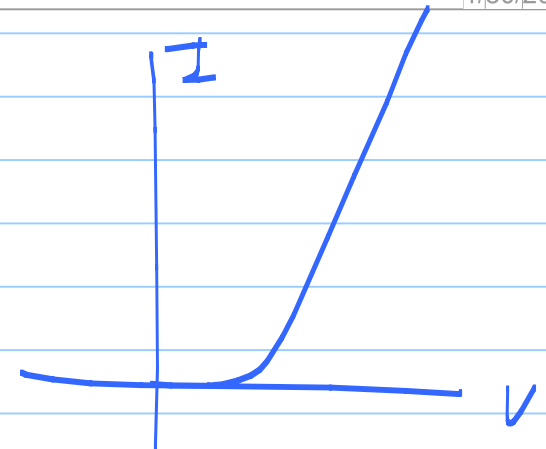
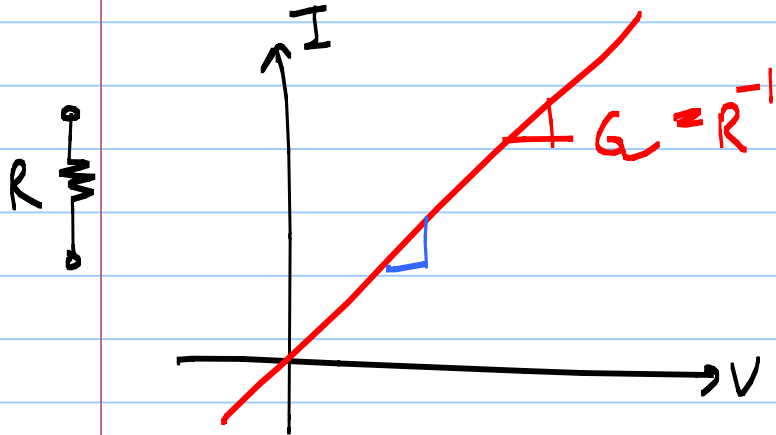
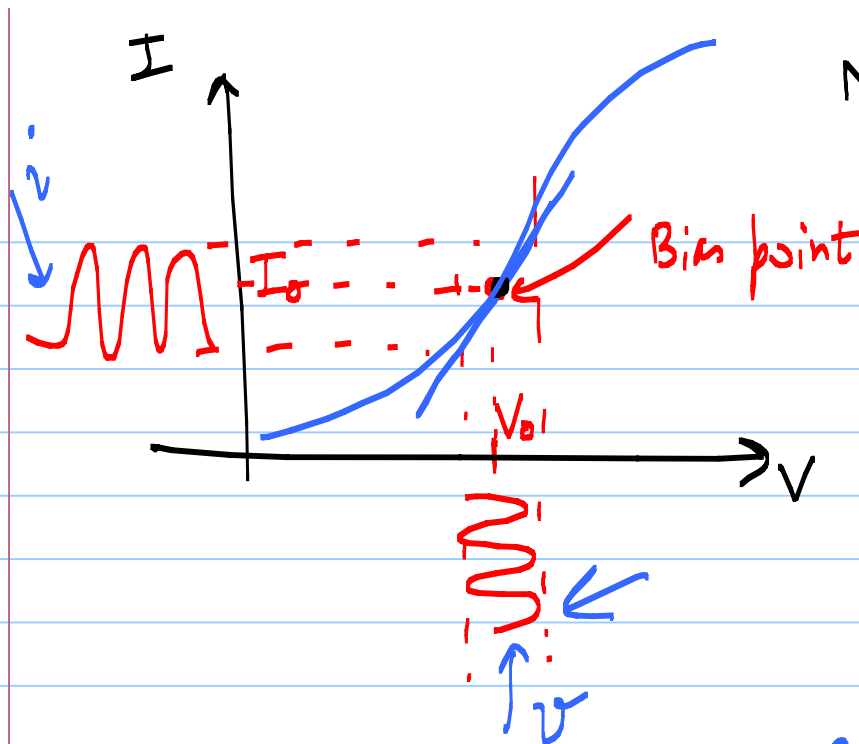


ECE 511 - Lecture 4.

