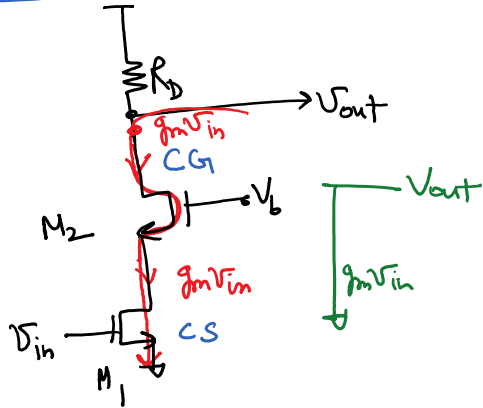


ECE 515- Lecture 13

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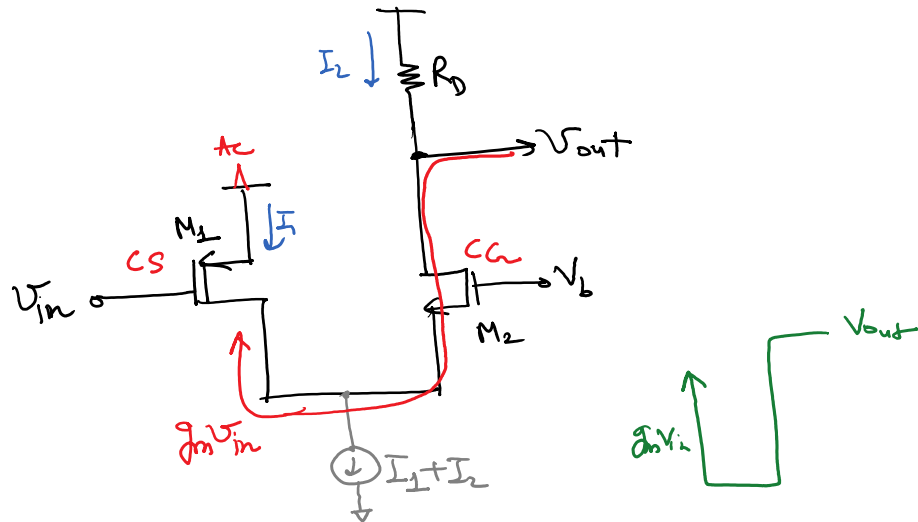
Folded Cascode:

Cascode Amplifier



M_1 & M_2 are NMOS
headroom issues

Folded Cascode



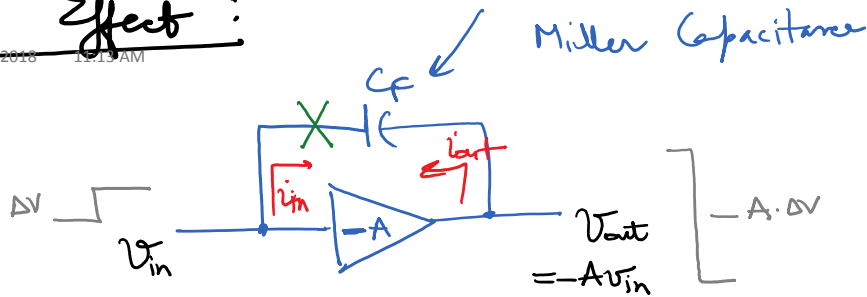
Small signal current is folded up

- (+) better voltage headroom
- (-) 2x bias current

we'll come back to this later.

Miller Effect :

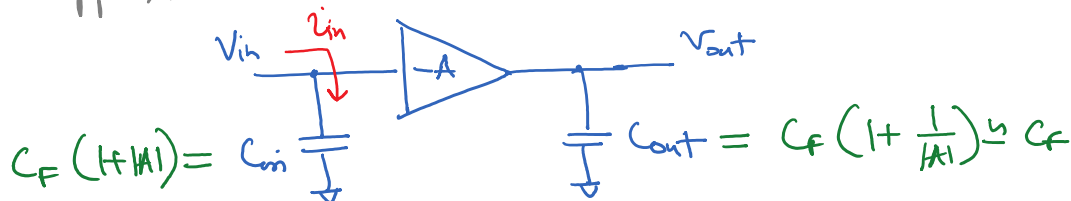
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Capacitor sees voltage change $(A+1)\Delta V$

