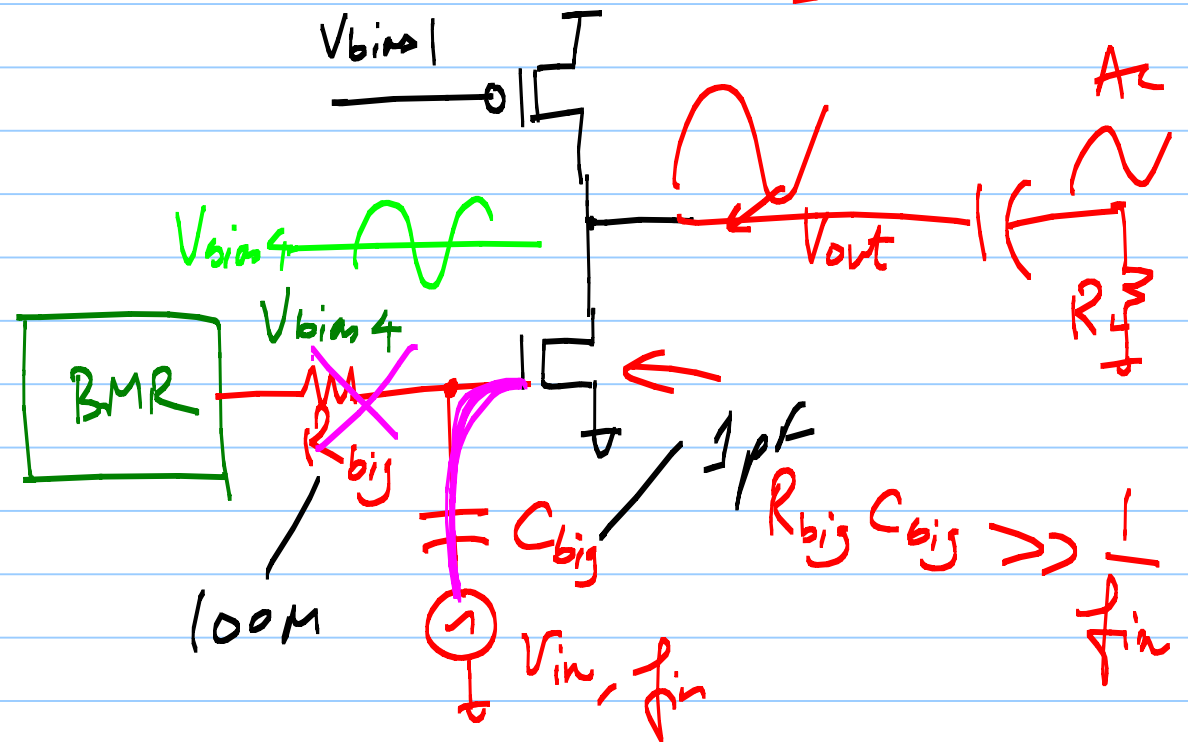
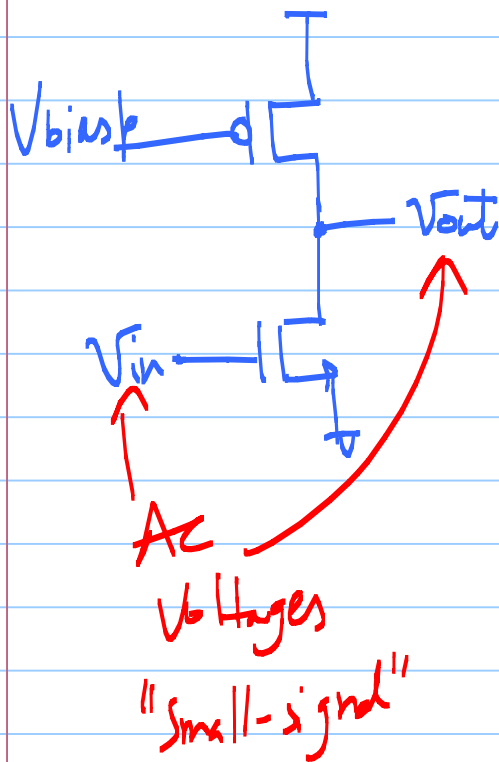


