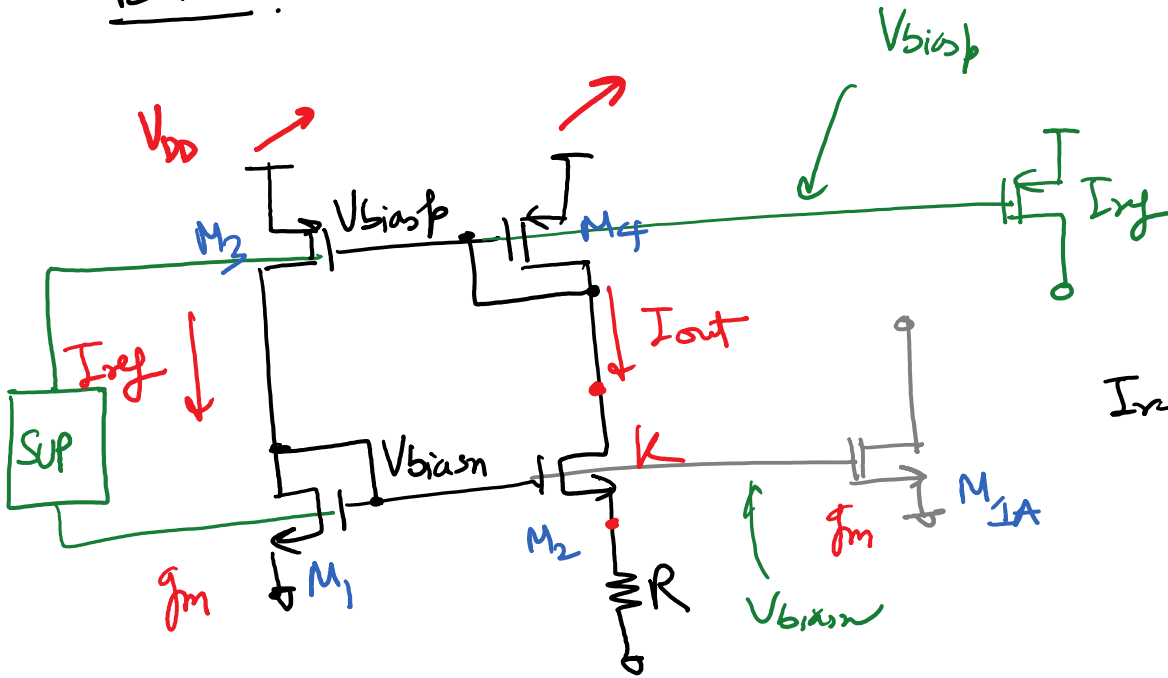


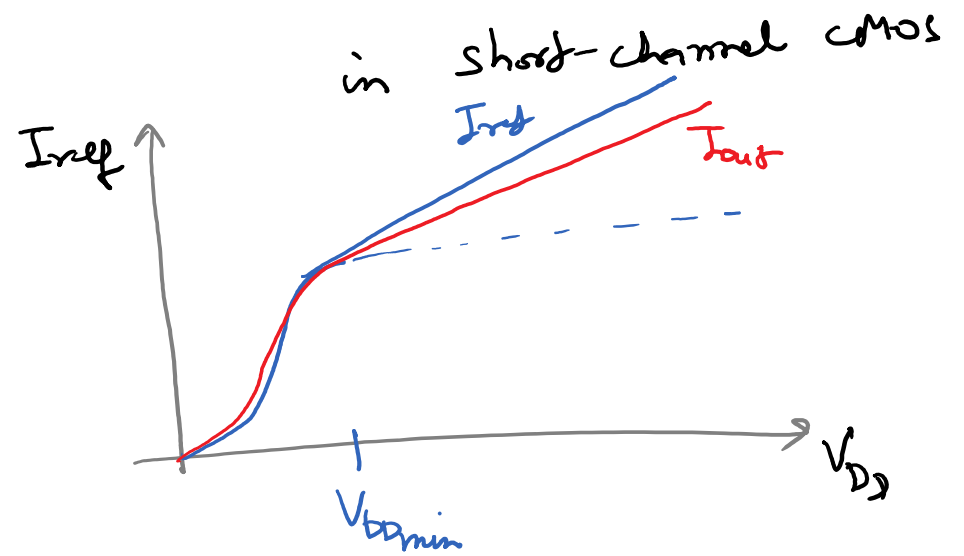
ECF 515- Lecture 7

