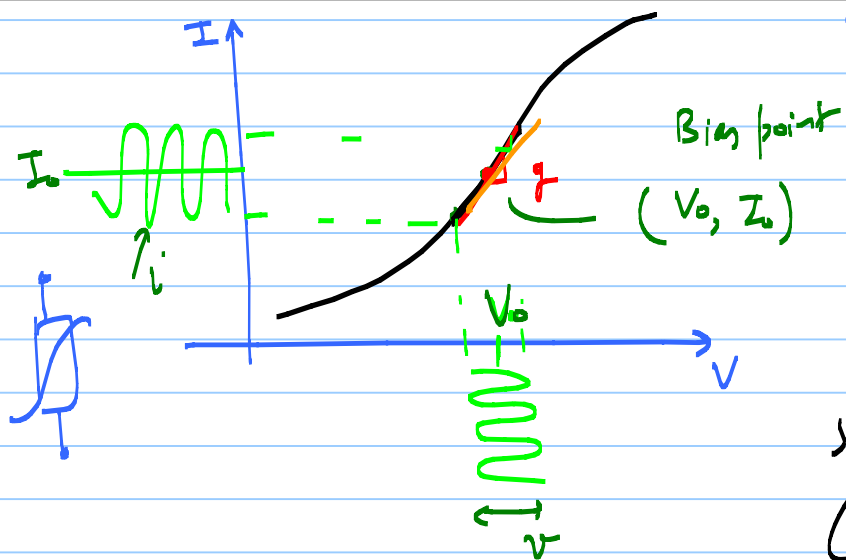


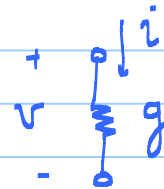
ECE 511 - Lecture 2

Note Title

1/24/2013



$$I = f(v)$$



Linearizing about the bias point

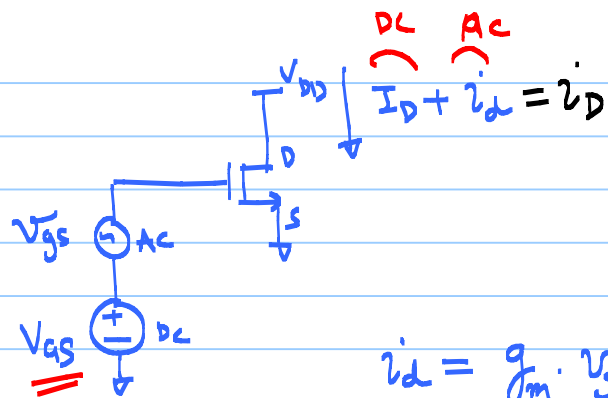
Small signal
 $i = gv$

$$g = \left. \frac{dI}{dv} \right|_{v=V_0}$$

slope bias point

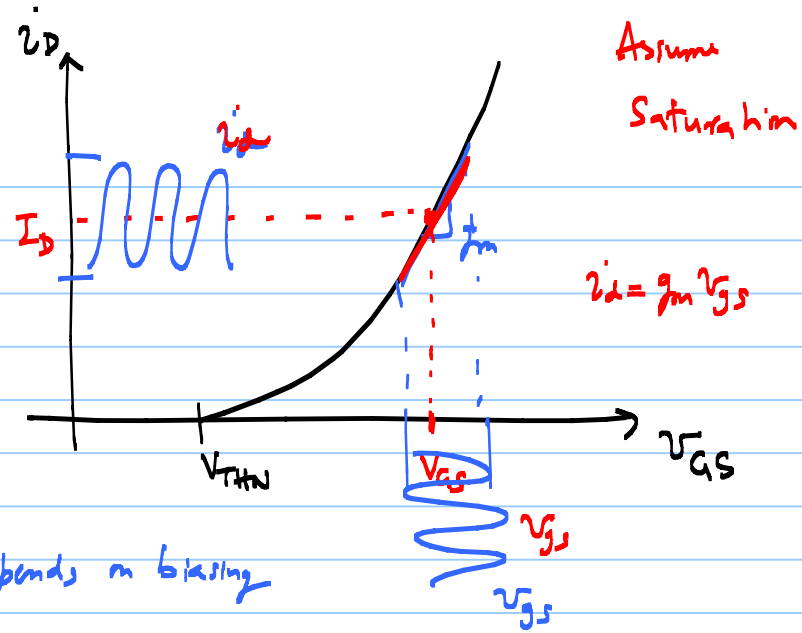
"Small-signal equivalent circuit"

