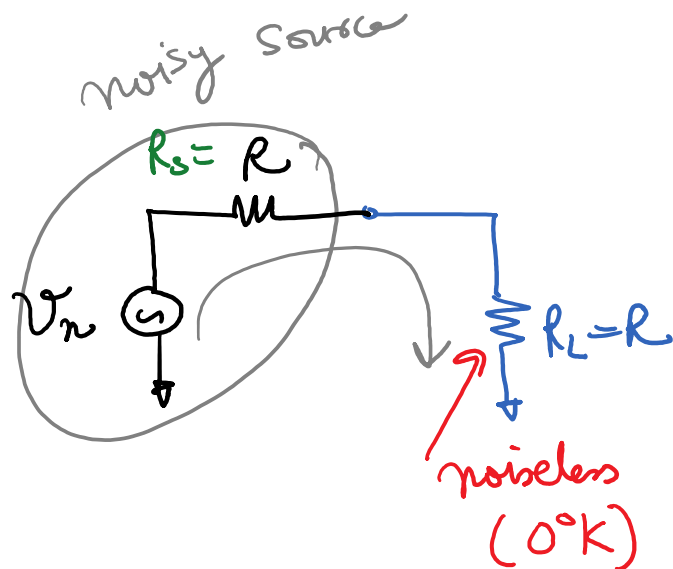


ECE 513 - Lecture 8

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Available noise power: power that can be transferred from a noise source to a "conjugately matched" "noiseless" load.

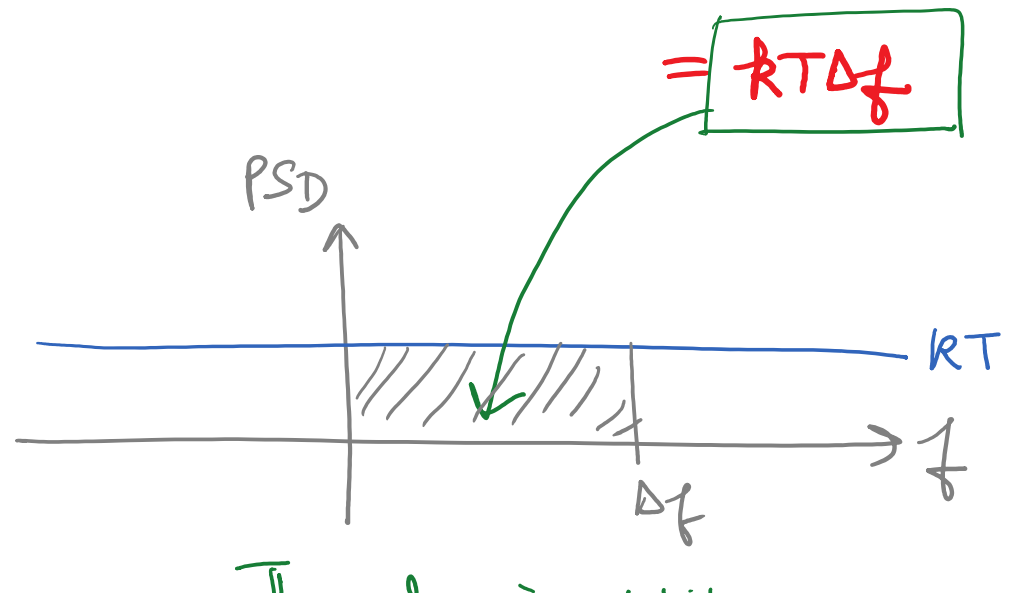
↳ so that the load don't reflect back its own noise



$$R_s = R + jX$$

$$R_L = R - jX$$

$$P_{available} = \frac{V_n}{2} \cdot \frac{V_n^*}{2R} = \frac{|V_n|^2}{4R} = \frac{\cancel{4kTR} \cdot \Delta f}{\cancel{4R}}$$



$$R_L = R - jX$$

for maximum power transfer

1 ω_f .
Thermal noise - white noise

Noise Figure

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Noise factor:

Signal-to-noise-ratio
SNR

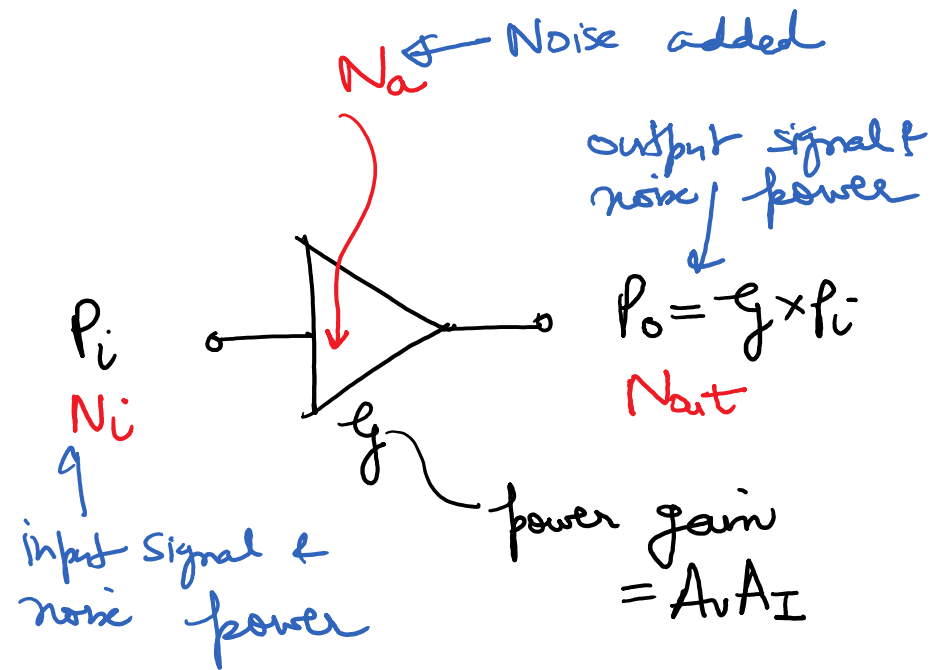
$$SNR_i = \frac{P_i}{N_i}$$

$$SNR_o = \frac{P_o}{N_{out}} = \frac{g \cdot P_i}{g N_i + N_a}$$

$$F = \frac{SNR_i}{SNR_o} = \frac{\cancel{P_i}}{N_i} \times \frac{g N_i + N_a}{\cancel{g P_i}}$$

$$\Rightarrow F = 1 + \frac{N_a}{g N_i} \geq 1$$

$$NF = 10 \log F$$



A lower 'F' the better

(dB)

Noise figure

$$NF = 10 \log_{10} F$$

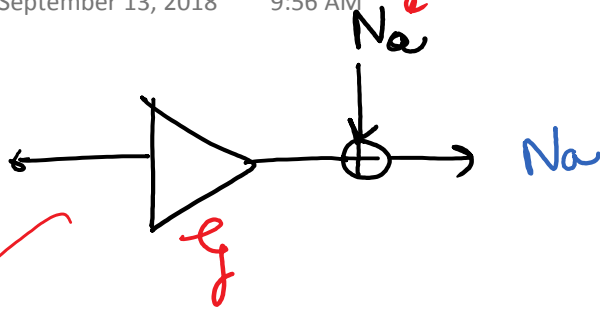
(dB)

Noise Temperature:

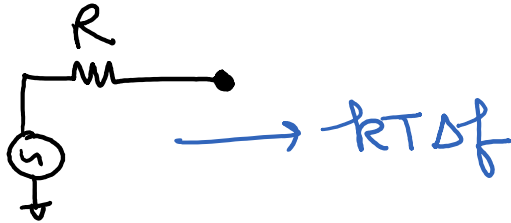
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added noise by the circuit



Equivalent temperature for a block as if all the noise is generated due to thermal noise.



$$kT_e \Delta f G = N_a$$

$$T_e = \frac{N_a}{k G \Delta f}$$

Equivalent
"Noise Temperature"

has nothing to do with the actual physical temperature.

