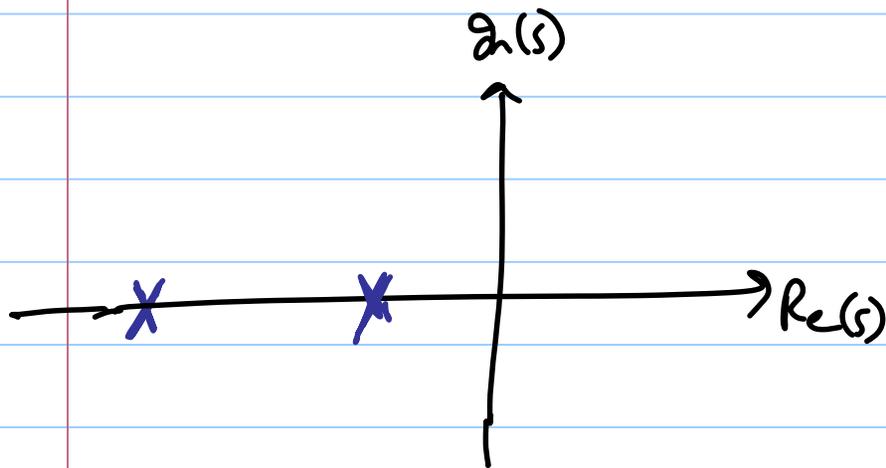
$$C_{out} = C_{gd1} \left(1 + \frac{1}{|A|}\right) + C_{db1} + C_{db2} + C_{dg2}$$

$$\omega_{in} = \frac{1}{R_s C_{in}} = \frac{1}{R_s [C_{gs1} + (1 + |A|) C_{gd1}]} \rightarrow \infty \quad R_s \ll 0$$

$$\omega_{out} = \frac{1}{R_{out} C_{out}} = \frac{1}{(r_{o1} \parallel r_{o2}) [C_{gd1} + C_{db} + C_{dg2} + C_L]} \quad \text{low-freq pole}$$

$$\approx \frac{1}{(r_{o1} \parallel r_{o2}) C_L}$$

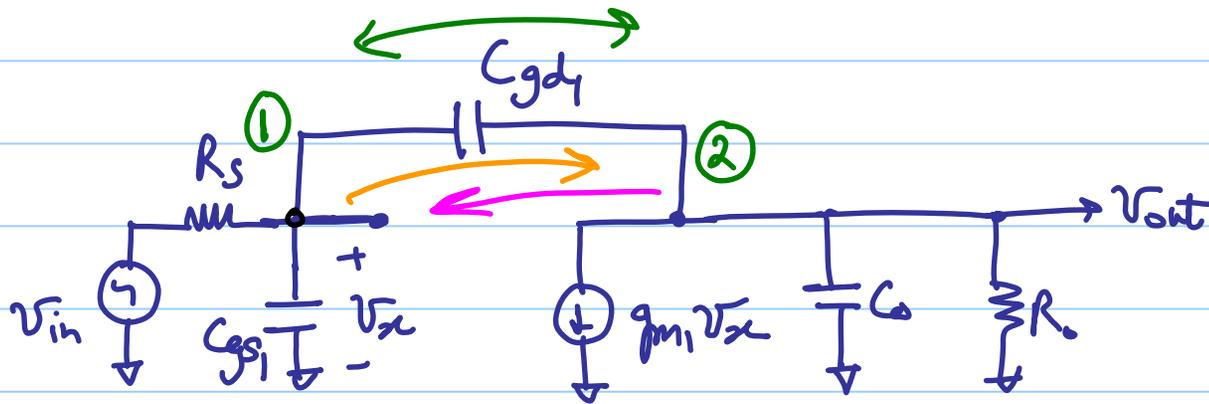
$$\frac{V_{out}}{V_{in}}(s) \approx \frac{A_v \rightarrow -g_{m1}(r_{o1} \parallel r_{o2})}{\left(1 + \frac{s}{\omega_{in}}\right) \left(1 + \frac{s}{\omega_{out}}\right)} \quad \checkmark$$



"Miller approx. doesn't capture the zero"

Draw Equivalent Circuit

$$R_o = r_{o1} || r_{o2}$$
$$C_o = C_{db} + C_{d2}$$



Evaluate T.F.

$$\frac{V_{out}(s)}{V_{in}(s)}$$

Write Nodal Equations @ ① & ②

KCL

$$\textcircled{1} \Rightarrow \frac{V_x - V_{in}}{R_s} + V_x C_{gs1} s + \underline{(V_x - V_{out}) C_{gd1} s} = 0$$

$$\textcircled{2} \Rightarrow \underline{(V_{out} - V_x) \cdot C_{gd1} s} + g_{m1} V_x + V_{out} \left(\frac{1}{R_o} + C_o s \right) = 0$$