NMOS in Saturation



$$i_d = g_m \cdot v_{gs}$$

depends on biasing



$$i_D = \frac{k_p n}{2} \frac{W}{L} (V_{GS} - V_{THN})^2$$

$$\underbrace{I_D}_{DC} + \underbrace{2i_d}_{AC} = \frac{k_p n}{2} \frac{W}{L} \left(\underbrace{V_{GS}}_{DC} + \underbrace{v_{gs}}_{AC} - V_{THN} \right)^2$$

$$i_d = g_m v_{gs}$$

$$g_m = \left. \frac{\partial i_D}{\partial V_{GS}} \right|_{V_{GS} = V_{GS}}$$

(AC)
Small-signal parameter

$$= \frac{k_p n}{2} \cdot \frac{W}{L} \cdot 2 (V_{GS} - V_{THN}) \bigg|_{V_{GS} = V_{GS}}$$

$$g_m = \frac{k_p n}{2} \cdot \frac{W}{L} (V_{GS} - V_{THN})$$

$$g_m = \beta (V_{GS} - V_{THN}) = \beta V_{OV}$$

$$g_m = \beta (V_{GS} - V_{THN}) \longrightarrow \textcircled{1}$$

$$= \beta \cdot \sqrt{\frac{2I_D}{\beta}} = \sqrt{2\beta I_D} \longrightarrow \textcircled{2}$$

$$= \beta (V_{GS} - V_{THN})$$

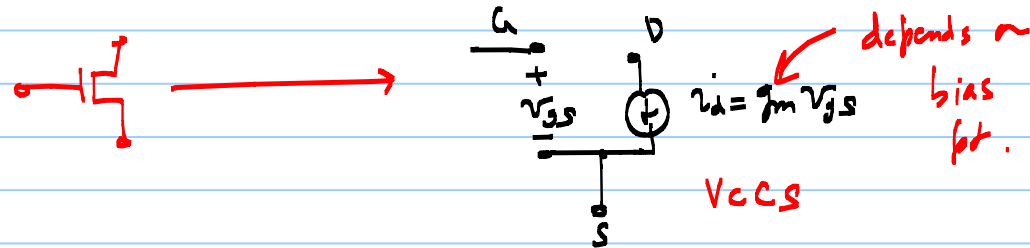
$$= \frac{2I_D}{(V_{GS} - V_{THN})^2} \cdot (V_{GS} - V_{THN}) = \frac{2I_D}{V_{GS} - V_{THN}} \longrightarrow \textcircled{3}$$