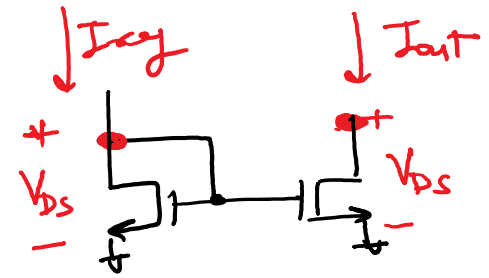
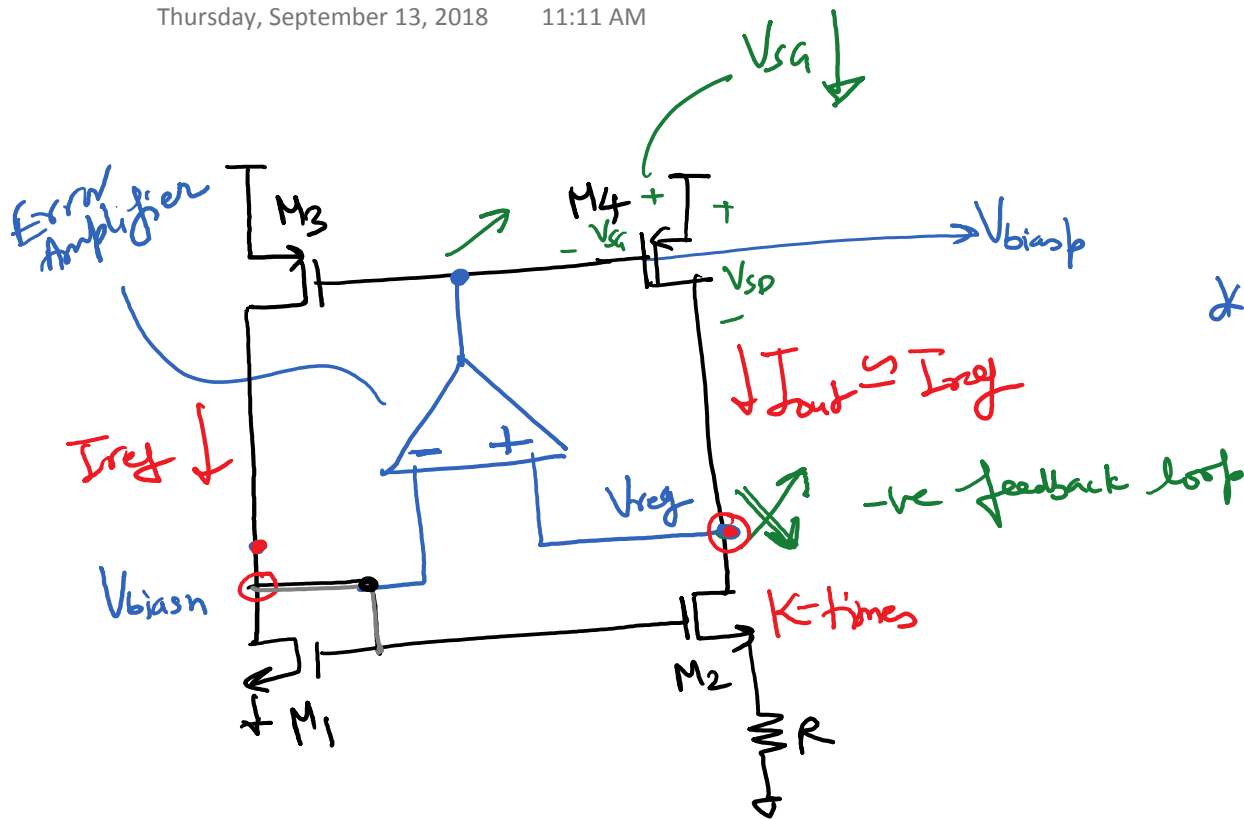
Thursday, September 13, 2018 11:02 AM

BMR .