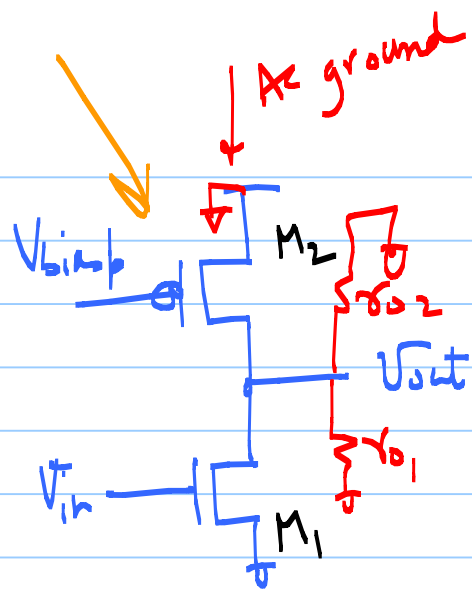
ECE 511 - Lecture 11

Note Title

2/29/2012

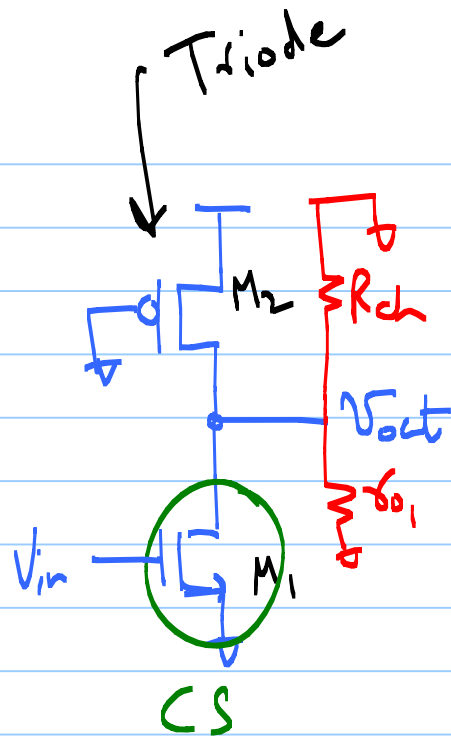
Fig 21.8





Small-signal

$$AC \text{ gain} = -g_{m1} \cdot (r_{o1} \parallel r_{o2})$$



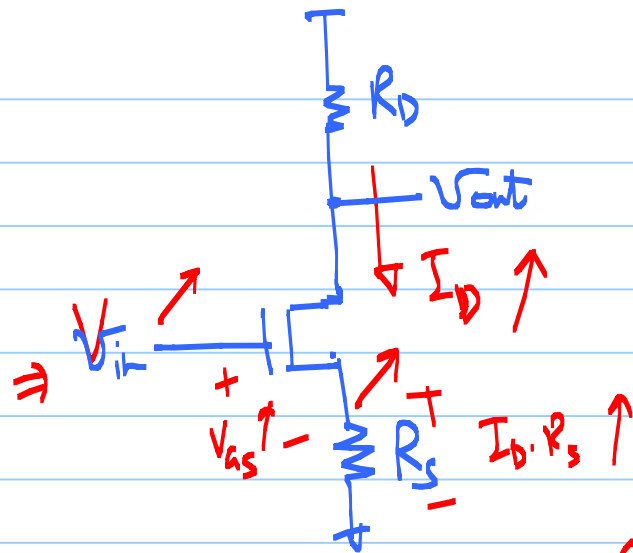
$$A = -g_{m1} \cdot v_{o1} \parallel R_L \approx -g_{m1} \cdot R_L$$

"low-gain"

$$R_L = \frac{1}{K_P \frac{W}{L} (V_{SG} - V_{THN})}$$

$$V_{SD} \ll V_{DD}$$

CS $\rightarrow$ Source Degeneration



-ve feedback

$\rightarrow$ keeps V_{GS} somewhat constant.

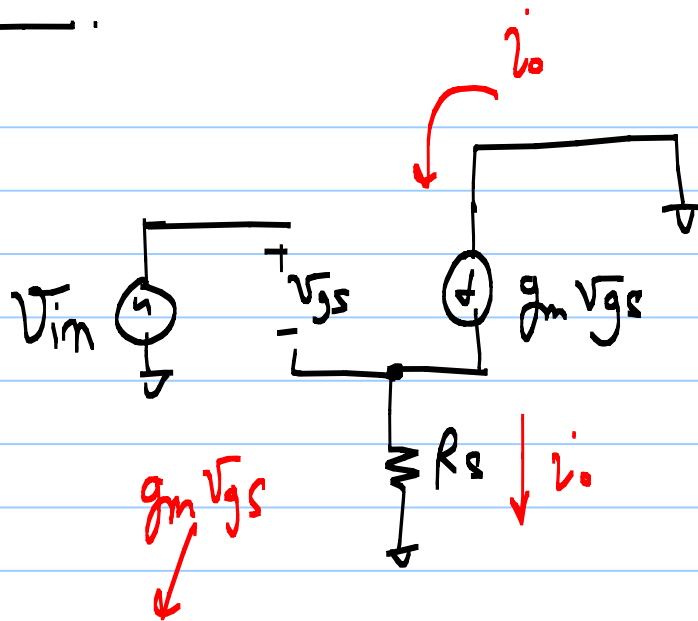
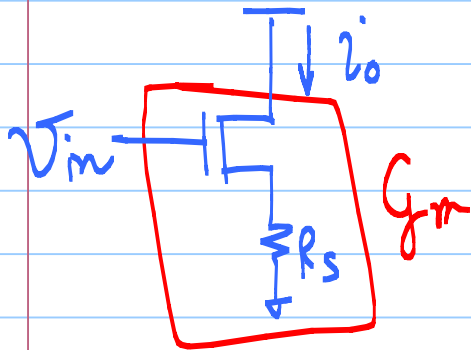
$\rightarrow$ a portion of V_{in} is dropped across R_S