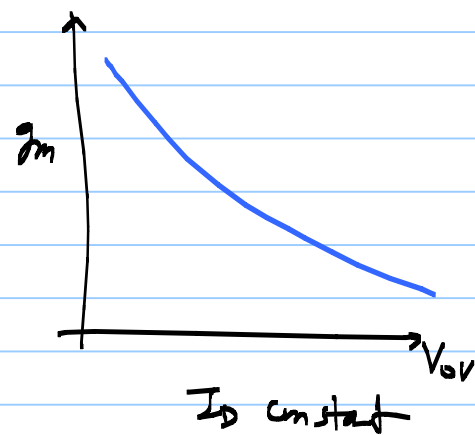
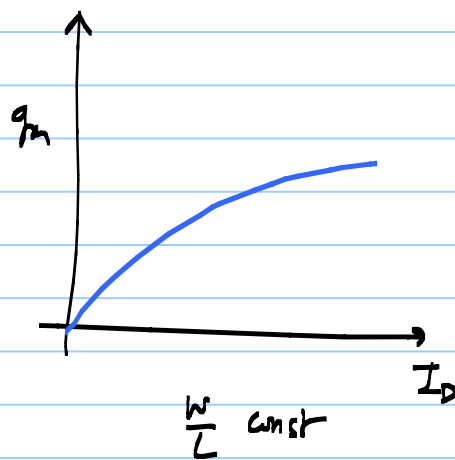
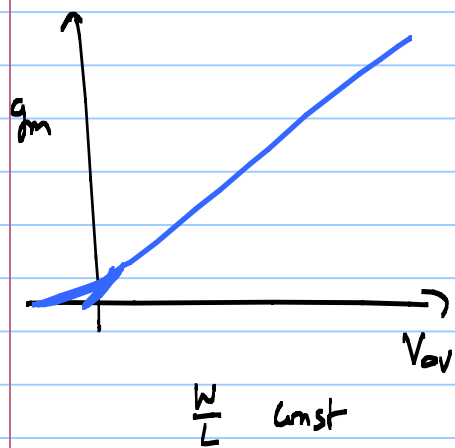
$$V_{GS} - V_{THN} = \sqrt{\frac{2I_D}{\beta}}$$

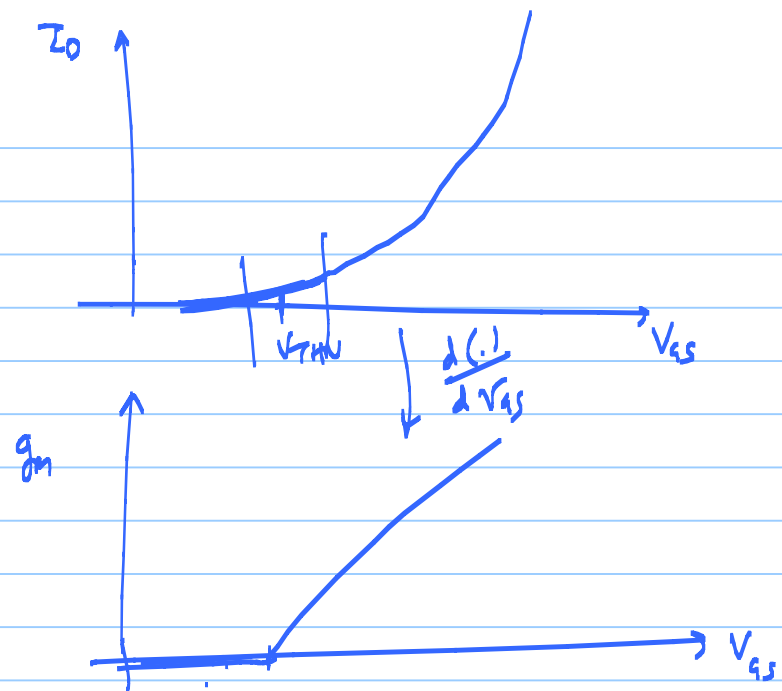
$$g_m = \beta V_{OV} = \sqrt{2\beta I_D} = \frac{2I_D}{V_{OV}}$$