Note Title

1/30/2012





$$I = f(V)$$

$I = f(V)$ ← Taylor Series expansion around $V = V_0$

$$\Rightarrow I = f(V_0) + f'(V_0) \underbrace{(V - V_0)}_v + \frac{f''(V_0)}{2} \underbrace{(V - V_0)^2}_{v^2} + \frac{f'''(V_0)}{6} \underbrace{(V - V_0)^3}_{v^3} + \dots$$

$$V = \underbrace{V_0}_{V_{DC}} + v \leftarrow AC$$

$$I = \underbrace{f(V_0)}_{I_0} + f'(V_0)v + \frac{f''(V_0)}{2}v^2 + \frac{f'''(V_0)}{6}v^3 + \dots$$

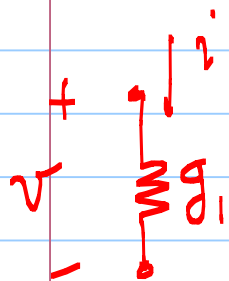
$$\Rightarrow \underbrace{I - I_0}_i = f'(V_0)v + \frac{f''(V_0)}{2}v^2 + \frac{f'''(V_0)}{6}v^3 + \dots$$

$$i = f'(V_0) \cdot v + \frac{f''(V_0)}{2}v^2 + \frac{f'''(V_0)}{6}v^3 + \dots$$

$$i = g_1 v + \underline{g_2} v^2 + \underline{g_3} v^3 + \dots \quad v \ll V_0$$

$i = g_1 v$ $\leftarrow$ Linear relationship between
AC voltage & current

$$g_1 = f'(V_0) = \left. \frac{\partial f}{\partial v} \right|_{v=V_0} \quad \leftarrow \text{first derivative at } v=V_0$$