$$I_D = \frac{V_{in} - V_{GS}}{R_S}$$
$$\propto \frac{V_{in}}{R_S}$$

I_D has linear dependence on V_{in}

Small-signal Analysis

$$\lambda=0, g_{mb}=0$$

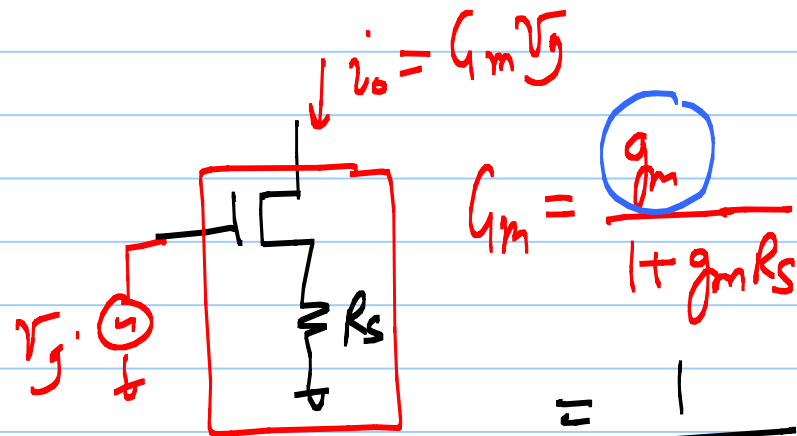
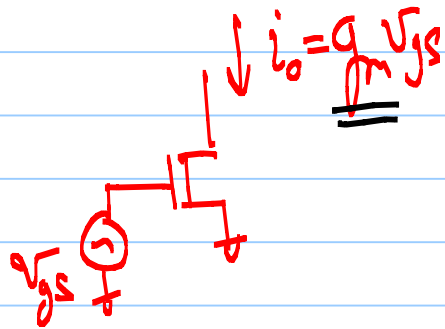


$$V_{gs} = V_{in} - i_o R_s$$

$$\Rightarrow i_o = g_m V_{gs} = g_m (V_{in} - i_o R_s)$$

$$\Rightarrow i_o (1 + g_m R_s) = g_m V_{in}$$

$$\Rightarrow \frac{i_o}{v_{in}} = \frac{g_m}{1 + g_m R_s} = G_m$$



$$G_m = \frac{g_m}{1 + g_m R_s}$$

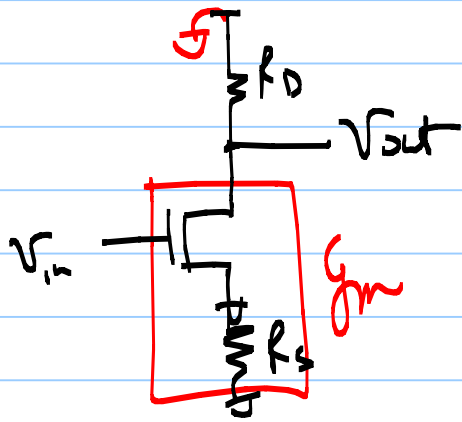
$$\approx \frac{1}{\frac{1}{g_m} + R_s}$$

$$\frac{1}{g_m} \ll R_s$$

$$\approx \frac{1}{R_s} \leftarrow \text{linear}$$

* $R_s \uparrow \Rightarrow R_s \gg \frac{1}{g_m} \Rightarrow g_m$ becomes a weak function of g_m

