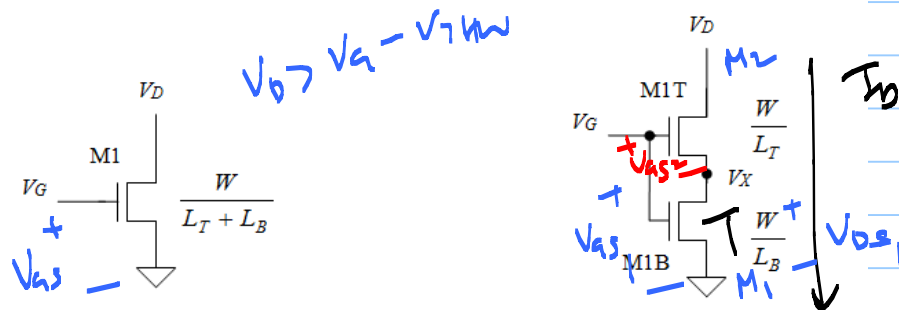


ECE 511 - Lecture 9

Note Title

2/19/2013



for M_1 in sat:

$$V_{DS1} > V_{GS1} - V_{THW}$$

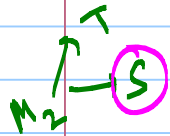
$$V_{GS1} - V_{AS1} > V_{GS1} - V_{THW}$$

$$V_{AS1} < V_{THW}$$

M₁ Triode

$$I_{D1} = k p_n \frac{W}{L_B} \cdot \left[(V_{G5} - V_{THW}) V_x - \frac{V_x^2}{2} \right]$$

$$I_{D1} \cdot L_B = k p_n W \left[(V_G - V_{THW}) V_x - \frac{V_x^2}{2} \right] \rightarrow \textcircled{1}$$

M₂ 

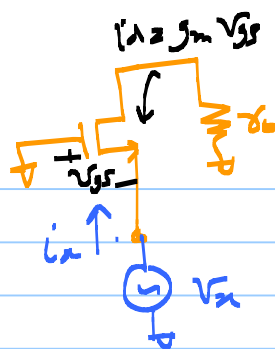
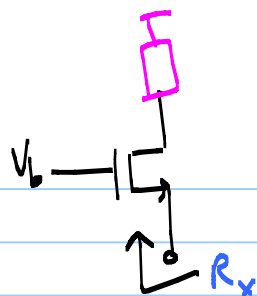
$$I_{D2} = \frac{k p_n W}{2 L_A} (V_G - V_x - V_{THW})^2$$

$$I_{D2} \cdot L_A = \frac{k p_n W}{2} \underbrace{(V_G - V_x - V_{THW})^2}_{(a+b)^2} \rightarrow \textcircled{2}$$

Add ① + ②

$$I_D (L_A + L_B) = k p_n W \left\{ \cancel{(V_G - V_{THW}) V_x} - \cancel{\frac{V_x^2}{2}} + \frac{1}{2} (V_G - V_{THW})^2 + \cancel{\frac{V_x^2}{2}} - \cancel{\frac{2}{2} (V_G - V_{THW}) V_x} \right\}$$