Capacitance multiplication effect

Miller approximation



$$C_F (1+|A|) = C_{in} \quad C_{out} = C_F \left(1 + \frac{1}{|A|}\right) \approx C_F$$

$$i_{in} = \frac{V_{in} - V_{out}}{1/sC_F} = sC_F (V_{in} - V_{out}) = sC_F (1+|A|) V_{in}$$

$$i_{in} = sC_F (1+|A|) V_{in}$$

$$i_{in} = \frac{V_{in}}{Z_{in}} = \frac{1}{sC_F (1+|A|)} = \frac{1}{sC_{in}}$$

$$\Rightarrow C_{in} = C_F (1+|A|)$$

$$i_{out} = -i_{in} = -sC_F (V_{in} - V_{out})$$

$$= -sC_F \left(-\frac{V_{out}}{|A|} - V_{out}\right) = +sC_F V_{out} \left(1 + \frac{1}{|A|}\right)$$

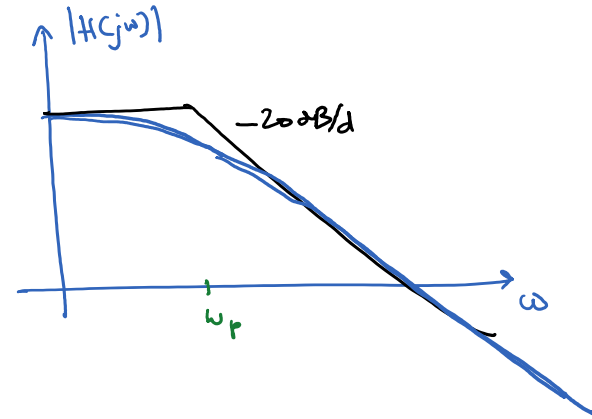
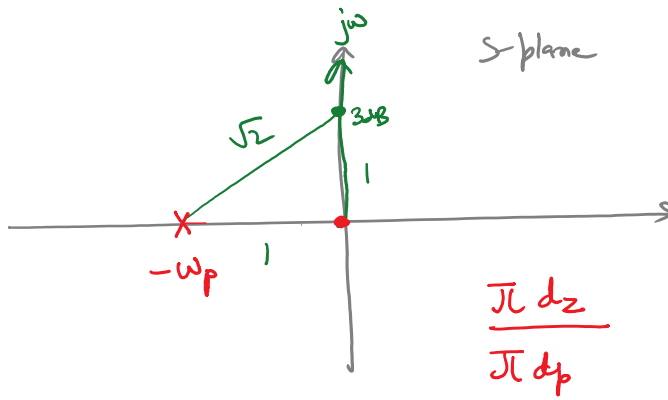
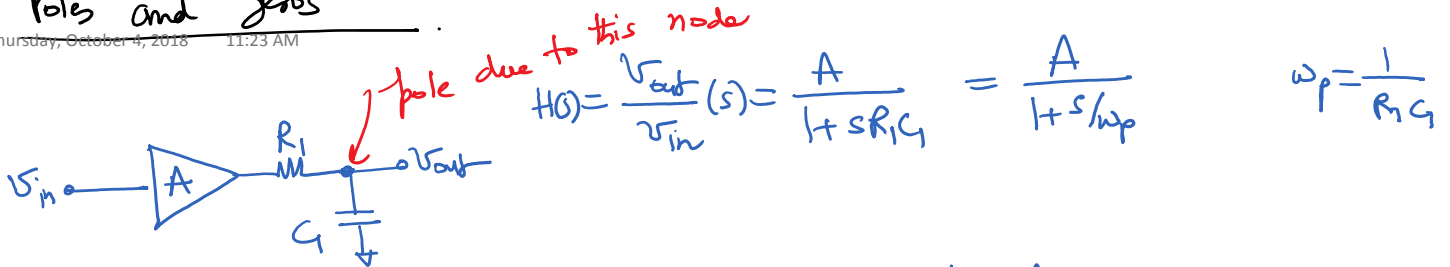
$$Z_{out} = \frac{V_{out}}{i_{out}} = \frac{1}{sC_F \left(1 + \frac{1}{|A|}\right)} = \frac{1}{sC_{out}}$$

