

Lecture 27

Note Title

5/7/2013

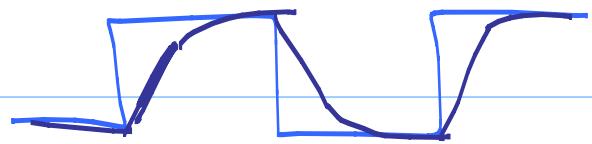
$$SR = \frac{I_{es}}{c_c} = 500 \frac{V}{\mu s} = \frac{100 \mu V}{c_c}$$

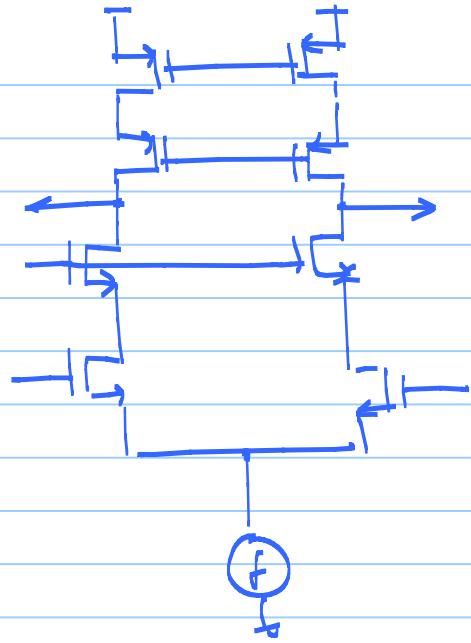
$$\Rightarrow c_c = \frac{100 \times 10^{-6} \times 10^{-6}}{500}$$

$$= 0.2 \text{ pF}$$

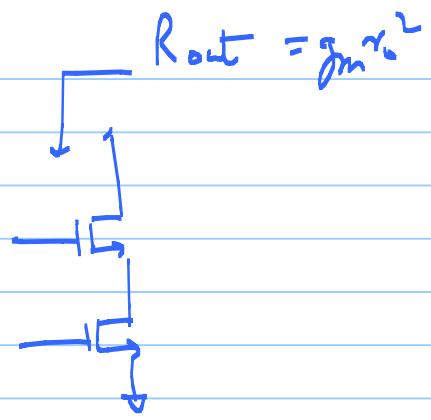
$$f_{OM_1} = \frac{f_m \cdot A_{OL}}{\text{Power}}$$