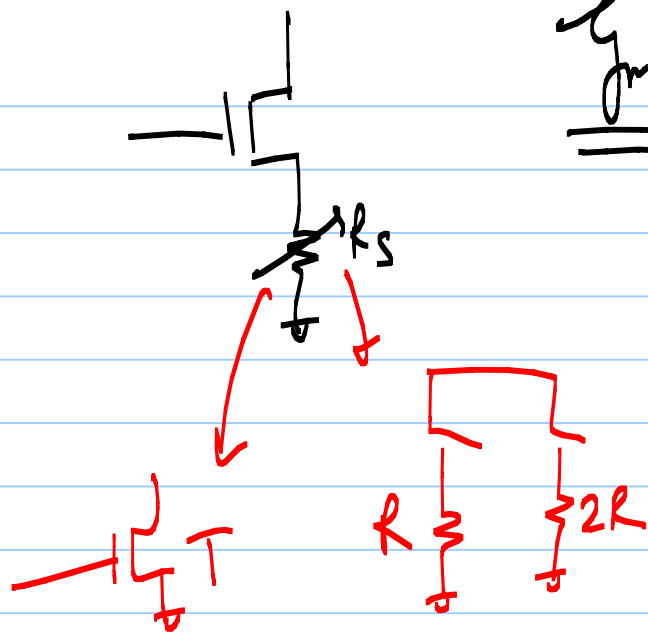
$\Rightarrow$ drain current (i_D) is a linearized function of V_{in}



$$A_v = -g_m R_D$$

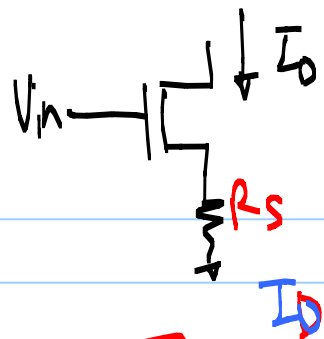
$$= -\frac{g_m R_D}{1 + g_m R_s}$$

$\Leftarrow$ lower small-signal gain

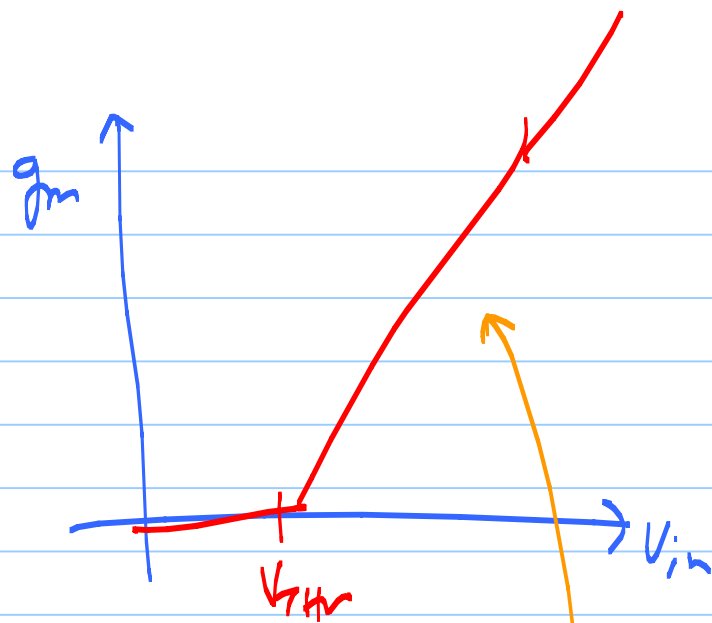


$$g_m \approx \frac{1}{r_s}$$

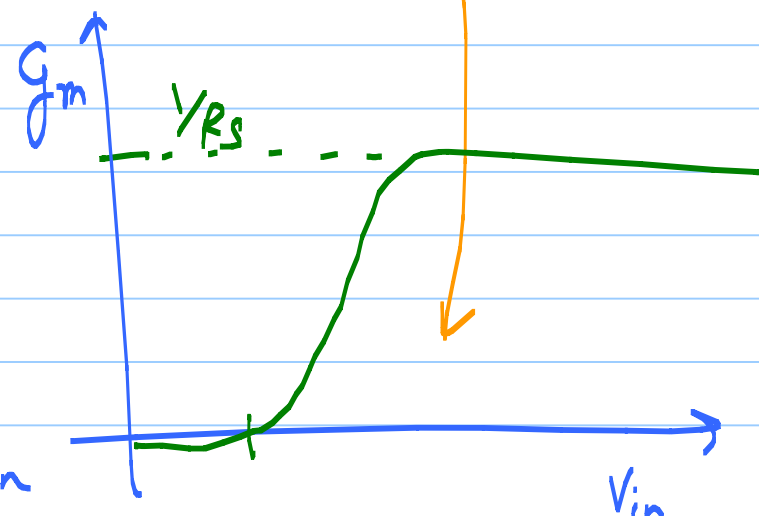
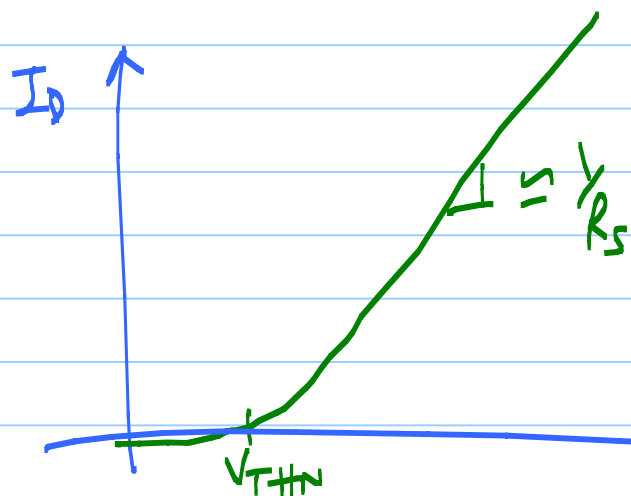
"VGA"