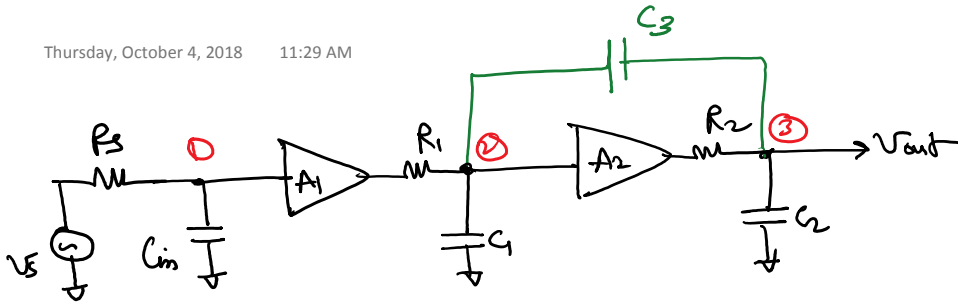
$$C_{out} = C_F \left(1 + \frac{1}{|A|}\right) \approx C_F$$

Doesn't capture the shunting of input & output at higher frequencies (misses a zero in the transfer function) for $|A| \gg 1$

Poles and Zeros

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$$\frac{V_{out}}{V_{in}}(s) = \frac{1}{1+sR_3C_{in}} \cdot \frac{A_1}{1+sR_1C_1} \cdot \frac{A_2}{1+sR_2C_2} \quad 3 \text{ poles}$$

& nodes are not interacting with each other.

Add $C_3 \rightarrow$ nodes ② & ③ are interacting with each other through C_3

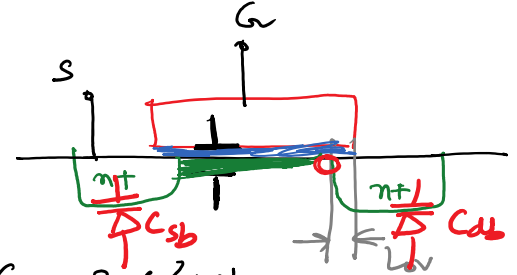
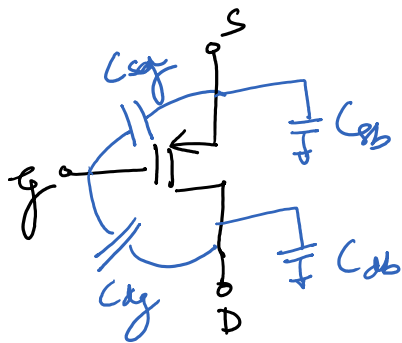
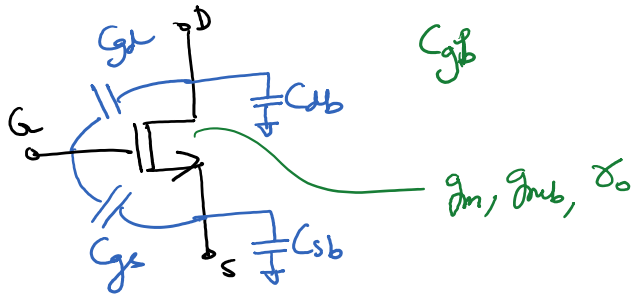
In general, we can't associate a pole to a node
 \rightarrow All the nodes contribute to all the poles.