$$f_{OM_2} = \frac{SR \cdot A_{OL}}{\text{Power}}$$

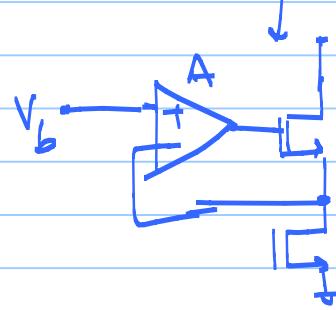




$$g_m r_o = 16$$



$$R_{out} = g_m r_o^2$$

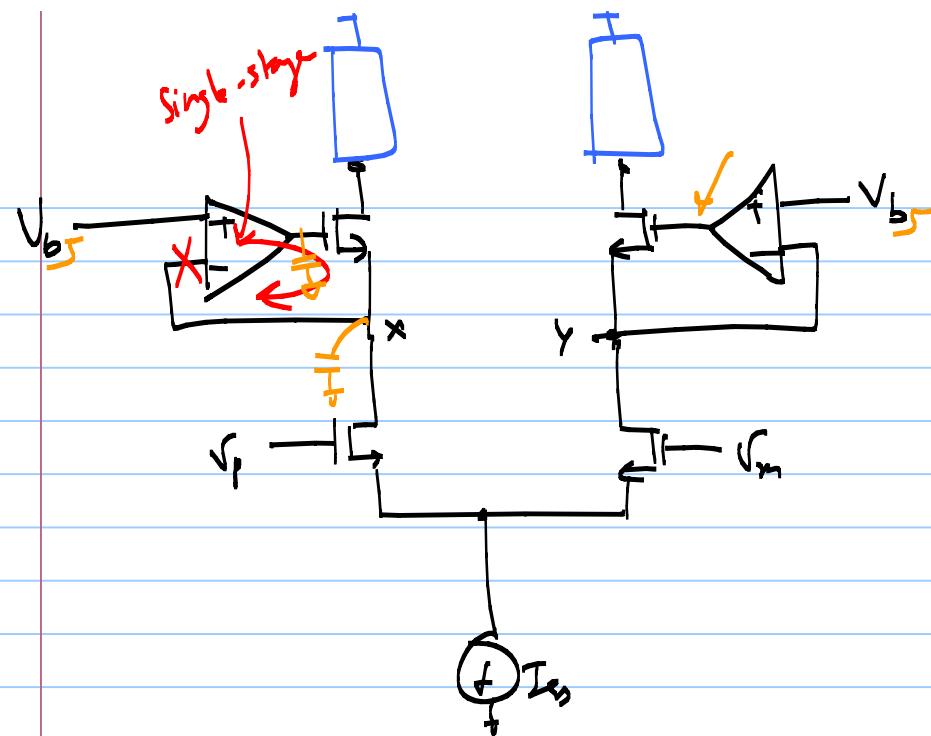


$$R_{out} = g_m r_o^2 \cdot A$$

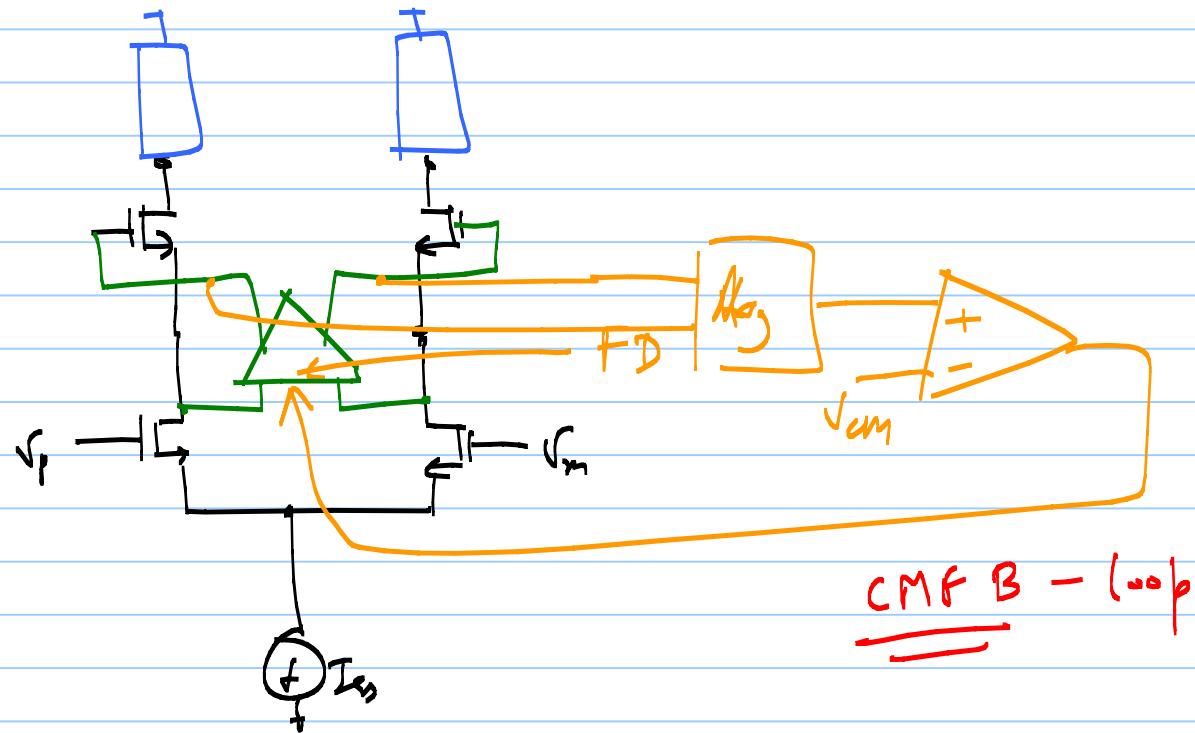
"gain-Boosting"

man- CMOS

$\leq 10_{\text{nm}}$



$$A_v = -\frac{r_m}{r_p} R_{out}$$



$0^{\circ} - 60^{\circ}\text{C}$

Temp Co.