$$i_d = g_m v_{gs}$$

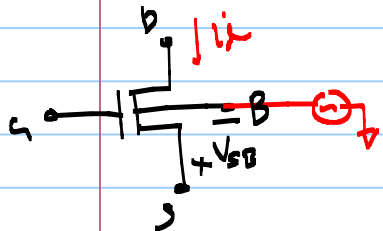
Ac Equivalent Circuit



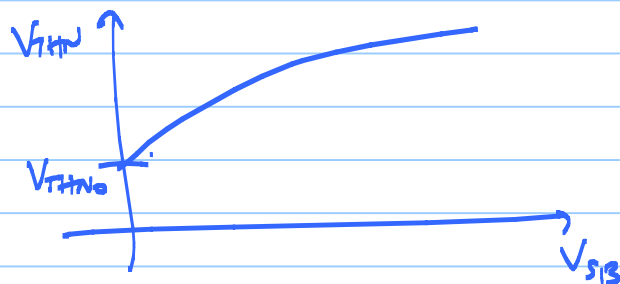




Body Effect



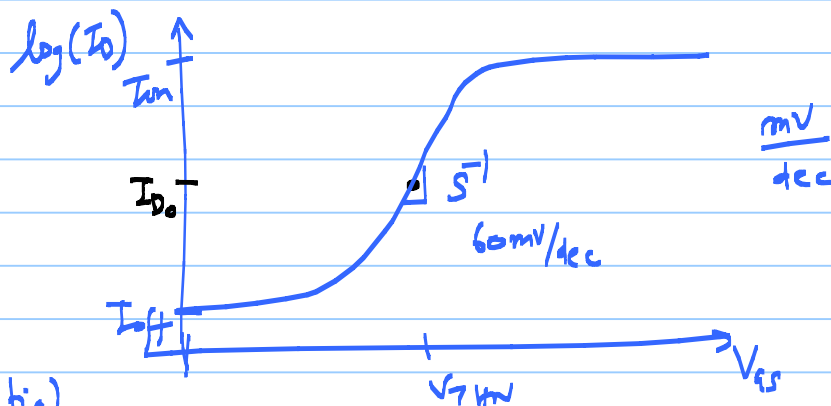
$$V_{TH}(V_{SB}) = V_{TH0} + \gamma_n \left[\sqrt{2|V_{fp}| + V_{SB}} - \sqrt{2|V_{fp}|} \right]$$

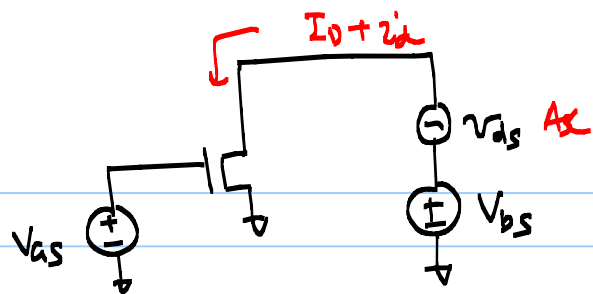


Subthreshold region

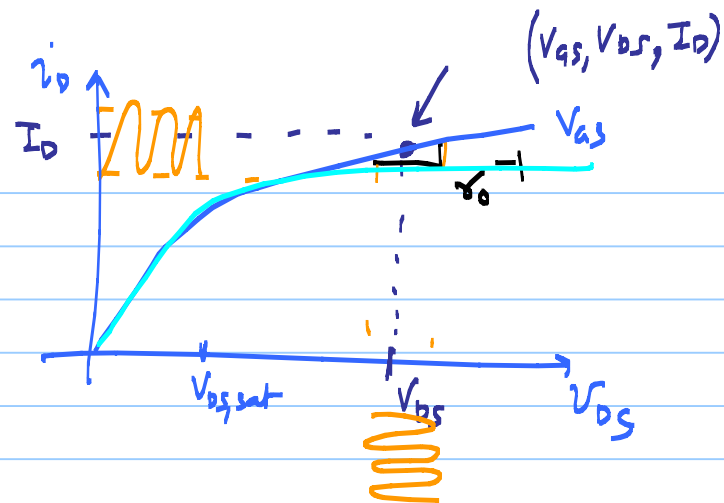
$$I_D = I_{D0} \cdot \frac{W}{L} \cdot e^{\frac{V_{GS} - V_{TH}}{n V_T}}$$

$$g_m = \frac{I_D}{n V_T} \quad \left(\text{good } \frac{g_m}{I_D} \text{ ratio} \right)$$