$\lambda = 0$



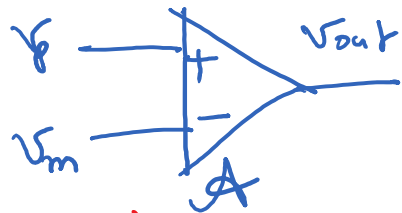


Negative feedback loop keeps V_{reg} close to V_{biasn}

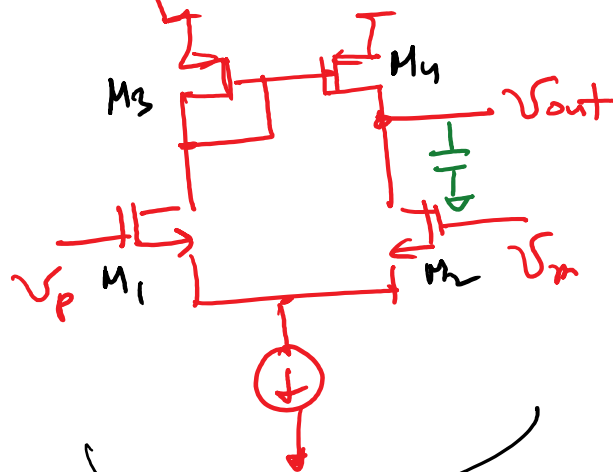
→ drains of M_3 & M_4 are at the same potential

↓
 I_{out} & I_{ref} are held closer

* effectively increasing the output resistance of the PMOS current source



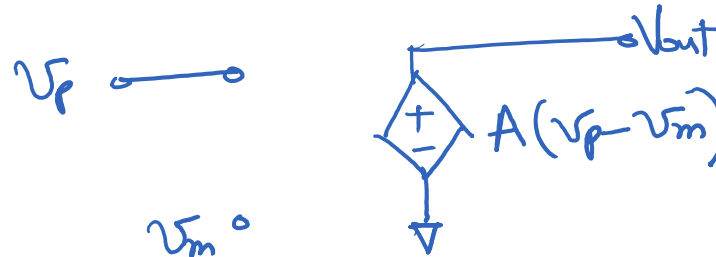
$\Rightarrow$



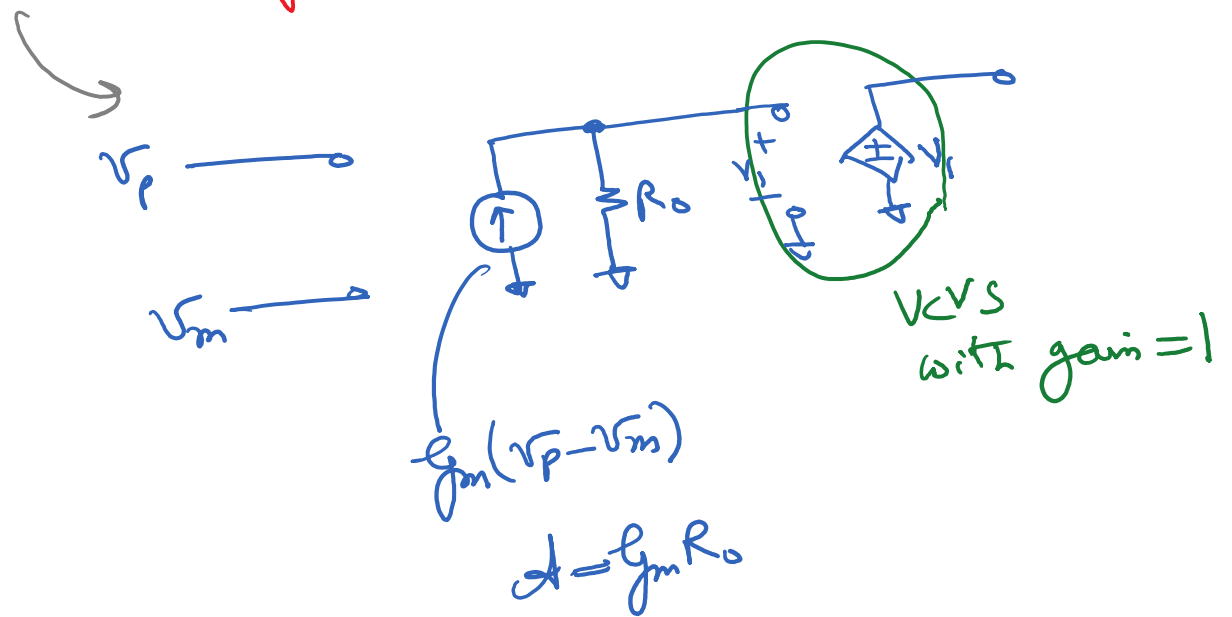
$$A_v = g_{m_{1,2}} \cdot r_{o2} \parallel r_{o4}$$