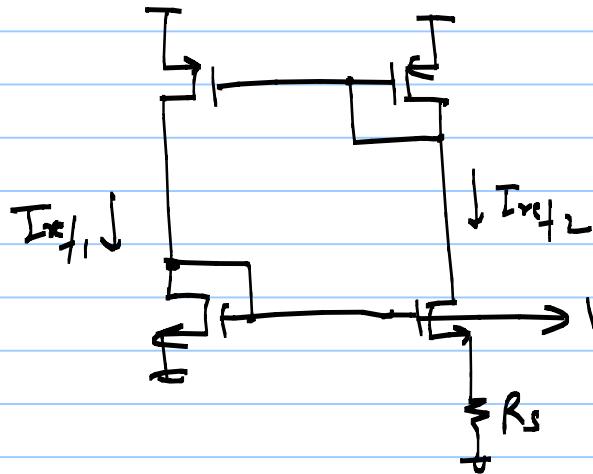


$$R(T) = R(T_0) \left[1 + TC_R \left(\frac{T-T_0}{T_0} \right) \right]$$

$$\boxed{TC_R = \frac{1}{R} \frac{\partial R}{\partial T}}$$

"Temperature Coefficient"

BMR



$$V_{ref} = \frac{2}{R_s k_{Bn}} \cdot \frac{V_L}{L} \left(1 - \frac{1}{\sqrt{R_s}} \right) + V_{THN}$$

μ_n Cox

$$\frac{\partial V_{ref}}{\partial T} = \left(\frac{\partial V_{THN}}{\partial T} \right) - \frac{2}{R_s k_{Bn} \cdot \frac{V_L}{L}} \left(1 - \frac{1}{\sqrt{R_s}} \right) \left(\frac{L}{R_s} \cdot \frac{\partial R_s}{\partial T} + \frac{1}{k_{Bn}} \cdot \frac{\partial k_{Bn}}{\partial T} \right)$$

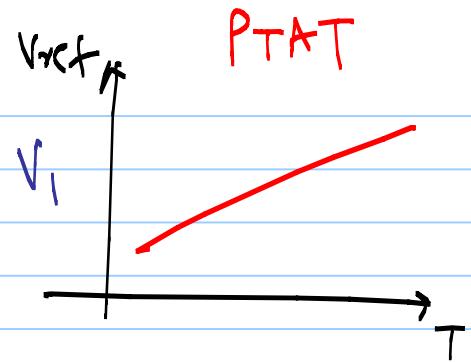
$\neq 0$

$$- \frac{1.5}{T}$$

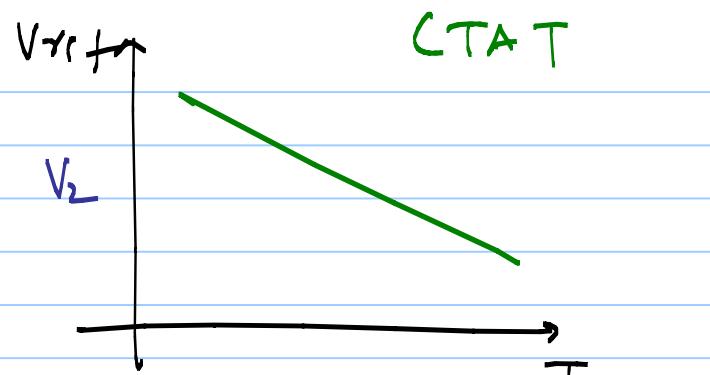
Select an R such that $\frac{\partial V_{ref}}{\partial T} = 0$ \downarrow ZT_C \rightarrow $2\pi \text{ km/p. } \omega.$

$$R = \frac{2}{\frac{\partial V_{ref}}{\partial T} \cdot k P_n \cdot \frac{W}{C}} \left(1 - \frac{1}{\sqrt{k}} \right) \left[\frac{1}{R} \cdot \frac{\partial R}{\partial T} - \frac{1}{T} \right]$$