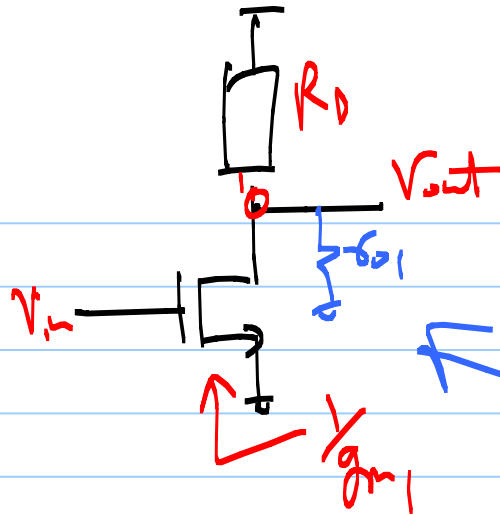


$R_S = 0$



$R_S > 0$



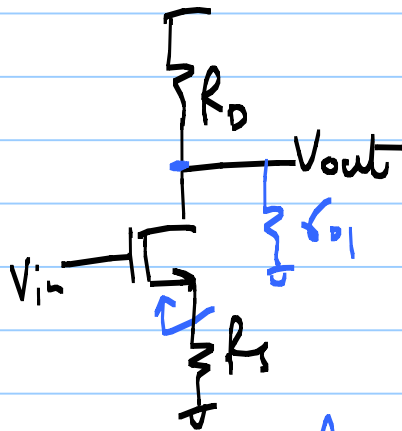
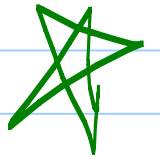


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$$A_v = - \frac{\text{Resistance seen in the drain}}{\text{Resistance seen in the source path}}$$

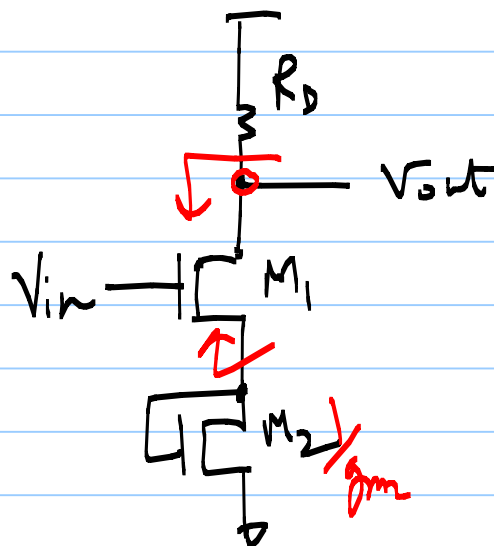
$$= - \frac{R_D || r_{o1}}{1/g_{m1}}$$

$$= - g_{m1} (R_D || r_{o1})$$

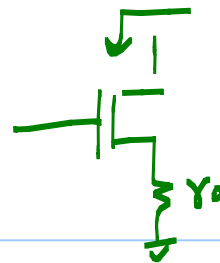


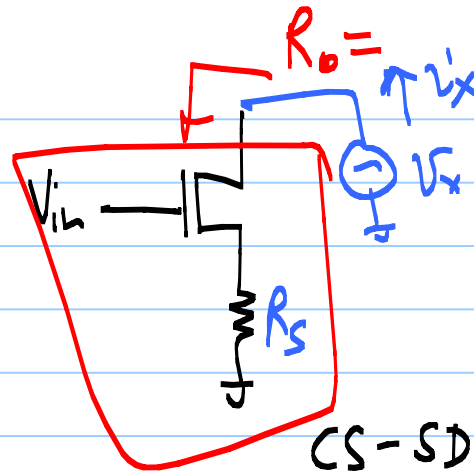
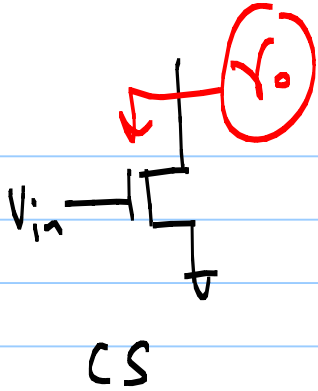
$$A_v = - \frac{(R_D || r_{o1})}{R_S + 1/g_m}$$