HF MOSFET Models

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$$C_{ox} = \frac{\epsilon_0 \epsilon_{ox}}{t_{ox}}$$

NMOS:



$$C_{gs} \approx \frac{2}{3} C_{ox}' WL$$

$$C_{gd} = C_{ox}' \cdot L_{ov} \cdot W$$

$$= C_{GD0} \cdot W$$

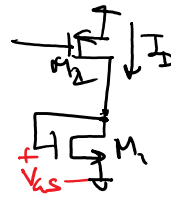
$$C_{gs} \gg C_{gd}$$

$$f_T \approx \frac{g_m}{2\pi C_{gs}}$$

CS Stage

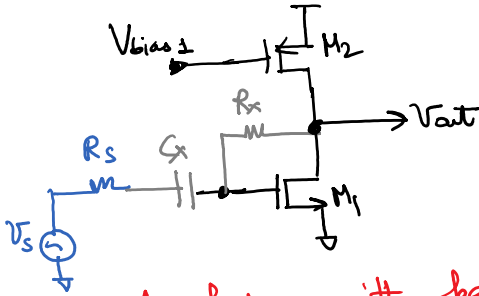
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DC



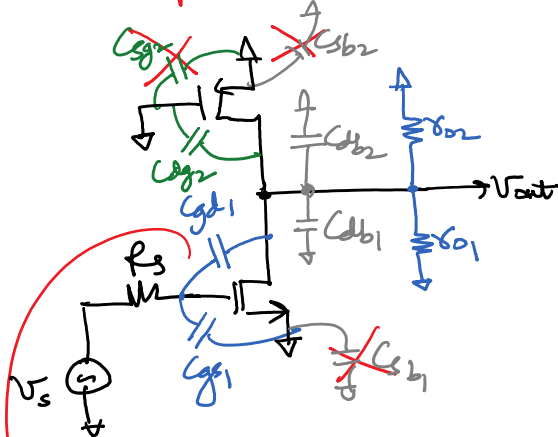
$$V_{R_x} = 0$$

M_1 is biased by the current source

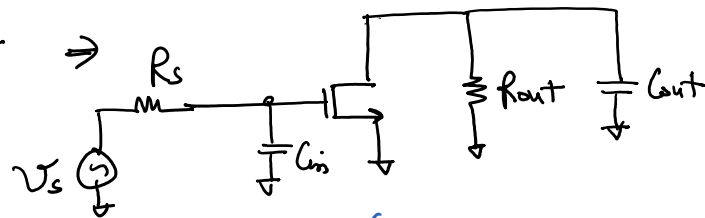


AC picture with parasitic caps

Let's apply Miller approximation



Miller Cap ΔC_{gd1}



$$R_{out} = r_{o1} || r_{o2}$$

$$C_{in} = C_{gs1} + C_{gd1} (1 + A)$$

$$C_{out} = C_{gd1} (1 + \frac{1}{A}) + C_{db1} + C_{db2} + C_{gs2}$$

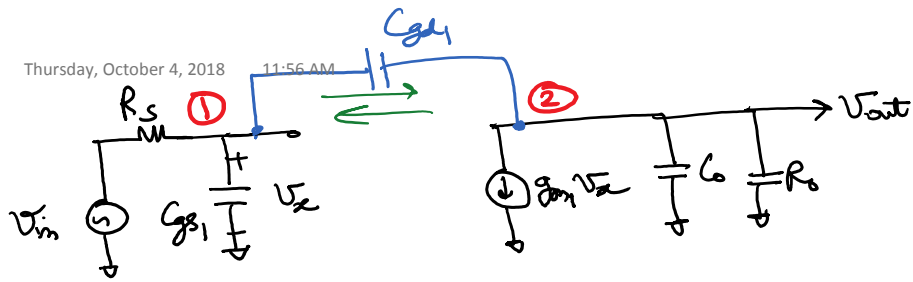
$$A = -g_{m1} r_{o1} || r_{o2}$$

$$\omega_{in} = \frac{1}{R_s C_{in}} = \frac{1}{R_s [C_{gs1} + (1 + A) C_{gd1}]}$$

$$\omega_{out} = \frac{1}{R_{out} C_{out}} = \frac{1}{(r_{o1} || r_{o2}) [C_{gd1} + C_{db1} + C_{db2} + C_{gs2}]}$$

$$\frac{V_{out}}{V_{in}}(s) = \frac{-A}{(1 + \frac{s}{\omega_{in}}) (1 + \frac{s}{\omega_{out}})}$$

