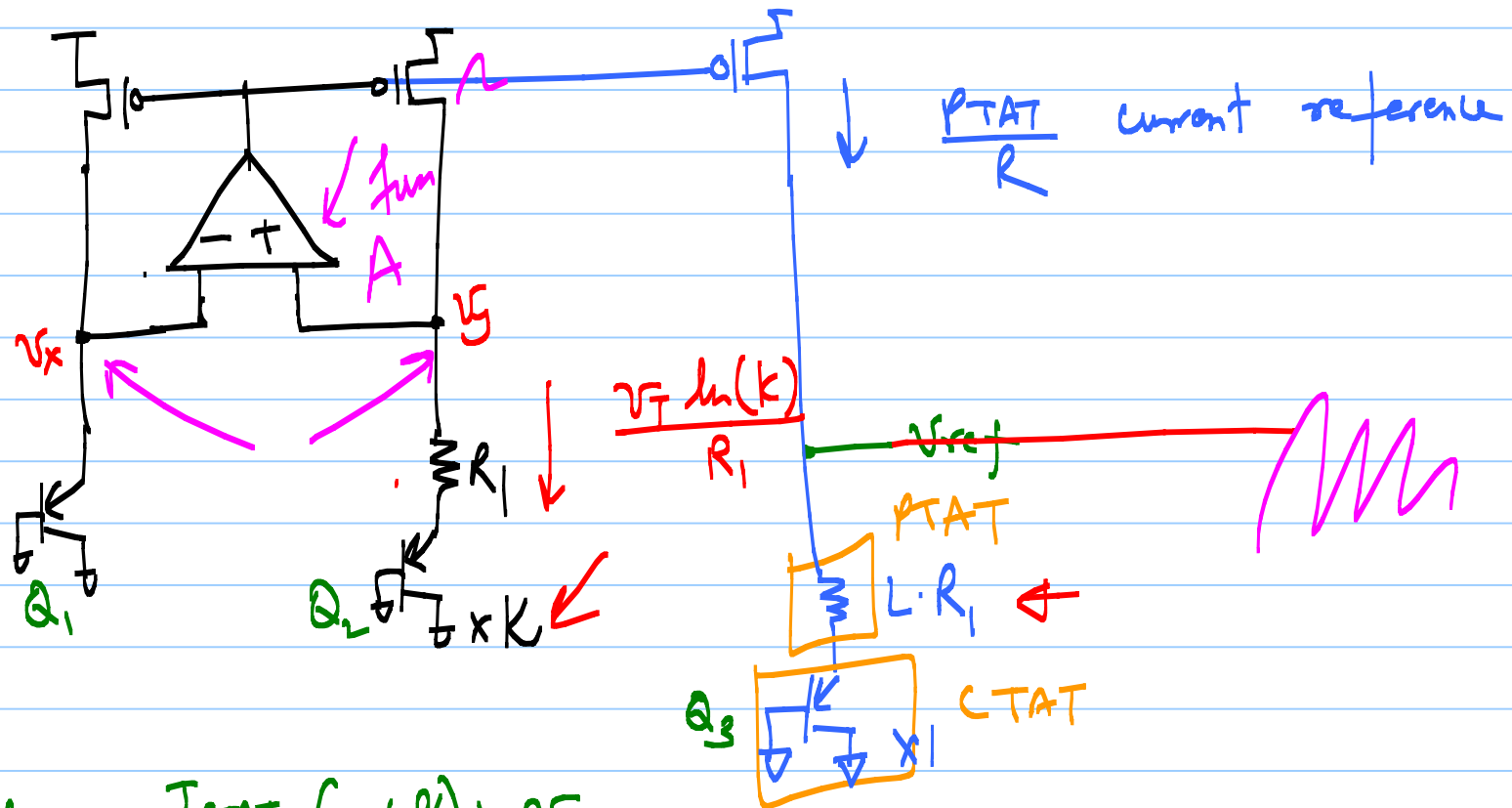


ECE 511 - Lecture 25 (Final Lecture)

