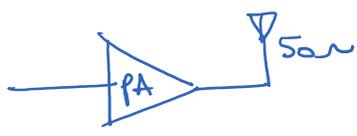


Power Amplifiers:

* Tuned power amplifiers

↳ Key component in TX path of wireless communication systems and radars

↳ Deliver the power required to transmit information to the antenna with high-efficiency and linearity over BWs of 20-20% of the center frequency.

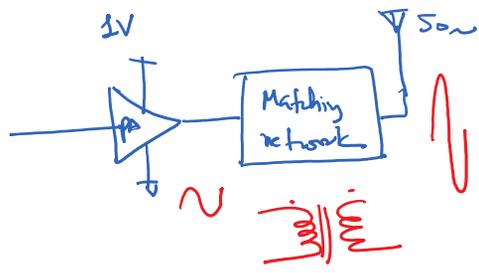


$$P_{out} = 1W \rightarrow +30 \text{ dBm}$$

$$P_{out} = \frac{V_{DD}^2}{Z_0}$$

$$V_{pp} = 2V_{DD}$$

$$V_{DD} = \sqrt{1W \times 50\Omega} = 5\sqrt{2} \text{ V}$$



Johnson's limit

$$V_{DD} \times f_T \leq 200 \text{ GHz} \cdot \text{V for Silicon}$$

* GaAs HEMT, SiGe HBT (recently), GaN

* Still challenging in CMOS to obtain high TX power and efficiency

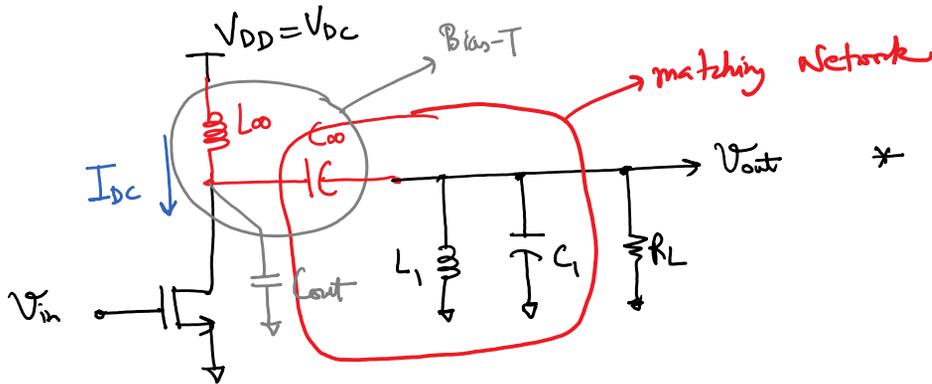
* Base station PAs still dominated by GaAs HBTs.

* TWT (Traveling wave ^{Vacuum} tubes) for very high power applications. i.e. Satellite

* TWT (Traveling wave ^{Vacuum} tube) for very high power applications.
ie Satellite

Class-A PA

Thursday, November 29, 2018 9:47 AM



* C_{oo}, L_1, C_1 form a matching network that matches transistor R_{out} to the load $R_L = Z_0 = 50\Omega$

* Very large CS transistor operating under large signal conditions with large output swing.

* The drain is biased through a bias-T

L_o presents an infinite inductance to V_{DD} and an infinite capacitance towards the load.

$$X_L = (j\omega_o L)$$

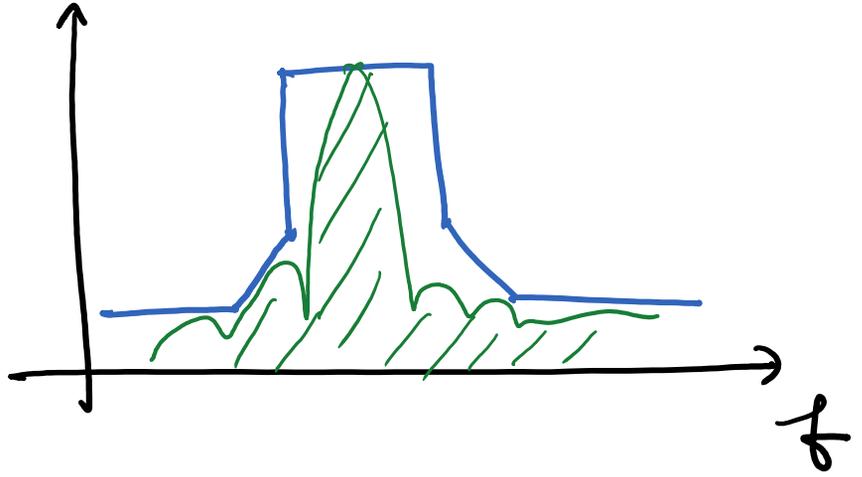
L_o is loaded with a parallel RLC tank (R_L, C_1, L) at the frequency of interest.