Ex.



$$A_v = - \frac{R_D \parallel (g_{m1} r_{o1} \cdot \frac{1}{g_{m2}})}{\frac{1}{g_{m2}} + \frac{1}{g_{m1}}}$$

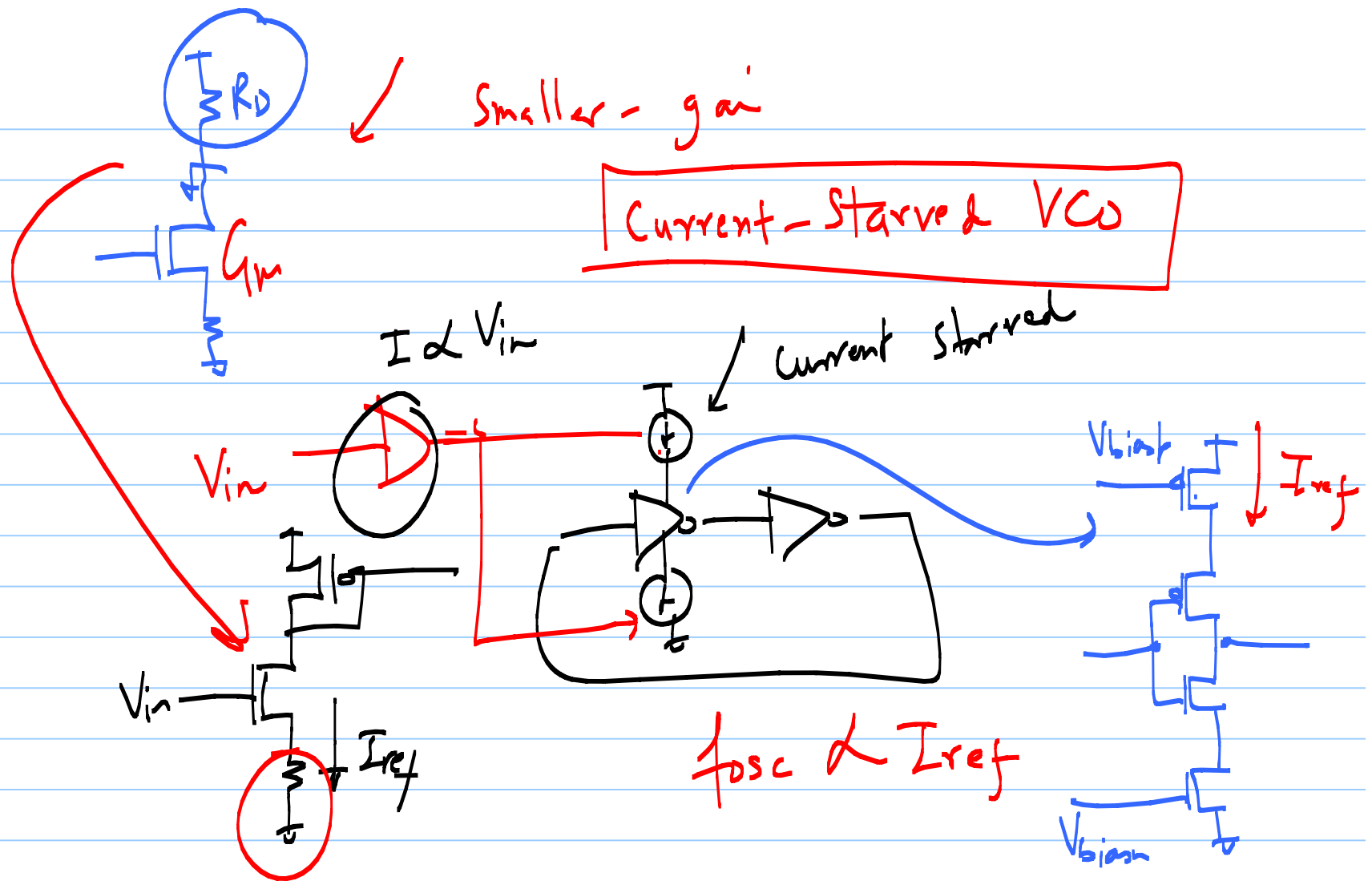