$$\Rightarrow I_D = \frac{k p_n \cdot W}{2(L_A + L_B)} [V_G - V_{THW}]^2$$



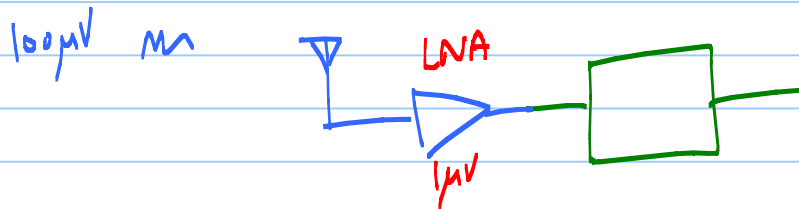
ignoring
 g_{mb}

$$KVL \Rightarrow v_{gs} = -v_x \rightarrow \textcircled{1}$$

$$i_x = -i_d = -g_m v_{gs} = g_m v_x$$

$$R_x = \frac{1}{g_m} \quad \frac{1}{g_m + g_{mb}}$$

Single-Stage Amplifiers



Input output characteristics of an amplifier

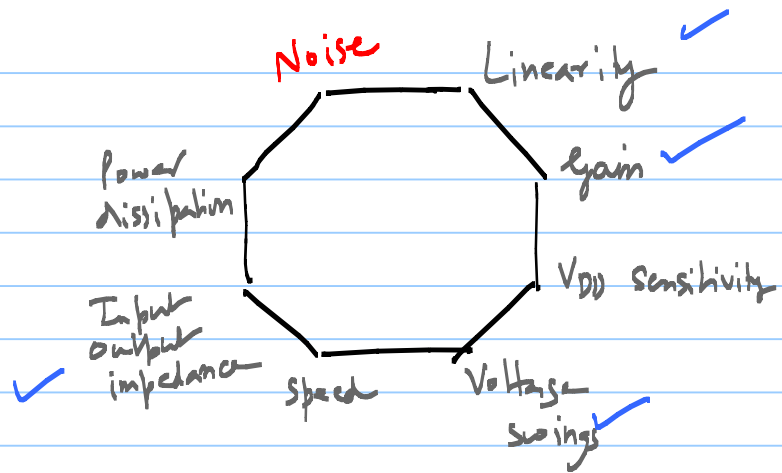
$$x(t) \rightarrow \text{Amplifier} \rightarrow y(t) = f(x(t))$$

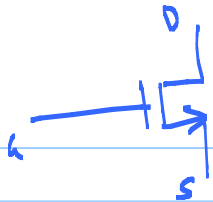
$$y(t) = \alpha_0 + \boxed{\alpha_1} x(t) + \alpha_2 x^2(t) + \alpha_3 x^3(t) + \dots$$

$\uparrow$ off DC-level $\leftarrow$ small signal gain $\leftarrow$ distortion terms

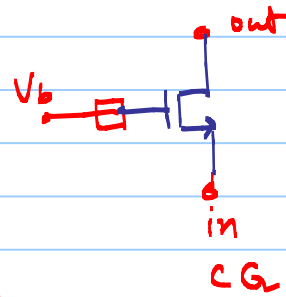
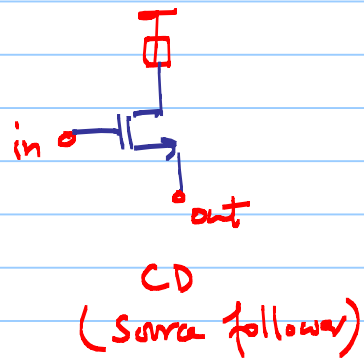
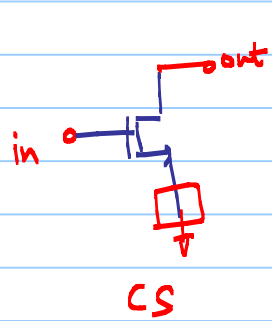
for "small-signal" $\Delta y = \alpha_1 \Delta x \leftarrow$ small signal signal