$$i = g_1 v$$

↑ $f'(V_0)$ ← small-signal parameter

↳ bias point

↑ linearized the device about the Bias point

↳ DC operating point

↳ Q-point

$$i = g_1 v + g_2 v^2 + g_3 v^3 + \dots$$

if v is not small enough

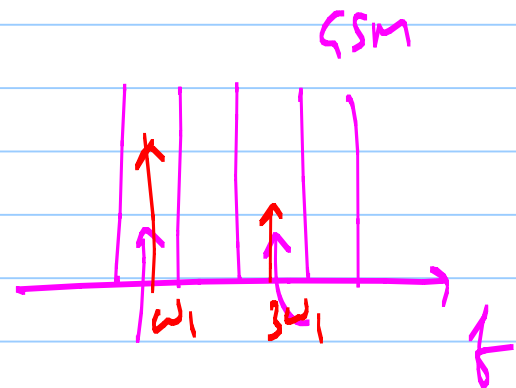
$$v = A \sin \omega_1 t$$

for small A

$$i = g_1 A \sin \omega_1 t$$

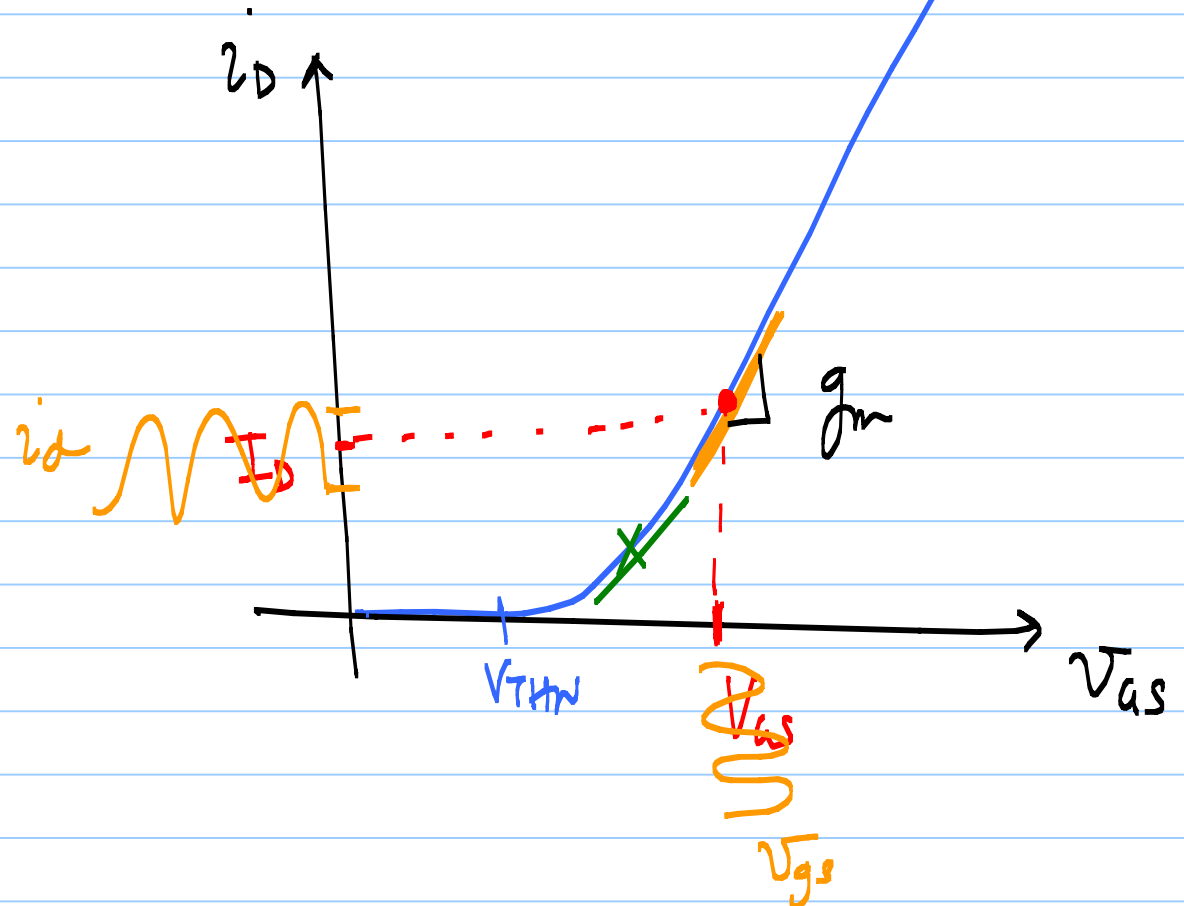
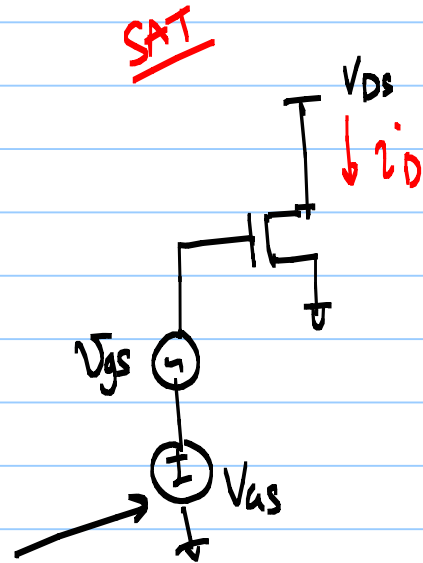
for larger A

$$i = () \sin \omega_1 t + () \sin 2\omega_1 t + () \sin 3\omega_1 t$$



NMOS in Saturation:

$$V_{DS} > V_{DS,sat} \\ = V_{GS} - V_{THN}$$



$$i_D = \frac{K_p}{2} \frac{\mu}{L} (V_{as} - V_{th})^2 \quad \checkmark$$

$$\lambda = 0$$

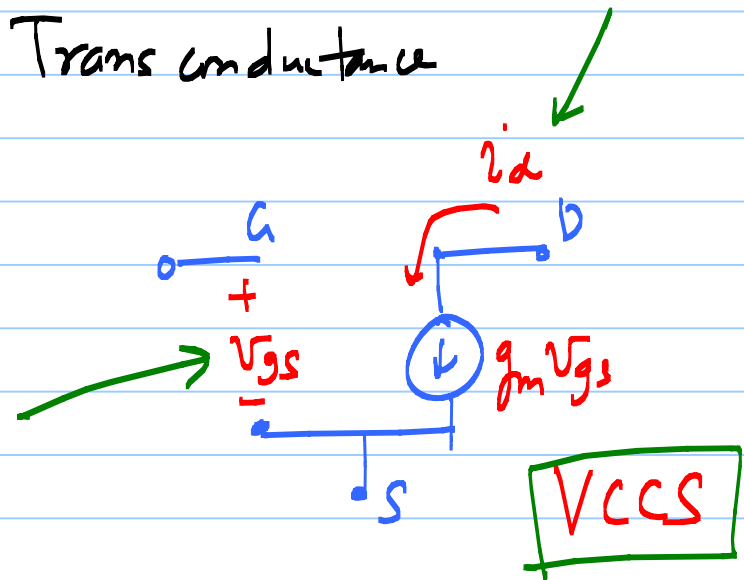
$$i_d = f'(V_0) V_{gs}$$

↓

$$i_d = g_m V_{gs}$$

$$g_m = \left. \frac{\partial i_D}{\partial V_{as}} \right|_{V_{as}=V_{as}}$$

← Trans conductance



$$g_m = \left. \frac{\partial I_D}{\partial V_{GS}} \right|_{V_{GS}}$$

$$= \frac{K P_n}{2} \cdot \frac{W}{L} \cdot 2 (V_{GS} - V_{THN}) \bigg|_{V_{GS} = V_{GS}}$$

$$g_m = \underbrace{K P_n \frac{W}{L}}_{\beta_n} (V_{GS} - V_{THN})$$

$$g_m = \beta_n (V_{GS} - V_{THN}) \quad \text{①}$$

$V_{ov} = V_{GS} - V_{THN}$
overdrive voltage

$$g_m = \beta_n (V_{GS} - V_{THN})$$

$$= \beta_n \sqrt{\frac{2I_D}{\beta_n}}$$

$$\Rightarrow g_m = \sqrt{2\beta_n I_D}$$

$$g_m = \frac{2I_D}{(V_{GS} - V_{THN})^2} \times \cancel{(V_{GS} - V_{THN})}$$

$$I_D = \frac{\beta_n}{2} (V_{GS} - V_{THN})^2$$

$$\Rightarrow V_{GS} - V_{THN} = \sqrt{\frac{2I_D}{\beta_n}}$$

$$\beta_n = \frac{2I_D}{(V_{GS} - V_{THN})^2}$$

②

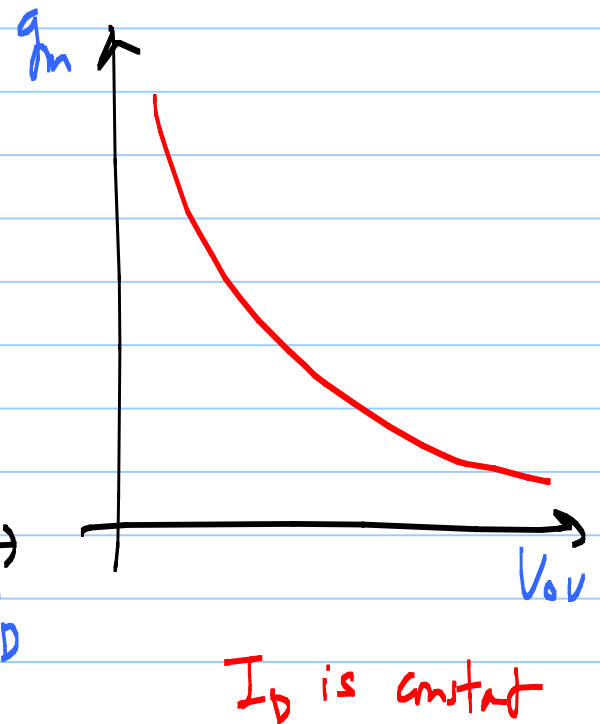
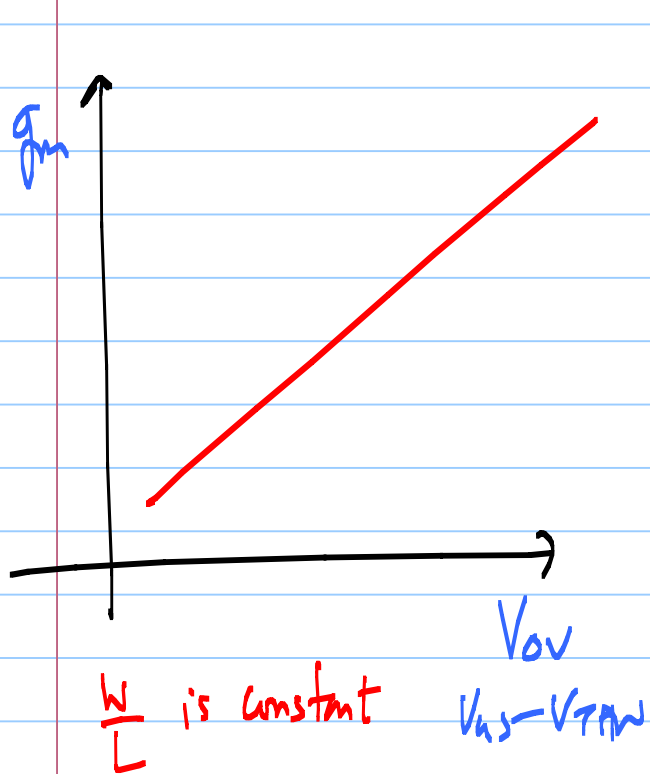
$$g_m = \frac{2I_D}{V_{GS} - V_{THN}}$$