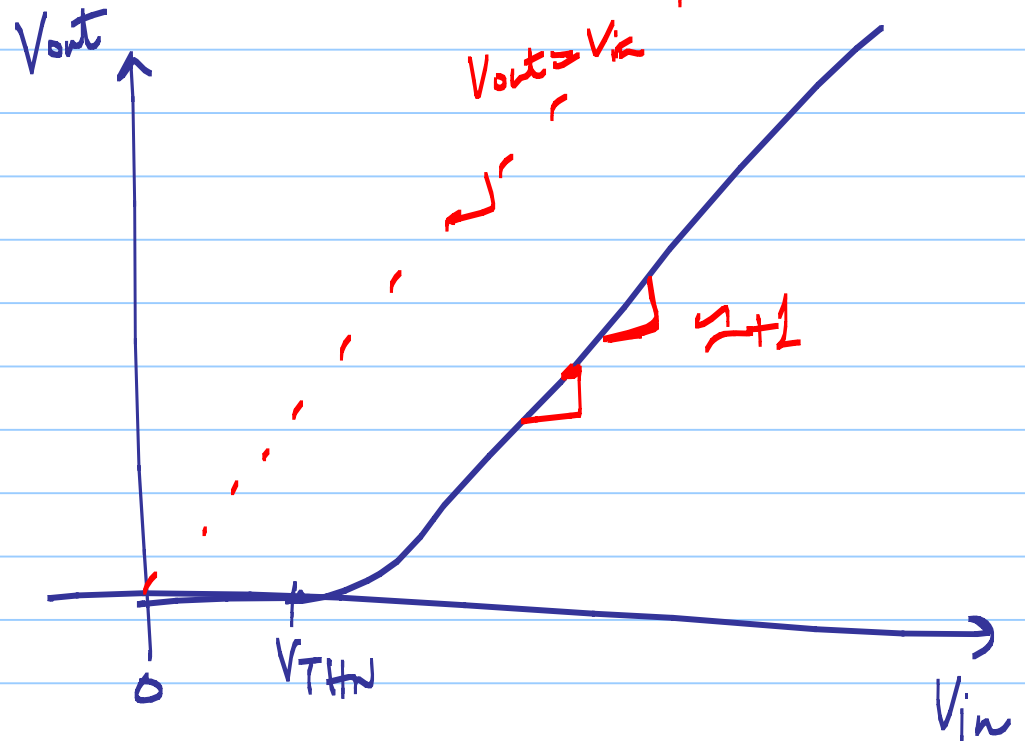
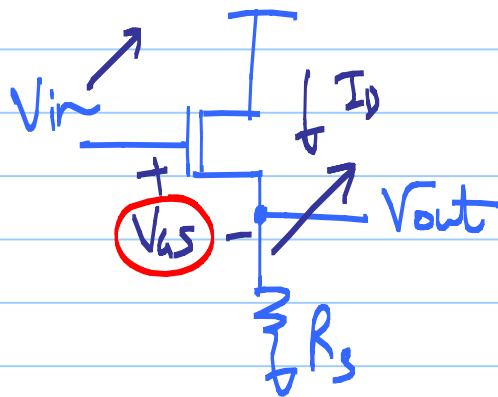
$$R_o = [1 + (g_m + g_{mb}) R_s] r_o$$