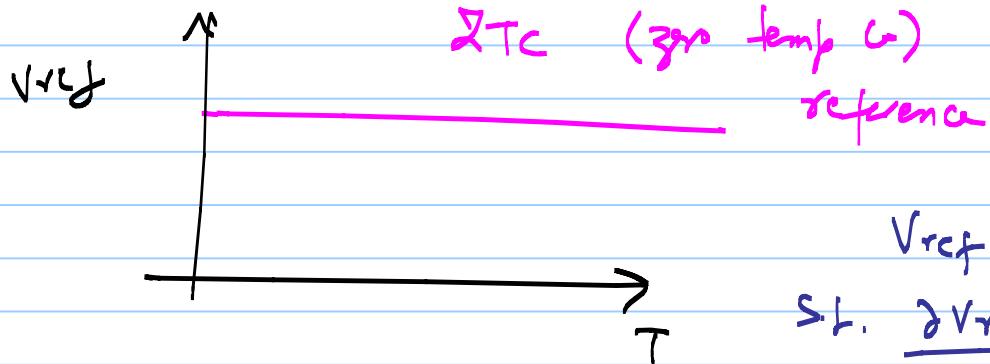
\hookrightarrow impractical to make BMR
with ZT_C



prop. to absolute temperature



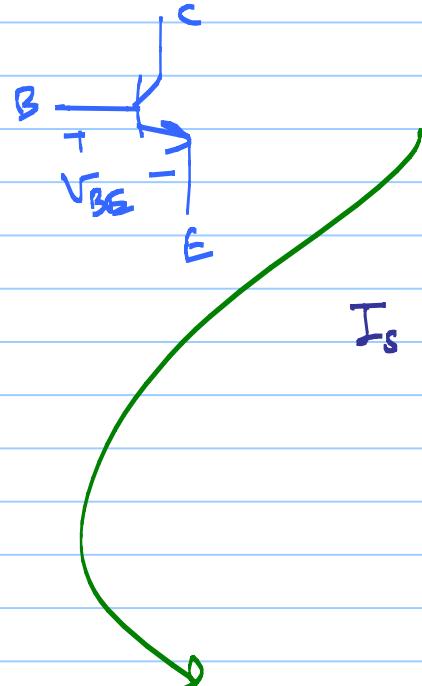
complementary to the
absolute Temperature



$$V_{ref} = \alpha_1 V_1 + \alpha_2 V_2$$

s.t. $\frac{\partial V_{ref}}{\partial T} = 0 \approx \boxed{\alpha_1 \frac{\partial V_1}{\partial T} + \alpha_2 \frac{\partial V_2}{\partial T} = 0}$

* CTA T \Rightarrow -ve Temp Co

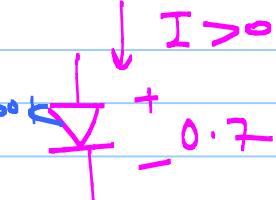


$$I_c = I_s e^{\frac{V_{BE}}{V_T}}$$

$$V_T = \frac{kT}{q} = 26 \text{ mV}$$

@ T = 300 K

$$\frac{\partial V_{THN}}{\partial T} < 0$$



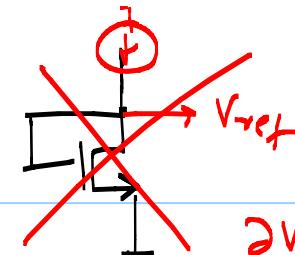
$$I_s \propto \mu k T n_i^2$$

$$\mu \propto \mu_0 T^m, \quad m = -\frac{3}{2}$$

$$n_i^2 \propto T^3 \cdot e^{-E_g/kT}$$

$E_g \rightarrow 1.12 \text{ eV}$

$$V_{BE} = V_T \ln \left(\frac{I_c}{I_s} \right)$$



A

A

$$I_s = b T^{(4+m)} \cdot e^{-E_g/kT} \rightarrow 2$$

* Compute the T_c of V_{BE}

$$\frac{\partial V_{BE}}{\partial T} = \frac{\partial V_T}{\partial T} \cdot \ln\left(\frac{I_c}{I_s}\right) - \frac{V_T}{I_s} \cdot \left(\frac{\partial I_s}{\partial T}\right) \rightarrow 3$$