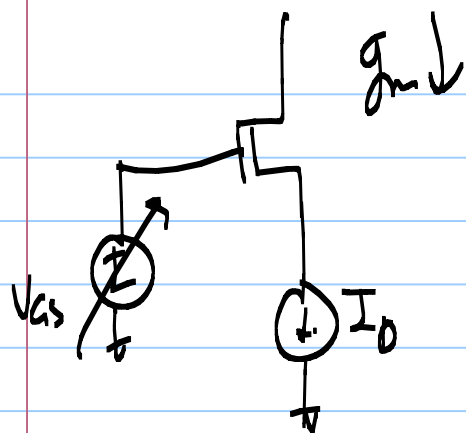
③

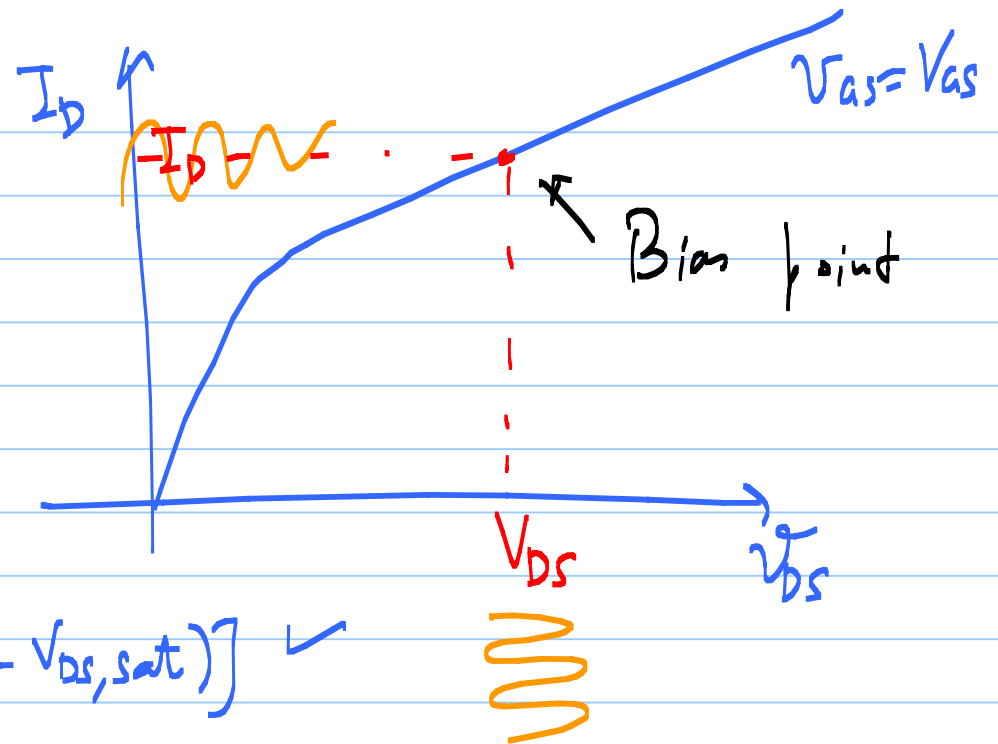
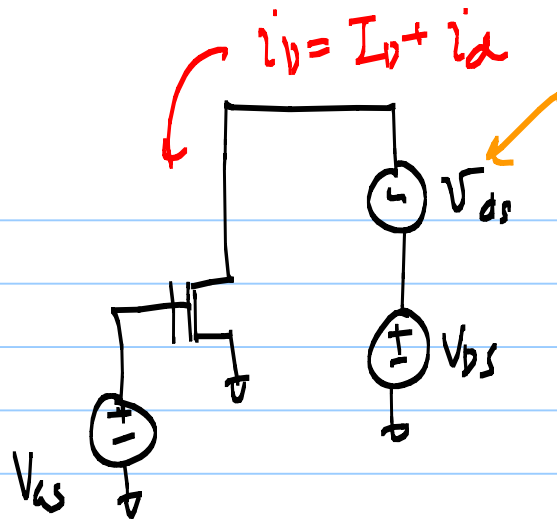
$$g_m = \beta_n (V_{GS} - V_{THn})$$