$$F = 1 + \frac{N_a}{g N_i}$$

$$= 1 + \frac{\cancel{k g T_e \Delta f}}{g \cdot (\cancel{k T \Delta f})}$$

$$= 1 + \frac{T_e}{T}$$

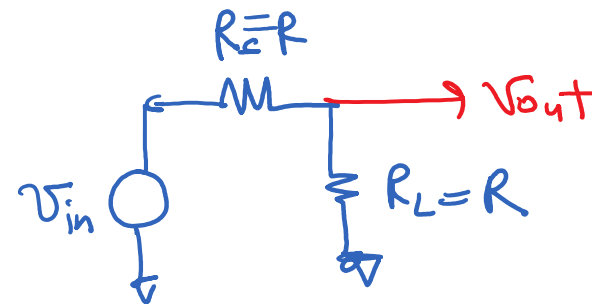
noise temperature
of the circuit

ambient temp.
of the source

physical temp

$$F = 1 + \frac{T_e}{T}$$

$$\Rightarrow T_e = (F-1)T$$

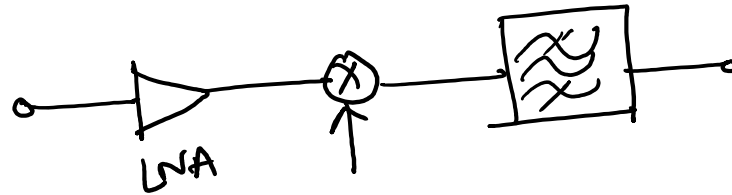
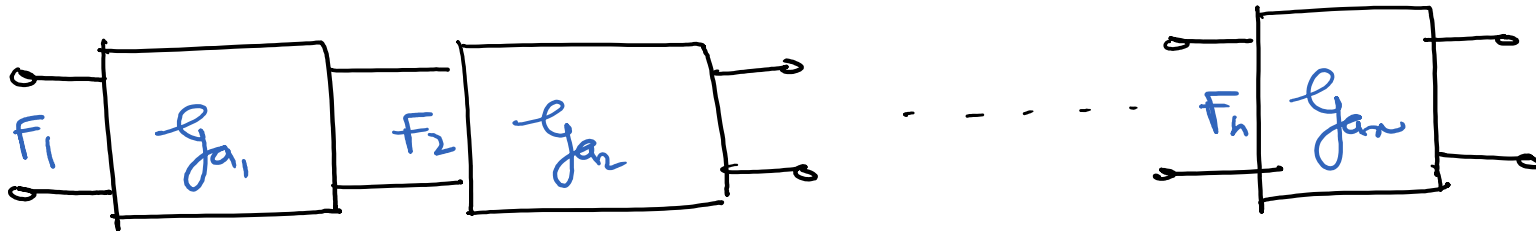


$$F = 2$$

$$NF = 3dB$$

Noise factor of a Chain of Two-ports

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Need to calculate: the noise factor (figure) of the entire Rx chain as a function of F and gain of the individual blocks in the Rx chain.

$$\text{Total output Noise} = [((kT_{e1}\Delta f g_{a1} + kT_{e2}\Delta f)g_{a2} + kT_{e3}\Delta f)g_{a3} + \dots + kT_{en}\Delta f]g_{an}$$

$$\triangleq kT_e \Delta f \cdot g$$

$$g = g_{a1} \times g_{a2} \times g_{a3} \dots \times g_{an}$$

→ Noise temp of the full Rx chain

$$T_e = \frac{N_{out}}{k \Delta f g_{a1} g_{a2} \dots g_{an}} = T_{e1} + \frac{T_{e2}}{g_{a1}} + \frac{T_{e3}}{g_{a1} g_{a2}} + \dots + \frac{T_{en}}{g_{a1} g_{a2} \dots g_{an-1}}$$

$$\therefore T_e = (F-1)T$$

$$(F-1)T = (F_1-1)T + \frac{(F_2-1)T}{g_{a1}} + \frac{(F_3-1)T}{g_{a1} g_{a2}} + \dots + \frac{(F_n-1)T}{g_{a1} g_{a2} \dots g_{an-1}}$$

$$F = F_1 + \frac{(F_2-1)}{g_{a1}} + \frac{(F_3-1)}{g_{a1} g_{a2}} + \dots + \frac{(F_n-1)}{g_{a1} g_{a2} \dots g_{an-1}}$$