Note Title

5/2/2012



$$V_{ref} = \frac{I_{PTAT}}{R_1} (L R_1) + V_{BE3} = V_T \ln(K) \cdot L + V_{BE3}$$

$$V_{ref} = \underbrace{V_T}_{PTAT} \underbrace{\ln(K) \cdot L}_{\alpha_2} + \underbrace{V_{BE3}}_{CTAT}$$

$$\text{for } \frac{\partial V_{ref}}{\partial T} = 0 \Rightarrow \underbrace{\left(\frac{K}{\alpha}\right) \cdot \ln(K) L}_{0.085 \frac{mV}{K}} + \underbrace{\frac{\partial V_{BE3}}{\partial T}}_{-1.5 mV/K} = 0$$

$$\Rightarrow \ln(K) \cdot L = 17.2$$

$$\text{for } L = 5,$$

$$K = e^{17.2/5} = e^{3.5} = 33$$

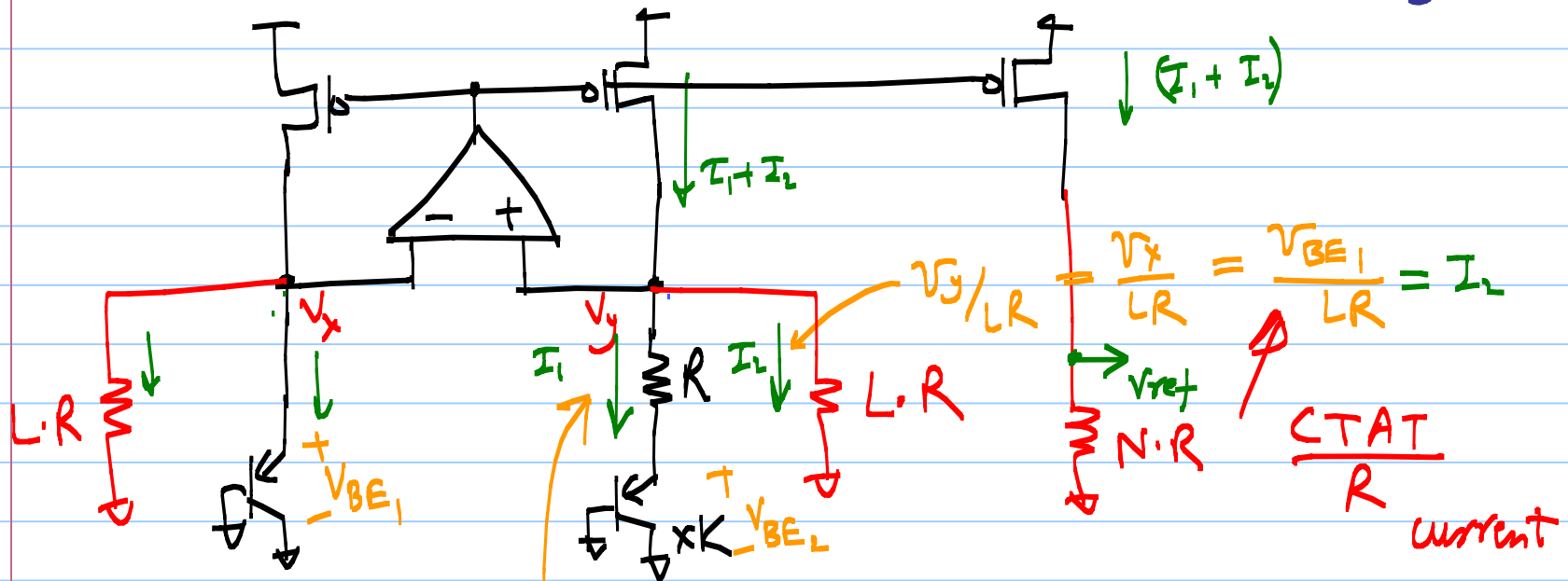
$$K = 33, L = 5$$

$$V_{ref} = V_{BE3} + \overset{26 mV}{V_T} \times 17.2$$

$$= 0.7 + 0.026 \times 17.2 = \boxed{1.25 V}$$

short channel BGR ($V_{DD} \leq 1V$)

$$V_x = V_y$$



$$V_T = V_J \Rightarrow \frac{V_T \ln k}{R} \leftarrow \frac{PTAT}{R} \text{ current}$$

$$V_{ref} = (I_1 + I_2) N \cdot R$$

$$V_{ref} = \left(\frac{V_T \ln K}{R} + \frac{V_{BE1}}{L \cdot R} \right) N \cdot R$$

$$V_{ref} = V_T \cdot \underbrace{N \ln(K)}_{\alpha_2} + \underbrace{\frac{N}{L}}_{\alpha_1} V_{BE1}$$