$$g_m = \sqrt{2\beta_n I_D}$$

$$g_m = \frac{2I_D}{V_{GS} - V_{THn}}$$







$$i_D = \frac{K}{2} \frac{W}{L} (V_{GS} - V_{TH})^2 [1 + \lambda (V_{DS} - V_{DS,sat})]$$

$$i_d = g_o v_{ds} = (g_o^{-1}) v_{ds}$$

output conductance $g_o = g_{DS}$

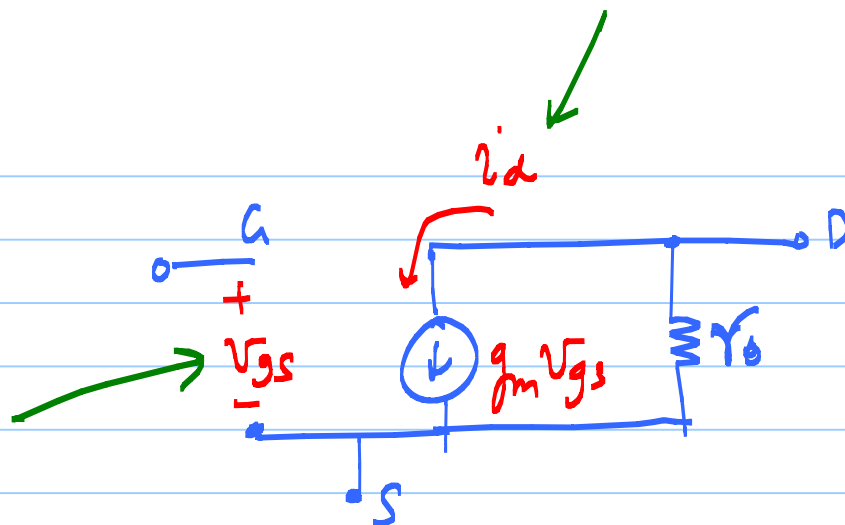
$$g_o = r_o^{-1} = \left. \frac{\partial i_o}{\partial v_{os}} \right|_{\substack{v_{os} = v_{bs} \\ v_{as} = \text{const}}}$$

$$= \underbrace{\frac{k_p n}{2} \frac{W}{L} (V_{as} - V_{THn})^2}_{I_{D,sat}} \cdot \lambda$$