Behavioral model

analogLib

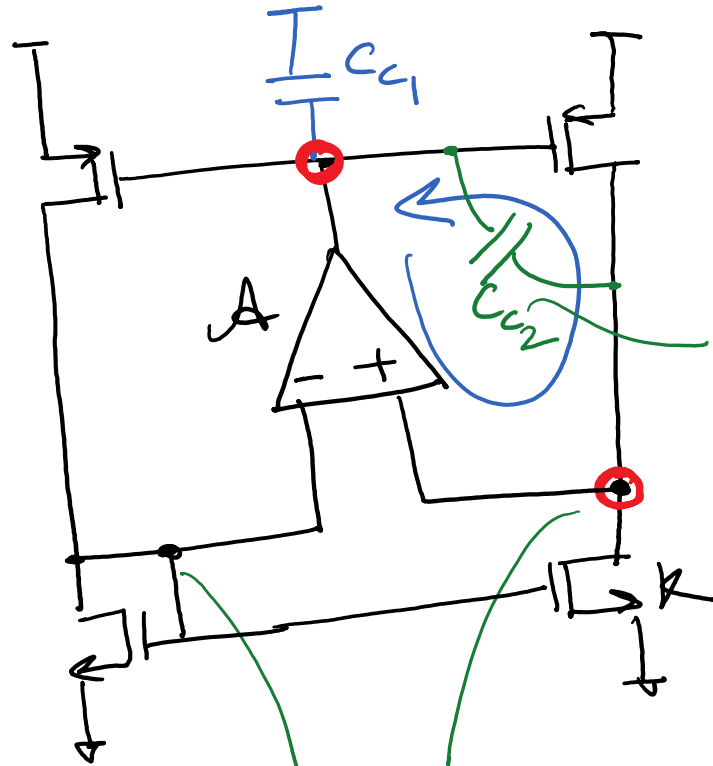


large gain $\rightarrow$ convergence



VerilogA

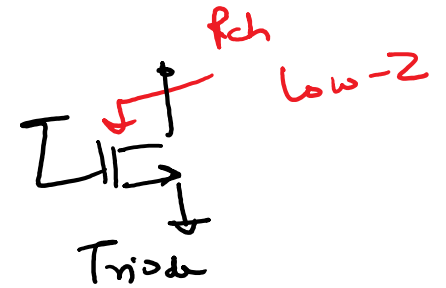
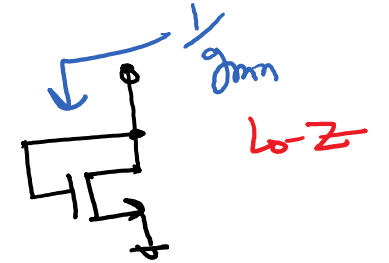
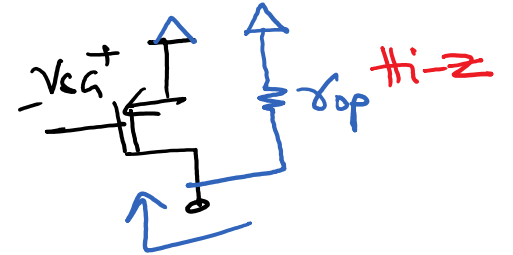
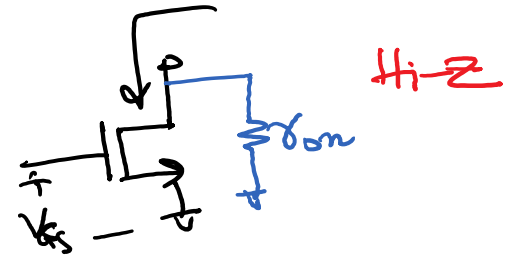
Hi-Z nodes