Friis formula

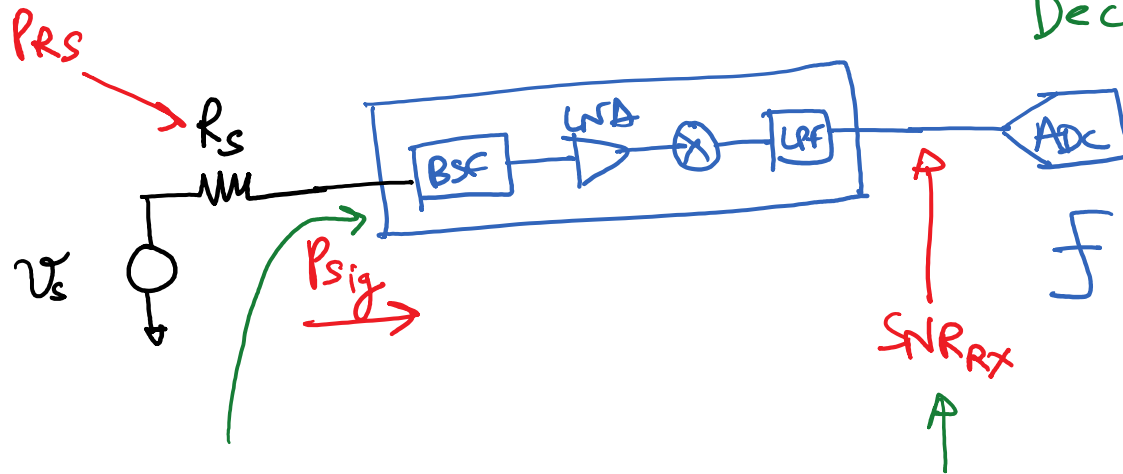
$$F = f_1 + \frac{(f_2 - 1)}{g_{a_1}} + \frac{(f_3 - 1)}{g_{a_1} g_{a_2}} + \dots + \frac{(f_n - 1)}{g_{a_1} g_{a_2} \dots g_{a_{n-1}}}$$

Friis
formula

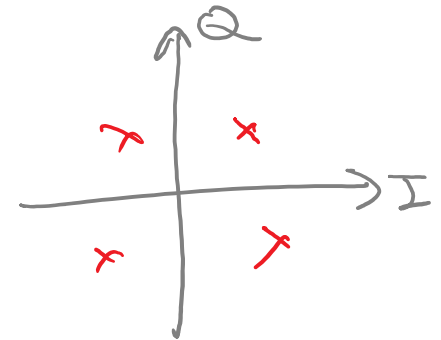
Receiver Sensitivity:

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Decision circuit at the baseband



* Sensitivity is the minimum input signal that a Rx can detect with "acceptable quality"

↳ sufficient SNR at the decision circuit

↳ determines how much BER the Rx can provide

bit error rate

$P_{sig} \Rightarrow$ Signal power p.u. Hz

$P_{rs} \Rightarrow$ Source noise p.u. Hz

$$F = \frac{SNR_{in}}{SNR_{out}} = \frac{P_{sig}/P_{rs}}{SNR_{out}}$$

$$\Rightarrow P_{sig} = P_{rs} \cdot F \cdot SNR_{out}$$

$$P_{sig,tot} = P_{sig} \cdot \Delta f = \underbrace{P_{rs}}_{kT} \cdot F \cdot \Delta f \cdot SNR_{out}$$

Signal power
at the
Rx input

$$P_{sig,tot} = F \cdot kT \cdot \Delta f \cdot SNR_{out}$$

SNR at the decision
circuit

SNR_{Rx} or SNR_{min}

Sensitivity, $S_i = F \cdot kT \cdot \Delta f \cdot SNR_{min}$

$$S_i = F \cdot kT \cdot \Delta f \cdot SNR_{min}$$

taking
 $10 \log_{10}()$ on
 both sides

$$P_{sen} \Big|_{dBm} = 10 \log_{10}(kT) + \underbrace{10 \log_{10} F}_{NF} + 10 \log_{10} \Delta f + 10 \log_{10} SNR_{min}$$

at 290K

$$P_{sen} \Big|_{dBm} = -174 \text{ dBm} + NF \Big|_{dB} + 10 \log_{10} \Delta f \Big|_{Hz} + SNR_{min} \Big|_{dB}$$

at 290K

Noise floor of the receiver