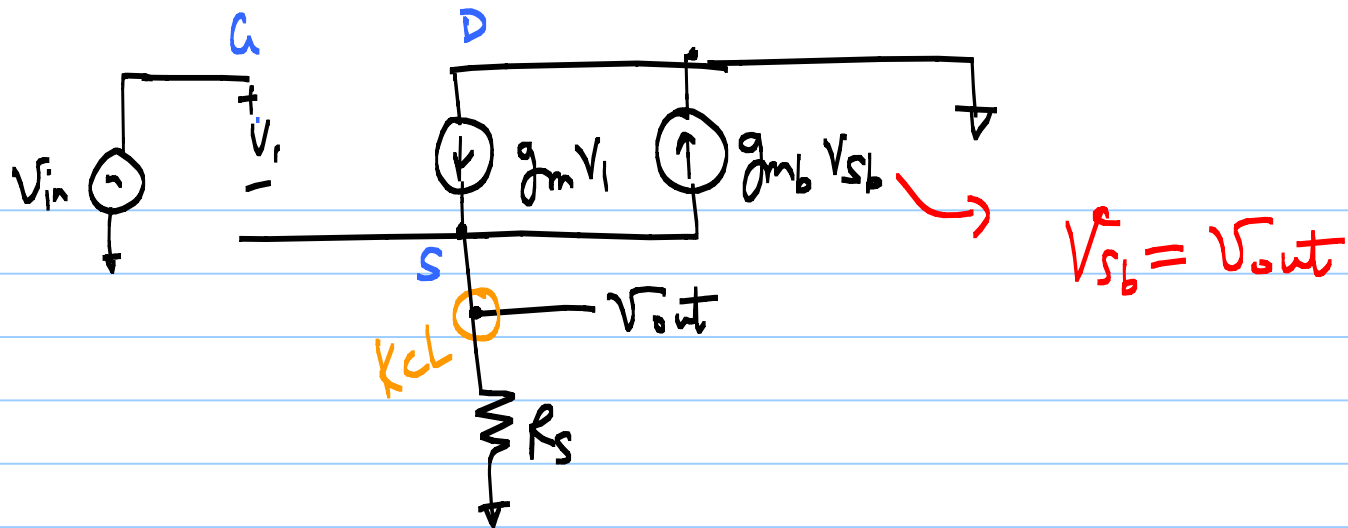
exact expression

$$\approx g_m R_s r_o = (g_m r_o) R_s \gg r_o$$



Source Follower (Common Drain Amplifier)





$$V_{in} - V_i = V_{out} \longrightarrow \textcircled{1}$$

$$g_m V_i - g_{mb} V_{out} = \frac{V_{out}}{R_S} \longrightarrow \textcircled{2}$$

$$V_{out} \left[(g_m + g_{mb}) + \frac{1}{R_S} \right] = g_m V_{in}$$

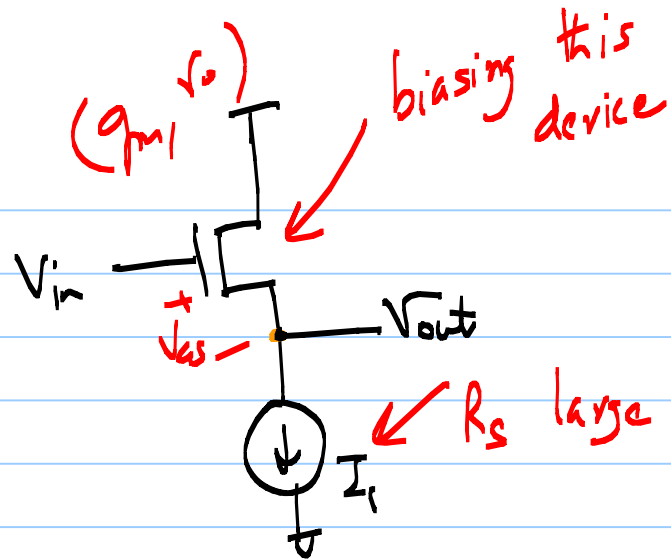
$$\Rightarrow A_v = \frac{V_{out}}{V_{in}} = \frac{g_m R_s}{1 + (g_m + g_{mb}) R_s}$$

$$g_{mb} = \eta \cdot g_m$$

$$= \frac{g_m R_s}{1 + (\eta + 1) g_m R_s}$$

$$= \frac{1}{(\eta + 1) + \left(\frac{1}{g_m R_s} \right)} \approx \boxed{\frac{1}{\eta + 1}} < 1$$

$$g_m R_s \gg 1$$

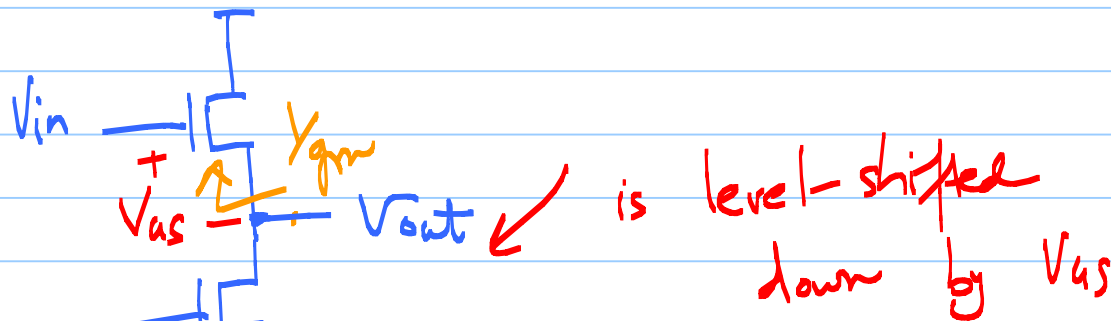


f_w $R_s \rightarrow \infty$

$A \approx + \frac{1}{\eta + 1} \approx 0.8$

$\eta \leftarrow$ body factor

$\eta = \frac{g_{mb}}{g_m}$



$V_{bias4} = V_{bias4}$