those nodes
back each other

ω_{p1}, ω_{p2}

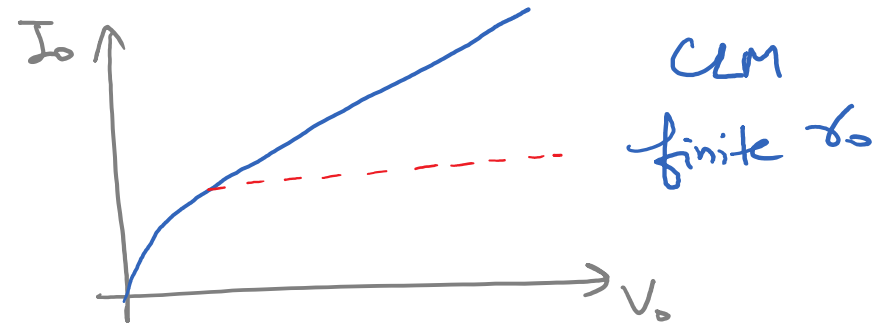
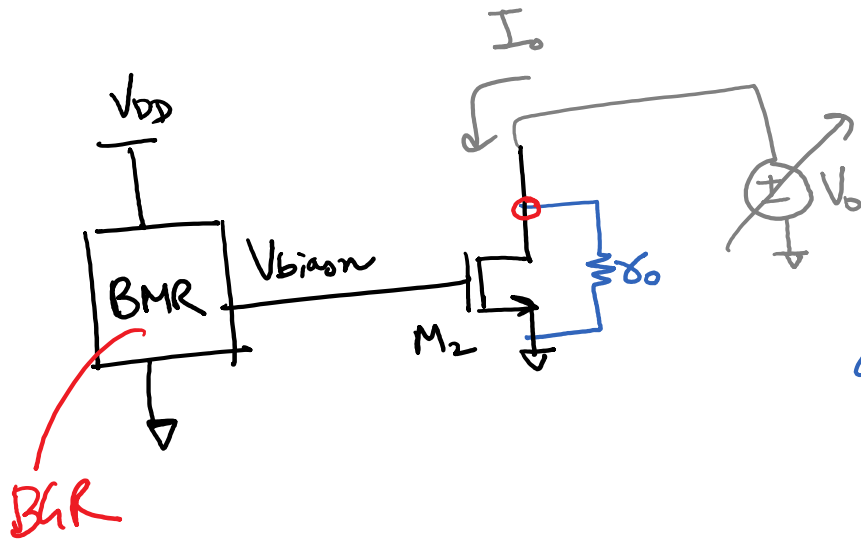
Miller Compensation
Cp



* Compensate this circuit $\Rightarrow$ make it stable.

Cascode (Cascode Current Mirrors)

Thursday, September 13, 2018 11:41 AM

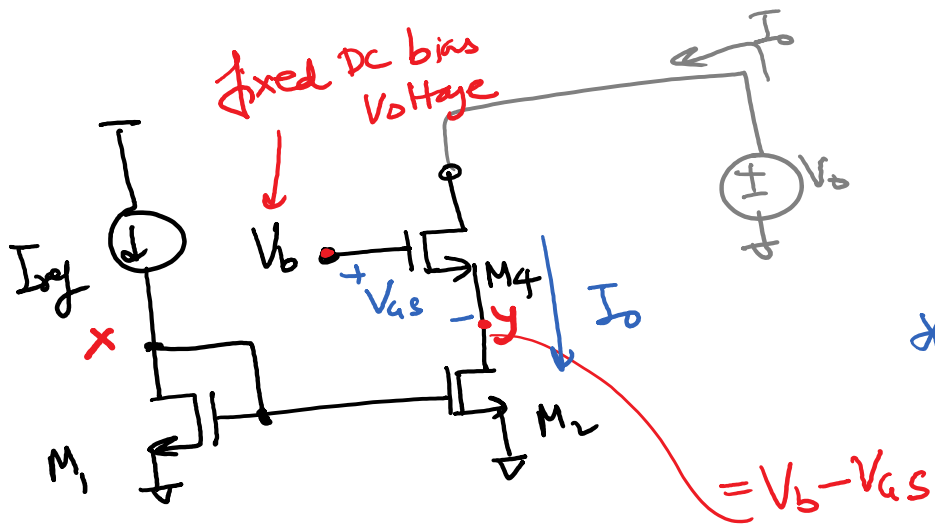
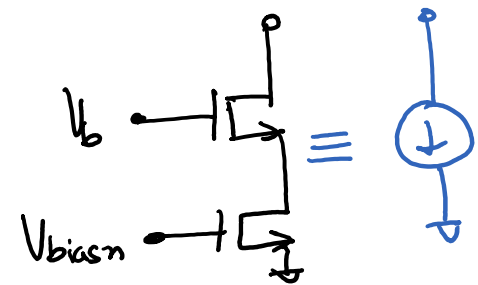


if we hold the drain of M_2 then the current I_0 will not vary
→ V_0 should be fixed
→ not useful in a circuit