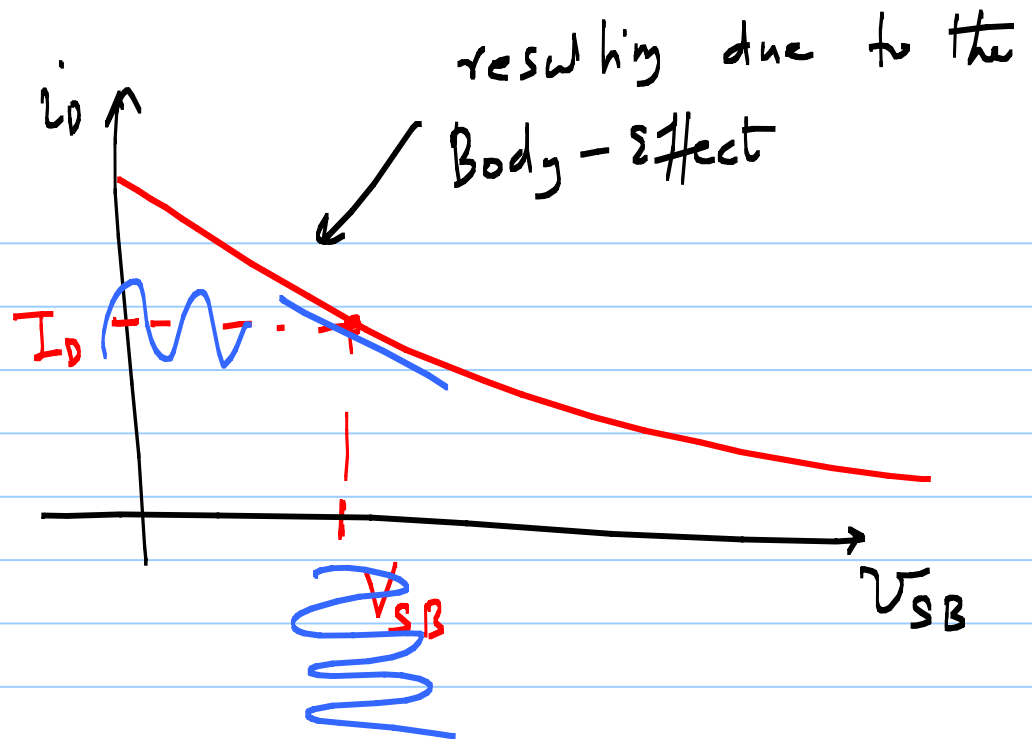
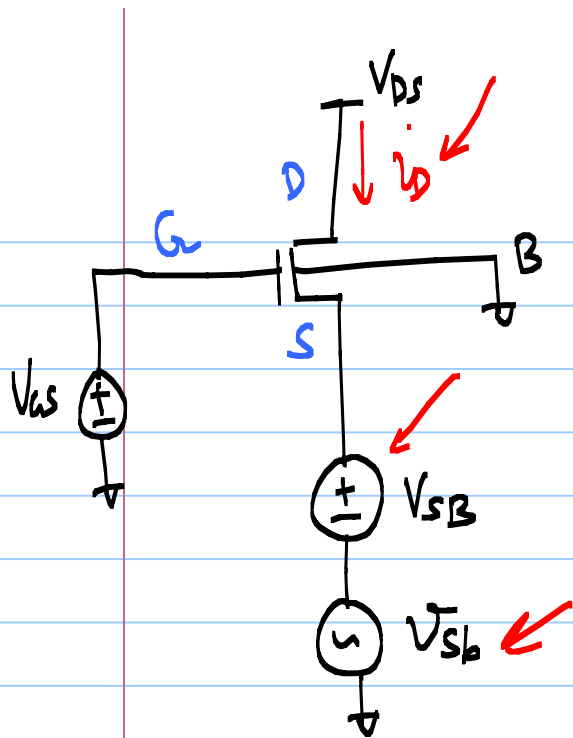
$$= \lambda \cdot I_{D,sat}$$

$\Rightarrow$

$$r_o = \frac{1}{\lambda \cdot I_{D,sat}}$$



V_{CCS}



$$i_D = f(V_{SB})$$

$$i_D = g_{mb} \cdot v_{sb}$$

Body g_m

$$g_{mb} = \left. \frac{\partial i_D}{\partial V_{SB}} \right|_{V_{SB} = V_{SB}}$$

$$= \left. \frac{\partial}{\partial V_{SB}} \left[\frac{K_P n}{2} \cdot \frac{W}{L} (V_{AS} - V_{THN})^2 \right] \right|_{V_{SB} = V_{SB}}$$

$$= \underbrace{K_P n \cdot \frac{W}{L} (V_{AS} - V_{THN})}_{g_m} \cdot \left[\frac{-\partial V_{THN}}{\partial V_{SB}} \right]_{V_{SB} = V_{SB}}$$

$$= g_m \cdot \underbrace{\left(-\frac{\partial}{\partial V_{SB}} (|2V_{fp}| + V_{SB})^{-1/2} \right)}_{\eta \leftarrow \text{body factor}}$$

$$g_{mb} = \eta \cdot g_m$$

$$|\eta| < 1$$

$$\eta = \frac{-\gamma}{2\sqrt{2|V_{fb}| + V_{SB}}}$$