$$\begin{aligned} \frac{\partial I_s}{\partial T} &= \frac{(4+m)}{T} b T^{4+m} \cdot e^{-E_g/kT} + b T^{4+m} e^{-E_g/kT} \cdot \frac{E_g}{kT^2} \\ &= \frac{(4+m)}{T} \cdot I_s + I_s \cdot \frac{E_g}{kT^2} \end{aligned}$$

$$\frac{\partial V_T}{I_S} \cdot \frac{\partial I_S}{\partial T} = (4+m) \frac{V_T}{T} + \frac{E_g}{kT^2} \cdot V_T$$

$$\Rightarrow \frac{\partial V_{BE}}{\partial T} = \frac{V_T}{T} \ln \left(\frac{I_c}{I_s} \right) - (4+m) \frac{V_T}{T} - \frac{E_g}{kT^2} \cdot V_T$$

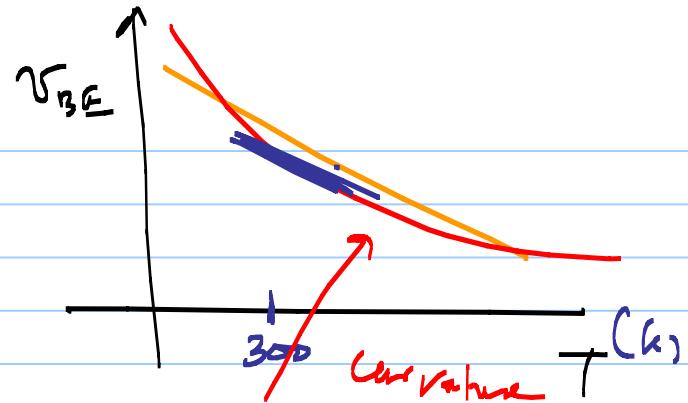
$$\boxed{\frac{\partial V_{BE}}{\partial T} = \frac{V_{BE} - (4+m)V_T - \frac{E_g}{2}}{T}}$$

$$1 = 1 \cdot C \times R^{-1} \propto C$$

* $\frac{\partial V_{BE}}{\partial T}$ depends upon V_{BE} itself
besides the temperature

* with $V_{BE} = 0.75V$, $T = 300^\circ K$

$$\boxed{\frac{\partial V_{BE}}{\partial T} \approx -1.5 \frac{mV}{^\circ K}}$$



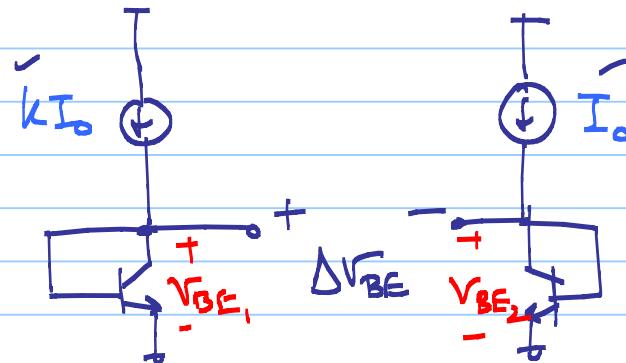
* V_{BE} is not a linear CTAT

②

P-TAT

mpn BJT's

diode connected



$$\Delta V_{BE} = V_{BE1} - V_{BE2}$$

$$= V_T \ln \left(\frac{kI_0}{I_s} \right) - V_T \ln \left(\frac{I_0}{I_s} \right)$$