ECE 515- Lecture 7

Thursday, September 13, 2018 11:46 AM

2 Transistor stack



* Add another device to hold the V_{gs} of the bottom device (M_2)

↳ leads to higher output impedance of the current mirror

$$V_x = V_{gs}$$

$$V_y = V_{gs}$$

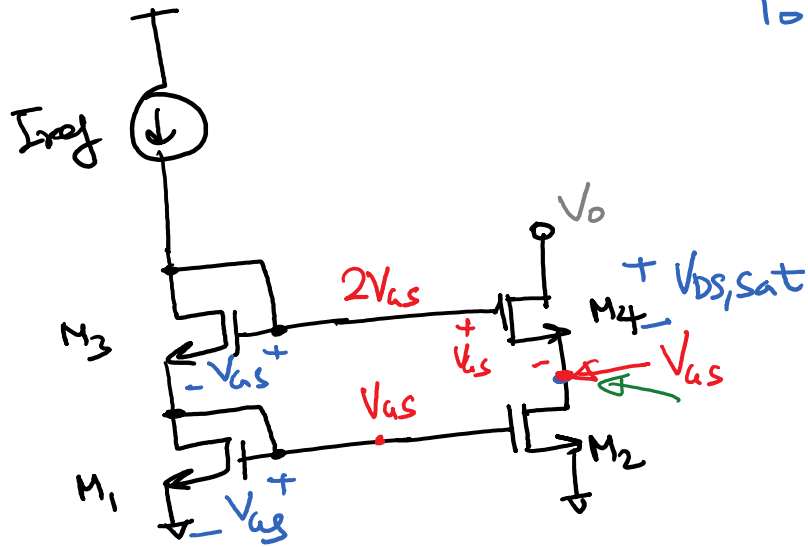
$$V_b = 2V_{gs}$$

$$\Rightarrow \text{generate } V_b = 2V_{gs}$$

$$\Rightarrow V_x \triangleq V_y$$

$$\Rightarrow I_o \text{ tracks } I_{ref}$$

Simple Cascode Current Mirror

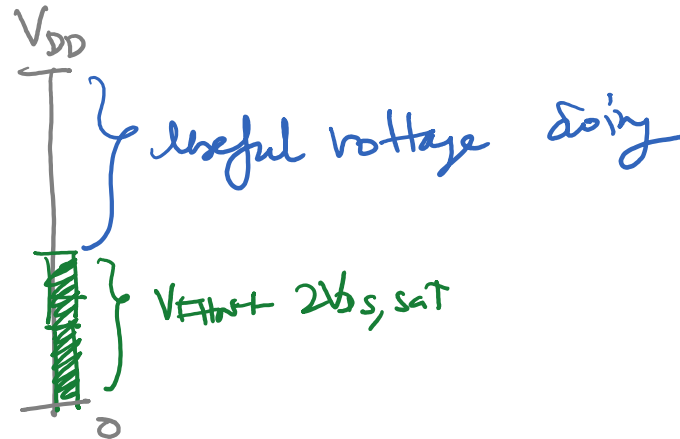


To keep M_2 & M_4 in SAT

$$V_o \geq V_{gs} + V_{ds,sat}$$

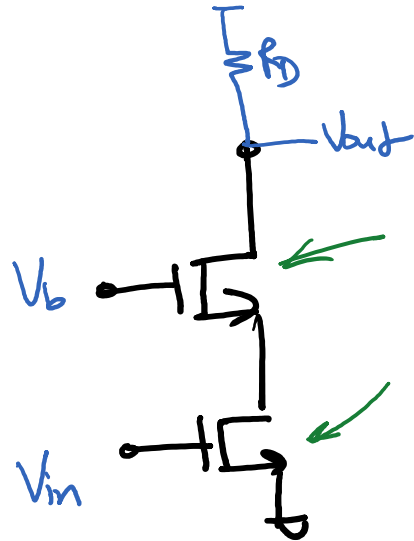
$$= (V_{ds,sat} + V_{thn}) + V_{ds,sat}$$