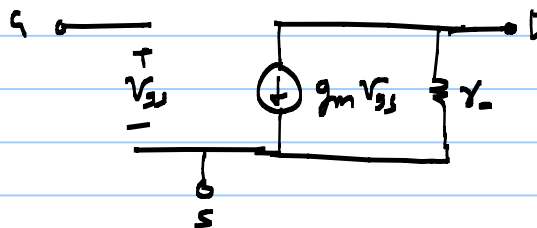


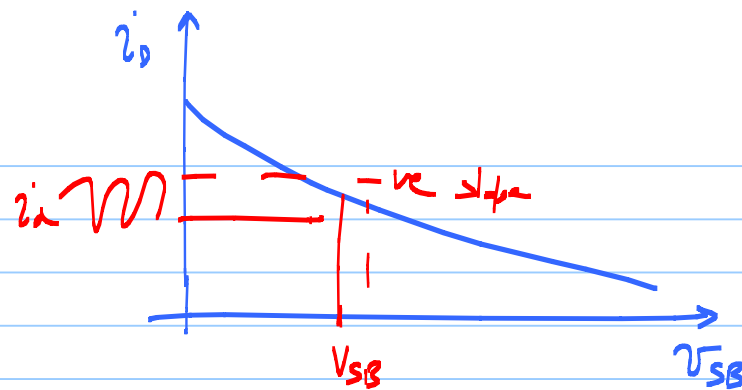
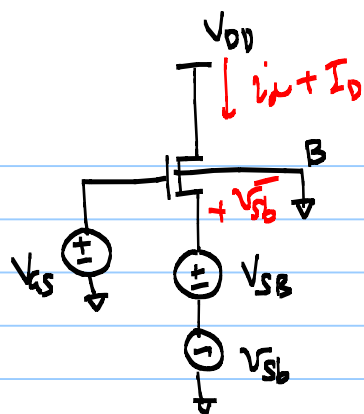
$$i_d = g_{m_s} \cdot v_{gs} = \frac{v_{ds}}{r_o}$$



$$r_o = \left(\frac{\partial i_D}{\partial v_{DS}} \bigg|_{\substack{v_{DS} = V_{DS} \\ v_{GS} = \text{const}}} \right)^{-1}$$

$$r_o = \frac{1}{\lambda I_{D,sat}}$$





$$i_D = f(V_{SB}) \quad \frac{V_{GS}}{V_{DS}} = \text{const.}$$

$$i_D = g_{mb} V_{SB}$$

$$g_{mb} = \left. \frac{\partial i_D}{\partial V_{SB}} \right|_{V_{SB}} = \frac{\partial}{\partial V_{SB}} \left[\frac{\mu_n}{2} \frac{W}{L} (V_{GS} - V_{THN})^2 \right]_{V_{SB}} \quad \text{where } i_D = f(V_{SB})$$

$$= \mu_n \cdot \frac{W}{L} (V_{GS} - V_{THN}) \left[-\frac{\partial V_{THN}}{\partial V_{SB}} \right]_{V_{SB}}$$