$$= V_T \ln (k)$$

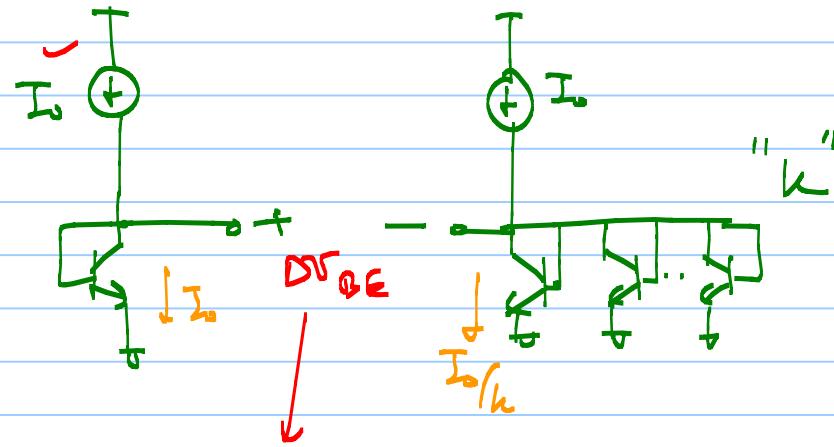
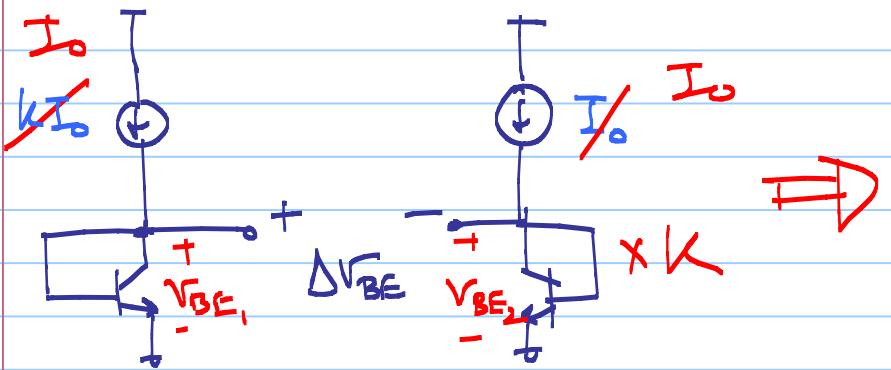
$$\Delta V_{BE} = \frac{k}{q} \ln(k)$$

$$\frac{\partial V_{BE}}{\partial T} = \frac{k}{q} \ln(k) > 0$$

independent of I_C .

linear PTAT





$$V_T \ln(k)$$

"PTAT"

Bandgap Reference $\Rightarrow \alpha_1 \cdot CTAT + \alpha_2 PTAT \Rightarrow ZTC$

$$V_{ref} = \alpha_1 V_{BE} + \alpha_2 (V_T \ln(k))$$

* How do we choose α_1 & α_2 ?

$\frac{\partial V_{ref}}{\partial T} = 0 \Rightarrow \alpha_1 \cdot \frac{\partial V_{BE}}{\partial T} + \alpha_2 \cdot \left(\frac{k}{q} \ln k \right) = 0$

$\alpha_2 \ln k = -\alpha_1 \cdot \frac{\partial V_{BE}}{\partial T}$

$\frac{1.5 \text{ mV}}{\text{°K}}$

$\frac{\partial V_T}{\partial T} = 0.087 \frac{\text{mV}}{\text{°K}}$

$$\alpha_2 \ln(h) = \alpha_1 \cdot \frac{1.5 \frac{mV}{h}}{0.087 \frac{mV}{h}}$$

$$\boxed{\alpha_2 \ln(h) = \alpha_1 \times 17.2}$$

Arbitrarily choose $\alpha_1 = 1$

$$\Rightarrow \alpha_2 \ln(h) = 17.2$$

\Rightarrow

$$\boxed{V_{REF} = V_{BE} + 17.2 \cdot V_T}$$

$$= 0.75V + 17.2 \times 26 mV$$

$$\approx 1.2V$$