?
 $\swarrow \quad \checkmark \quad \checkmark$
 $N, K, L = ???$

$$\text{fiv} \quad \frac{\partial V_{ref}}{\partial T} = 0 \Rightarrow \left[\frac{R}{\alpha_2} \right] N \cdot \ln(K) + \frac{N}{L} \cdot \left(\frac{\partial V_{BE1}}{\partial T} \right) = 0$$

$$\Rightarrow L = \frac{1.5 \text{ mV}/^\circ\text{K}}{\ln(K) \cdot 0.085 \frac{\text{mV}}{^\circ\text{K}}}$$

$$\Rightarrow \underline{L \cdot \ln(K) = 17.2}$$

Let's choose $\boxed{k=8}$ $\Rightarrow$ $\boxed{L=9.41}$ (k, L) ~~☆~~

By design $V_{ref} = 500 \text{ mV}$

$$V_{ref} = V_T \ln(k) \cdot N + \left(\frac{N}{L}\right) V_{BE1}$$

$\alpha_1 < 1$

$$\Rightarrow N = \frac{V_{ref}}{V_T \ln k + \frac{V_{BE1}}{L}} = 3.91$$

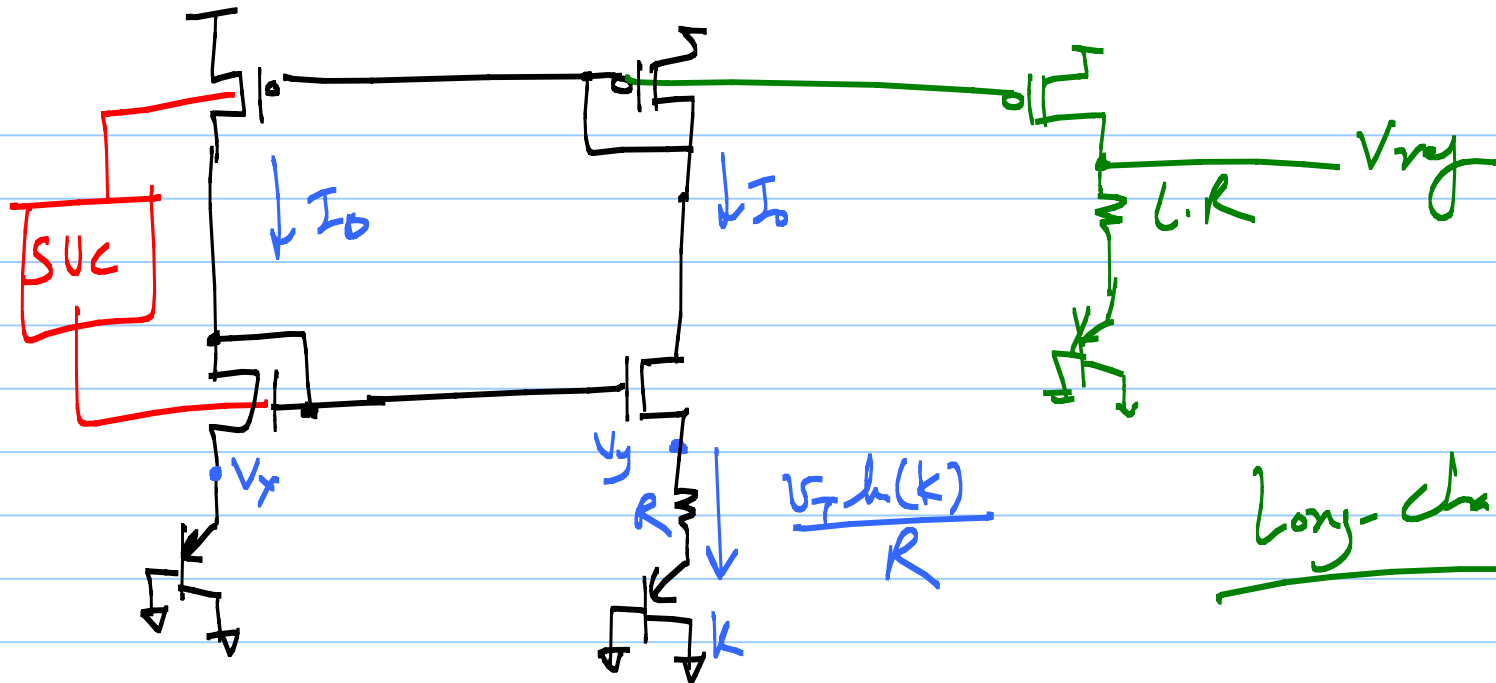
$\leftarrow 0.7 \text{ V}$

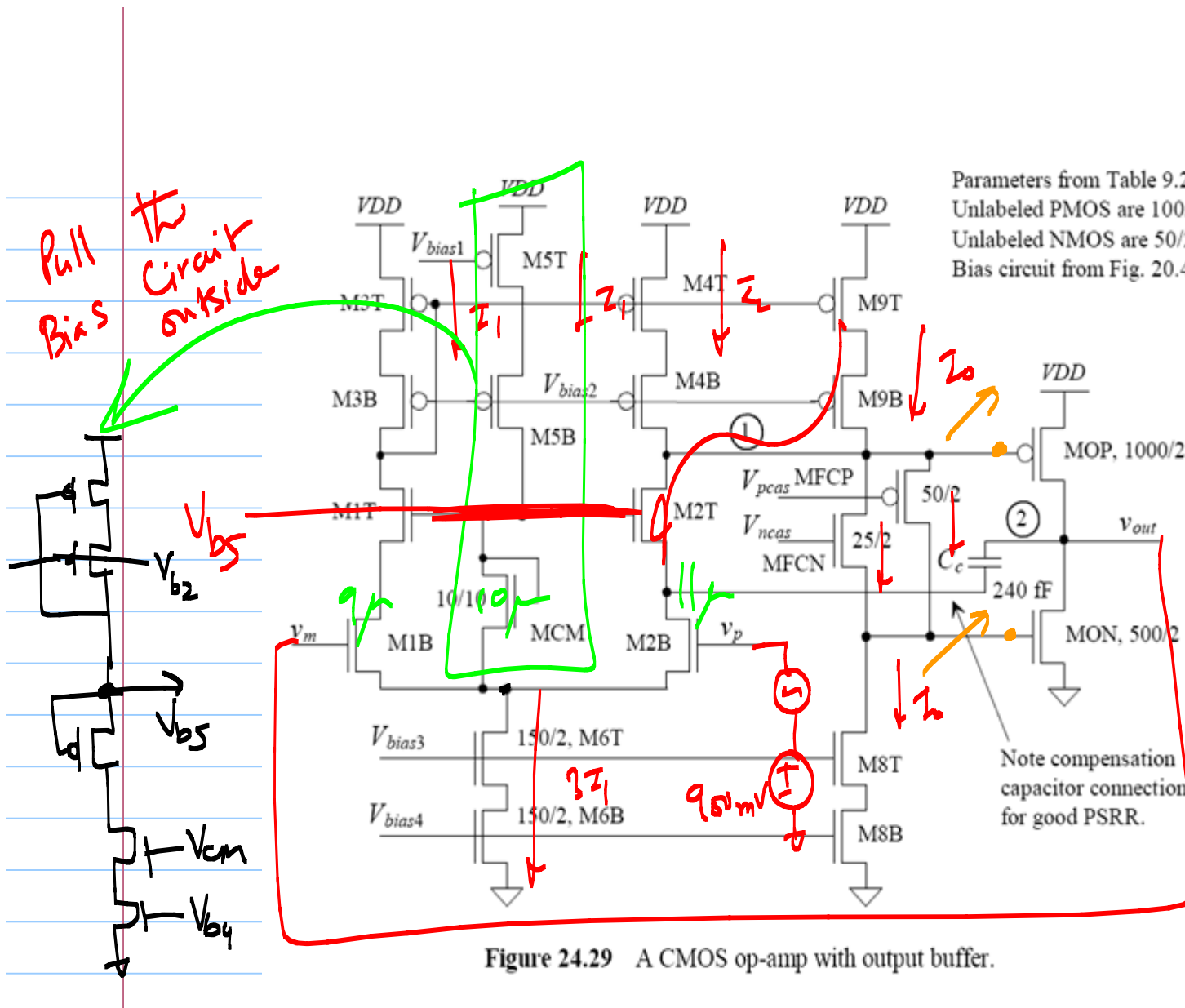
$\downarrow$
 $\boxed{N=3.91}$

$\downarrow$
 $\boxed{V_{ref} = 500 \text{ mV}}$

* No unique solution

BMR-type design:





Fixed
 V_{ov}
 $\rightarrow 50\% V_{DD}$
 $\rightarrow 90mV$
 $\downarrow + V_{THN}$
 V_{THP}
 $V_{AS} = 350mV$
 $V_{SA} = 400mV$
 $I = 10\mu A$
 $(\frac{W}{L}) \sim (\frac{W}{L})$

ADG L $\Rightarrow$ Results $\rightarrow$ Show Op points
 $\searrow$ Print

gas is high $\Rightarrow$ Triode g_m
 $\leftarrow$ $g_{ds} \propto \omega^{-1}$
gas is low $\leftarrow$ Caps
Deep Saturation

!

Table 9.7 Typical parameters for analog design using the *short-channel* CMOS process discussed in this book. These parameters are valid only for the device sizes and currents listed.

Short-channel MOSFET parameters for general analog design $V_{DD} = 1\text{ V}$ and a scale factor of 50 nm ($scale = 50e-9$)			
Parameter	NMOS	PMOS	Comments
Bias current, I_D	10 μA	10 μA	Approximate, see Fig. 9.31
W/L	50/2	100/2	Selected based on I_D and V_{ov}
Actual W/L	2.5 $\mu\text{m}/100\text{nm}$	5 $\mu\text{m}/100\text{nm}$	L_{min} is 50 nm
$V_{DS,sat}$ and $V_{SD,sat}$	50 mV	50 mV	However, see Fig. 9.32 and the associated discussion
V_{ovn} and V_{ovp}	70 mV	70 mV	
V_{GS} and V_{SG}	350 mV	350 mV	No body effect
V_{THN} and V_{THP}	280 mV	280 mV	Typical
$\partial V_{THN,P}/\partial T$	-0.6 mV/C°	-0.6 mV/C°	Change with temperature
v_{satn} and v_{satp}	110 x 10 ³ m/s	90 x 10 ³ m/s	From the BSIM4 model
t_{ox}	14 Å	14 Å	Tunnel gate current, 5 A/cm ²
$C'_{ox} = \epsilon_{ox}/t_{ox}$	25 fF/ μm^2	25 fF/ μm^2	$C_{ox} = C'_{ox}WL \cdot (scale)^2$
C_{ovn} and C_{ovp}	6.25 fF	12.5 fF	PMOS is two times wider
C_{gzn} and C_{gzp}	4.17 fF	8.34 fF	$C_{gz} = \frac{2}{3}C_{ox}$
C_{gdn} and C_{gdp}	1.56 fF	3.7 fF	$C_{gd} = CGDO \cdot W \cdot scale$
g_{mn} and g_{mp}	150 $\mu\text{A/V}$	150 $\mu\text{A/V}$	At $I_D = 10\text{ }\mu\text{A}$
r_{on} and r_{op}	167 k Ω	333 k Ω	Approximate at $I_D = 10\text{ }\mu\text{A}$
$g_{mn}r_{on}$ and $g_{mp}r_{op}$	25 V/V	50 V/V	!!Open circuit gain!!
λ_n and λ_p	0.6 V ⁻¹	0.3 V ⁻¹	$L = 2$
f_{Tn} and f_{Tp}	6000 MHz	3000 MHz	Approximate at $L = 2$

V_{ov}

70% V_{DD}

fix
 V_{ov}



✓
 $f_T \propto \frac{V_{OV}}{L_{min} = 180nm}$

$f_{in} \approx \frac{f_T}{10}$

✓
 $g_m r_o \propto \frac{L}{V_{OV}}$

fixed V_{ov}

$$g_m = \frac{2I_D}{V_{ov}}$$

$$\Rightarrow \left(\frac{g_m}{I_D} \right) = \frac{2}{V_{ov}}$$

fixed $\left(\frac{g_m}{I_D} \right)$ ratio

↳ independent of W

↳ $\left(\frac{g_m}{I_D} \right)$ method for sizing.