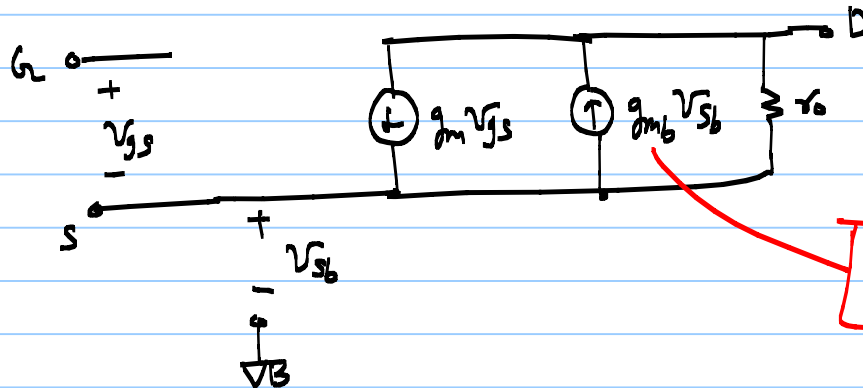
$$g_{mb} = g_m \cdot \eta$$

body
coefficient

$$\eta = -\frac{\gamma}{2} (|2V_{fb} + V_{SB}|^{-1/2})$$

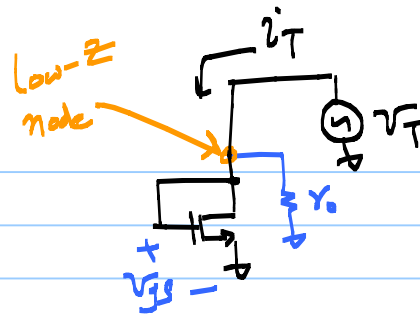
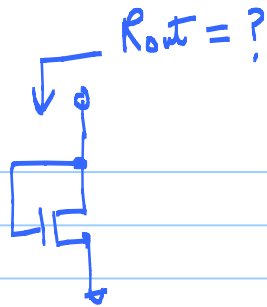
g_{mb} opposes the g_m

AC equivalent circuit



$$g_{mb} = |\eta| g_m$$

$$\eta < 1$$



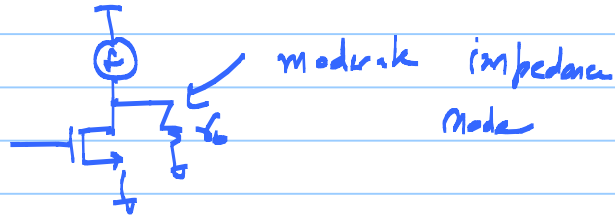
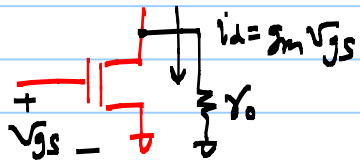
$$R_{out} = \frac{v_T}{i_T}$$

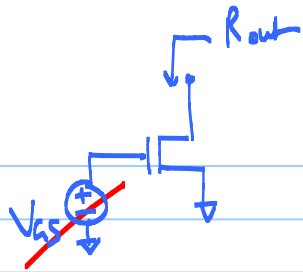
$$i_T = g_m v_T$$

$$R_{out} = \frac{v_T}{i_T} = \frac{1}{g_m} \parallel r_o$$

$$\approx \frac{1}{g_m} \approx 1k\Omega$$

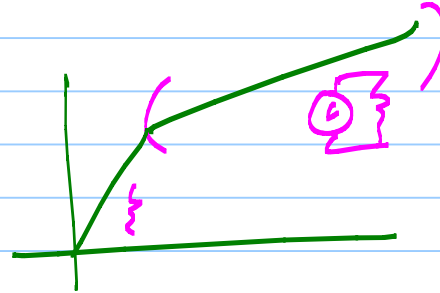
Ac

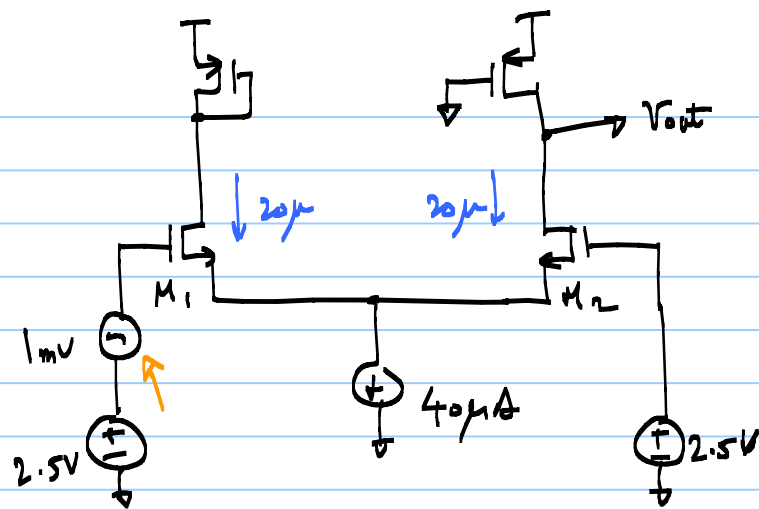




$$R_{ch} = \frac{1}{k p_n \frac{W}{L} (V_{GS} - V_{THN})}$$

$$R_{ch} < \frac{1}{g_m} \Big|_{sat}$$





① DC picture