if $x(t)$ starts increasing in Amplitude





VCCS in
small signal



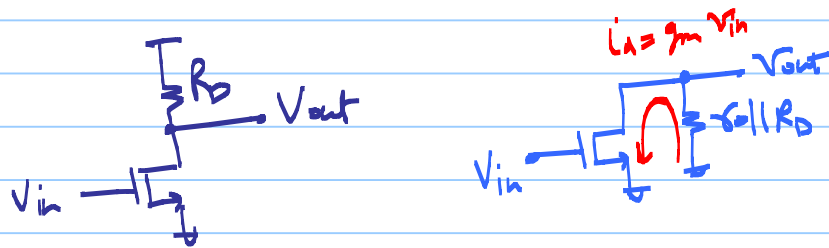
$$3P_2 = \cancel{X}$$

$$3C_2 = 3$$

Drain can't be
on input

* 3 basic configurations & their combinations

Common Source Stage

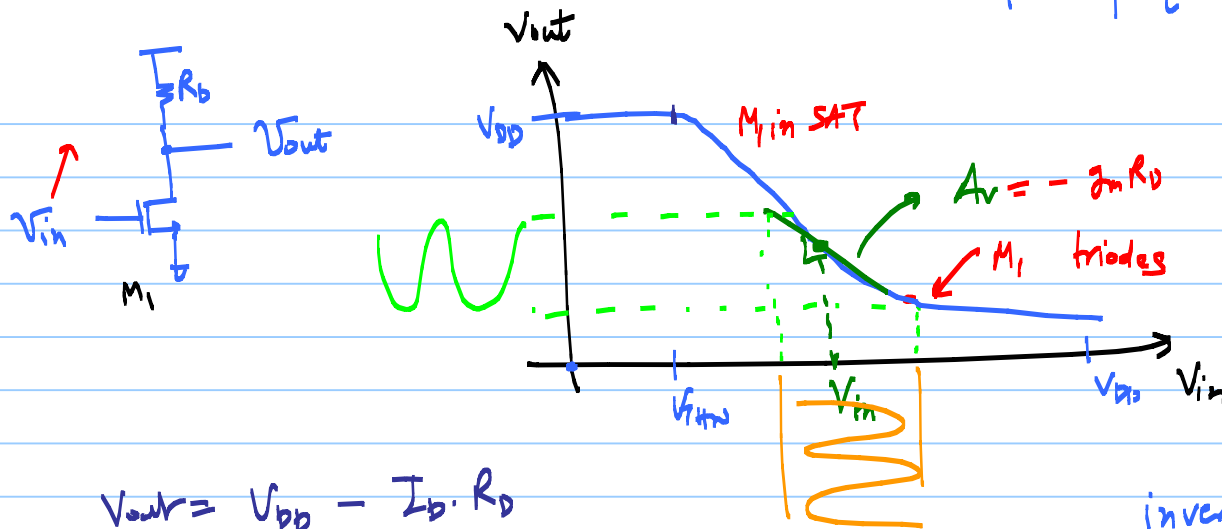


$$V_{out} = -g_m V_{in} (r_o \parallel R_D)$$

$$A_v = -g_m (R_D \parallel r_o)$$

$$\approx -g_m R_D \quad \text{for } R_D \ll r_o$$

low-freq behavior

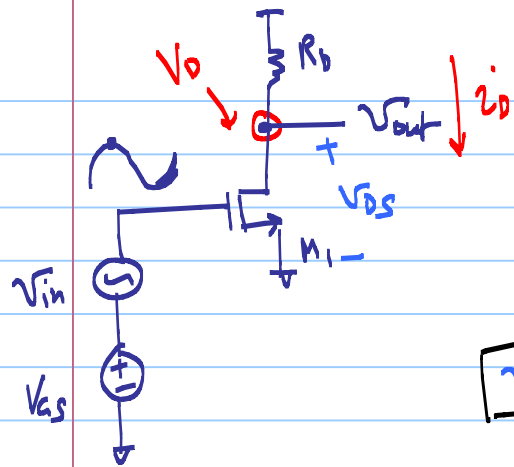


$$V_{out} = V_{DD} - I_D \cdot R_D$$

$$V_{out} = V_{DD} - R_D \cdot \frac{k_n}{2} \frac{W}{L} (V_{in} - V_{thn})^2$$

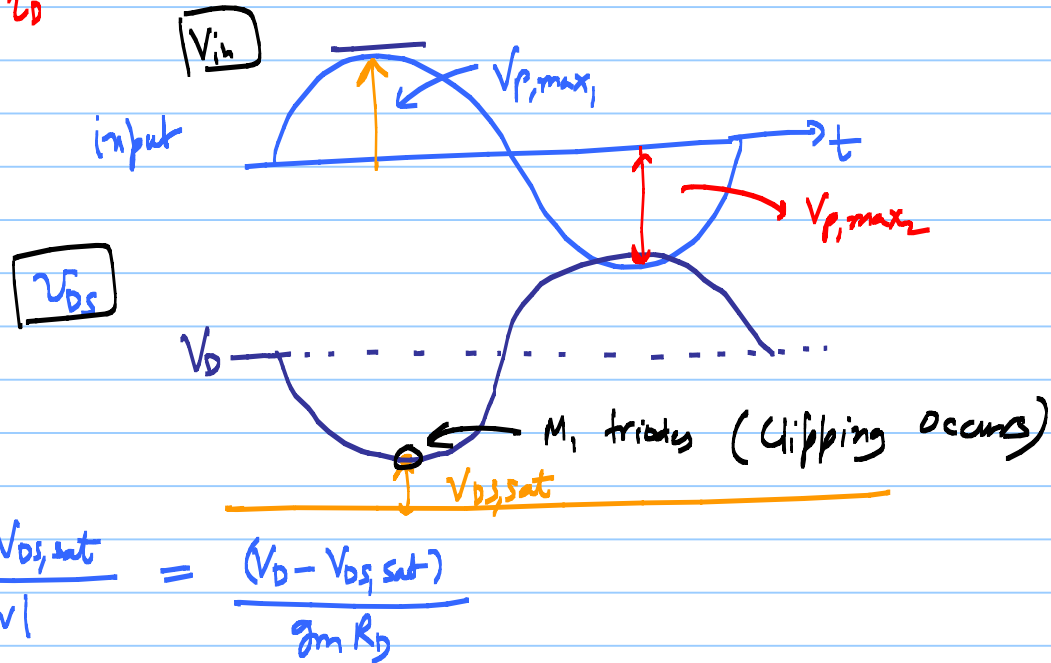
$$A_v = \frac{\partial V_{out}}{\partial V_{in}} = -g_m R_D$$