But this result is erroneous
→ we are missing a zero in the circuit



Write nodal equations at ① & ②

$$\textcircled{1} \frac{V_x - V_{in}}{R_s} + V_x s C_{gs1} + (V_x - V_{out}) s C_{gd1} = 0$$

$$\textcircled{2} (V_{out} - V_x) s C_{gd1} + g_m V_x + V_{out} \left(\frac{1}{R_o} + s C_o \right) = 0$$

Solve for V_x in ① and substitute in ②

$$V_x = - \frac{V_{out} (s C_{gd1} + \frac{1}{R_o} + s C_o)}{g_m - s C_{gd1}}$$

$$\frac{V_{out}}{V_{in}}(s) = \frac{(s C_{gd1} - g_m) R_o}{R_s R_o \xi s^2 + [R_s (1 + g_m R_o) C_{gd1} + R_s C_{gs1} + R_o (C_{gd1} + C_o)] s + 1} \quad D(s)$$

$$\xi = C_{gs1} C_{gd1} + g_m C_o + C_{gd1} C_o$$

2nd order transfer function

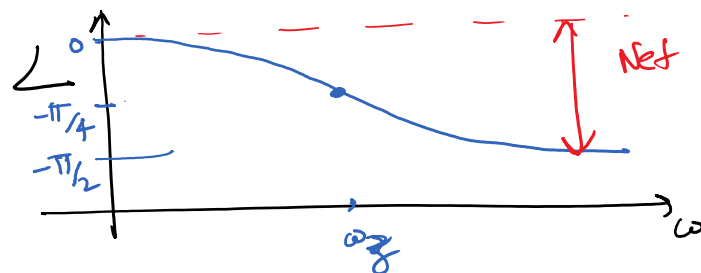
Set $N^x = 0$
Numerator

$$s C_{gd1} - g_m = 0 \Rightarrow \omega_z = \frac{+g_m}{C_{gd1}}$$

Right half s-plane
RHP zero

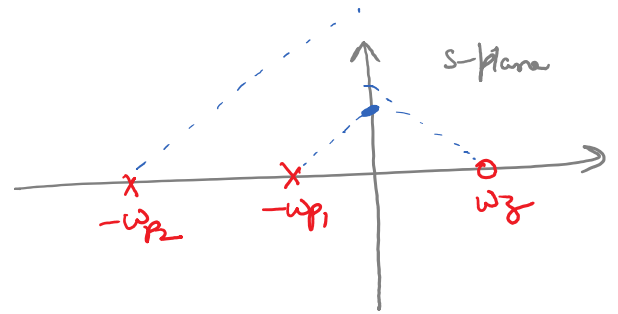
$$\Rightarrow N(s) = -g_m R_o \left(1 - \frac{s}{\omega_z} \right)$$

$$\text{phase shift} = \tan^{-1} \left(\frac{\omega/\omega_z}{1} \right) = -\tan^{-1} \left(\frac{\omega}{\omega_z} \right)$$



Net phase shift is $-\pi/2$
 -90°

Denominator, $D(s)$
2nd order system



If we assume $|w_{p1}| \ll |w_{p2}|$

$$D(s) = \left(\frac{s}{w_{p1}} + 1\right) \left(\frac{s}{w_{p2}} + 1\right)$$

$$= \frac{s^2}{w_{p1}w_{p2}} + \underbrace{\left(\frac{1}{w_{p1}} + \frac{1}{w_{p2}}\right)}_{\approx \frac{1}{w_{p1}}} s + 1$$

If $w_{p1} \ll w_{p2} \Rightarrow \frac{1}{w_{p1}} \gg \frac{1}{w_{p2}}$

$$w_{p1} = \frac{1}{R_s(1+g_m R_o)C_{gd1} + \underbrace{R_o C_{gs1}}_{\text{Extra term}} + R_o(C_{gd1} + C_o)}$$

Compare with

$$w_{in} = \frac{1}{\underbrace{R_s C_{gs1}} + \underbrace{(1+g_m R_o) R_s C_{gd1}}}$$