* Due to strongly nonlinear behavior, a simulation driven design methodology is required for PA design.

* [1] Cripps

PSD Mask

PSD



Tuned PA Fundamentals:

Class A-F PAs

* Each class of PA has different linearity and thus it's hard to compare them

* Output power, P_{out}

* Power gain, G

* Carrier frequency, f

* Linearity (OP_{1dB})

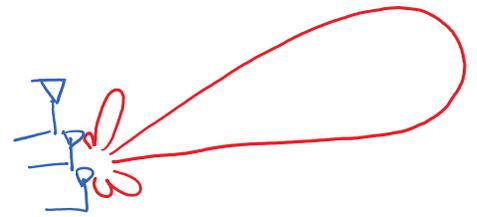
IP_3, OIP_3

* Power-added efficiency (PAE)

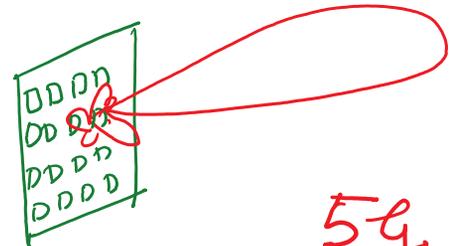
* Power backoff efficiency

* SiGe BiCMOS

$\nabla \rightarrow 1W$



∇ 1D Beamforming Array



5g

$$* FOM_{PA} = P_{out} \cdot G \cdot PAE \cdot f^2$$

To compensate for the 20dB/dec roll-off of the transistor power gain as a function of

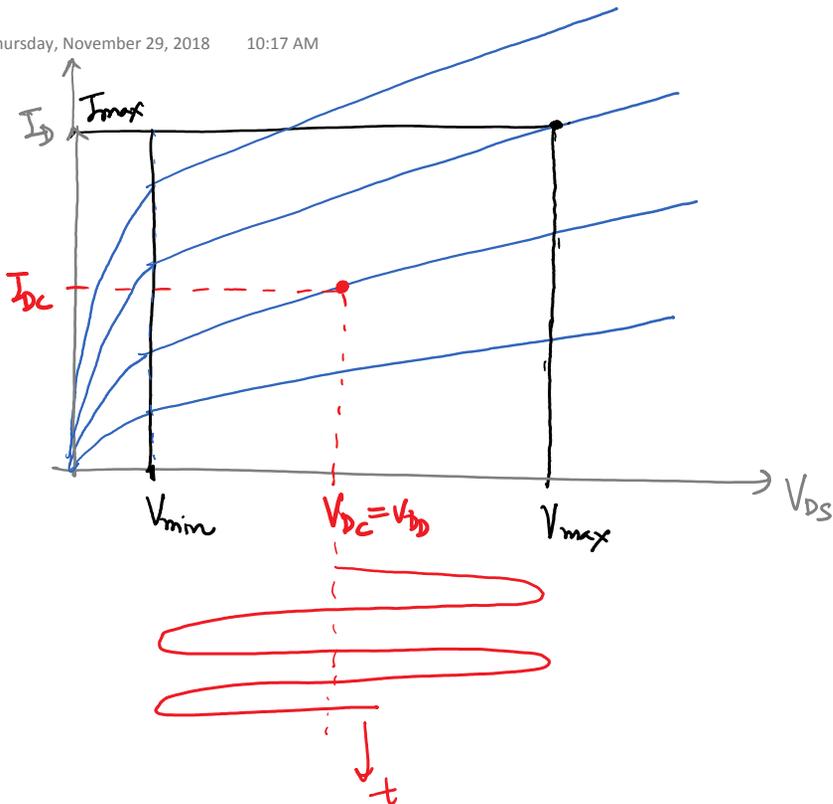
frequency, a factor of f^2
is included in the FOM.

* Linearity is not included as
its class-dependent.

* Drain-efficiency $\eta_{\text{drain}} = \frac{P_{\text{out}}}{P_{\text{DC}}}$

* power added efficiency (PAE) $\stackrel{P}{=} \frac{P_{\text{out}} - P_{\text{in}}}{P_{\text{DC}}}$

As the gain $g \rightarrow \infty \Rightarrow \text{PAE} \rightarrow \eta_{\text{drain}}$



$V_{min} \Rightarrow$ Triode region
 $V_{DS,sat}$

$V_{max} \Rightarrow$ maximum allowed V_{DS}
 \hookrightarrow breakdown or reliability concerns

$I_{max} \Rightarrow$ output current going
 \hookrightarrow depends upon the saturation velocity & carrier mobility etc.