inverting amplifier
 V_{out} is 180° out of phase

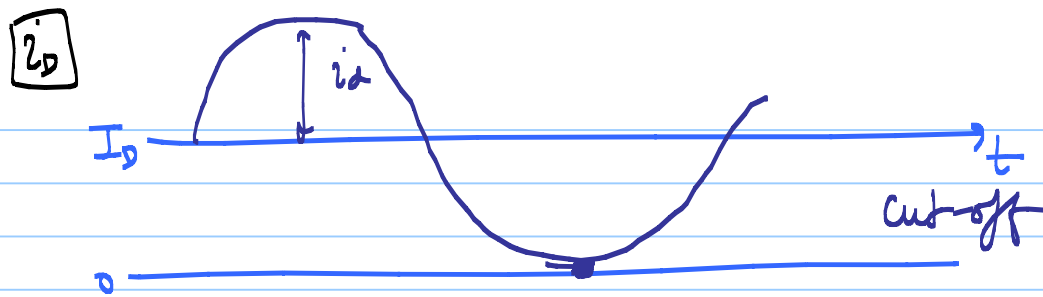


$$v_{out} = - \frac{g_m (R_D || r_o)}{A_v} v_{in}$$

Assume linear behavior



$$V_{p,max} = \frac{V_D - V_{D,sat}}{|A_v|} = \frac{(V_D - V_{D,sat})}{g_m R_D}$$



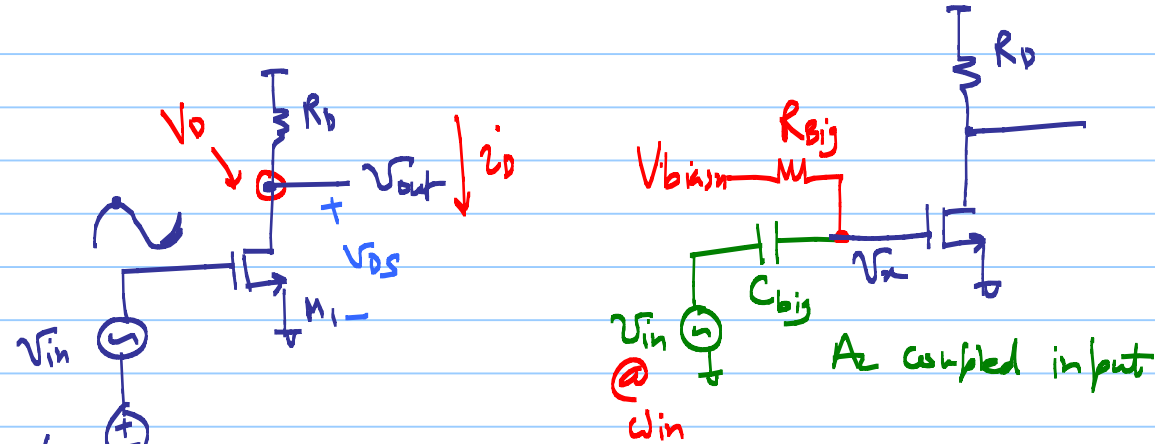
$$i_a \quad i_a = -I_D$$

$$g_m V_{p,max} = -I_D$$

$$|V_{p,max}| = \frac{I_D}{g_m}$$

$$\text{input amplitude} < \min \{ V_{p,max_1}, V_{p,max_2} \}$$

Note:



Ac coupled input