$$= 2V_{ds,sat} + V_{thn}$$



We are wasting our V_{thn} of voltage swing

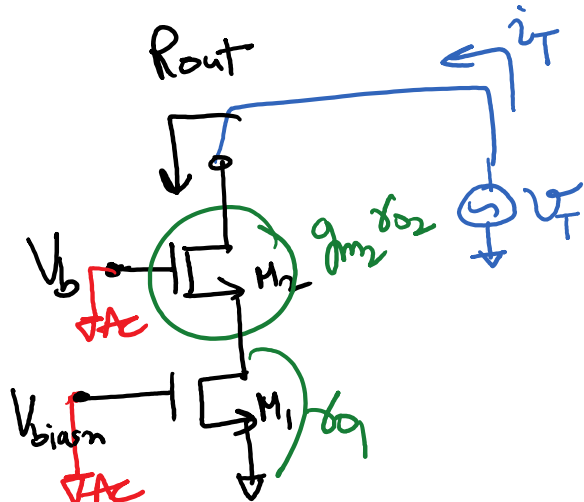
* We will optimize this current mirror later for wide swing biasing



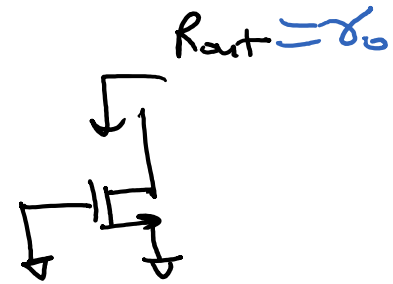
Common gate amplifier
grid

Common Source amplifier
Cathode

Cascode $\Rightarrow$ Cascade of Common Cathode and common grid
 from the vacuum tube days.

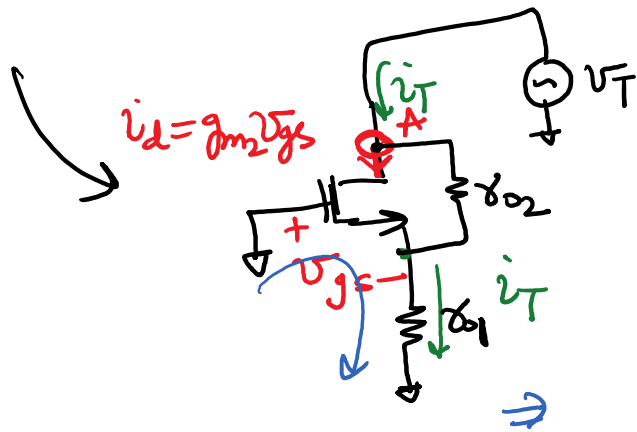


$$R_{out} \triangleq \frac{V_T}{i_T}$$



KVL: $V_{gs} + i_T r_{O1} = 0 \Rightarrow V_{gs} = -i_T r_{O1} \rightarrow \textcircled{1}$

KCL @ A: $i_T - g_{m2} V_{gs} - \frac{(V_T - i_T r_{O1})}{r_{O2}} = 0 \rightarrow \textcircled{2}$



$$i_T + g_{m2} r_{O1} i_T - \frac{(V_T - i_T r_{O1})}{r_{O2}} = 0$$

$$i_T r_{O2} + g_{m2} r_{O1} r_{O2} i_T + i_T r_{O1} = V_T$$

$$\frac{V_T}{i_T} = R_{out} = g_{m2} r_{O2} r_{O1} + r_{O1} + r_{O2}$$

$$R_{out} = (g_{m2} r_{O2}) r_{O1} + r_{O1} + r_{O2}$$

$$\approx g_{m2} r_{O2} r_{O1} \approx g_m r_o^2$$

$$r_o \rightarrow g_m r_o^2$$

σ_0 μ
 $1 \text{ kn} \rightarrow 100 \text{ kn}$
 $\text{for } \mu \sigma_0 = 100$

$$\leq \mu_2 \sigma_2 \sigma_1 \leq \mu \sigma_0$$