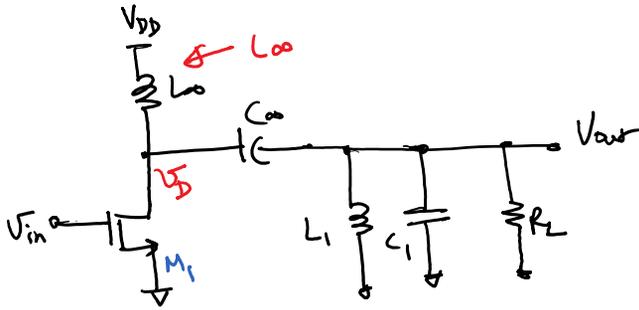
* $I_{max} \rightarrow$ limited by f_t degradation due to high-injection effects and doesn't exceed $2J_{pft}W$

$P_{out} \propto (V_{max} - V_{min}) I_{max}$

and $PAE \propto \left(1 - \frac{V_{min}}{V_{max}}\right)$

* Ideally, we must select the transistor technology with the largest V_{max} and I_{max}

and ideally $V_{min} = 0$ & $R_{on} = 0$
 \hookrightarrow switch resistance

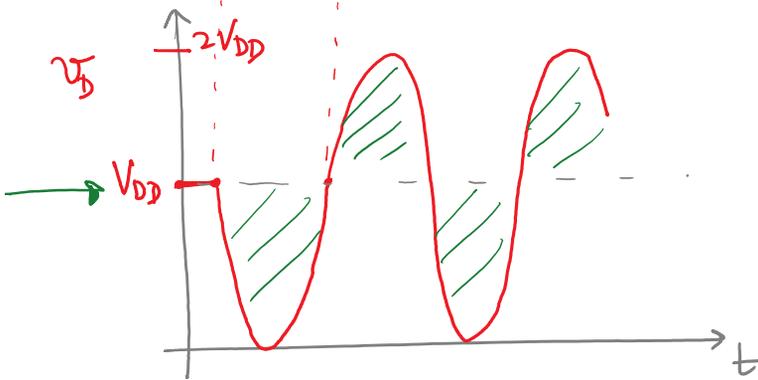
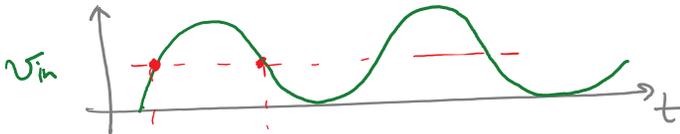


$$A_{v0} = -g_m R_L$$

$$f_0 = \frac{1}{2\pi \sqrt{L_1 C_1}}$$

$$Q = \omega_0 R_L C_1 = 2\pi f_0 R_L C_1$$

$$BW \Rightarrow \Delta f = \frac{f_0}{2Q}$$



Assume $V_{min} = V_{DS,at=0} = 0$

* For ideal inductor, the average (or DC) voltage drop = $\omega L = 0$
 \rightarrow average value of $V_D = V_{DD}$.

$\Rightarrow V_D$ must swing between 0 and $2V_{DD}$.

* This is only possible because an inductor, rather than a resistor, is connected between the drain & supply.

* at resonance $\omega = \omega_0 = \frac{1}{\sqrt{LC}}$

$$P_{out} = \frac{1}{T} \int_0^T \underbrace{V_{DD} \cos(\omega t)} \cdot \underbrace{\frac{V_{DD} \cos(\omega t)}{R_L}} \cdot dt$$

$$= \frac{V_{DD}^2}{2R_L T} \int_0^T [1 + \cos(2\omega t)] dt$$

$$= \frac{V_{DD}^2}{2R_L}$$

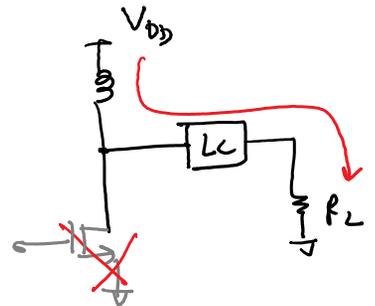
would have been $\frac{V_{DD}^2}{4R_L}$
for conventional analog amplifier (CS)

* Power pulled from the supply

$$P_{DC} = V_{DD} \cdot I_{DC} = V_{DD} \cdot \frac{V_{DD}}{R_L} = \frac{V_{DD}^2}{R_L}$$

$$\Rightarrow \eta = \frac{P_{out}}{P_{DC}} = \frac{1}{2} \Rightarrow 50\% \text{ efficiency}$$

Class-A drain efficiency



Classes of Tuned PAs

