

# ECE 513 - Lecture 12

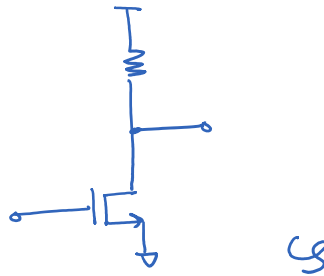
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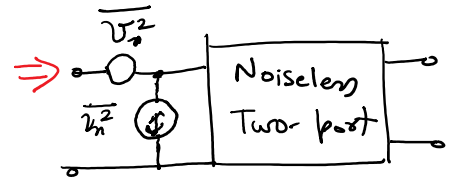
## Two-port Noise:

- \* Maximum power transfer ( $Z_{in} = Z_s^*$ )  $\Rightarrow$  power match
- \* Least Noise factor (Noise figure)  $\Rightarrow$  noise match

LNA



$$NF \simeq NF_{min}$$

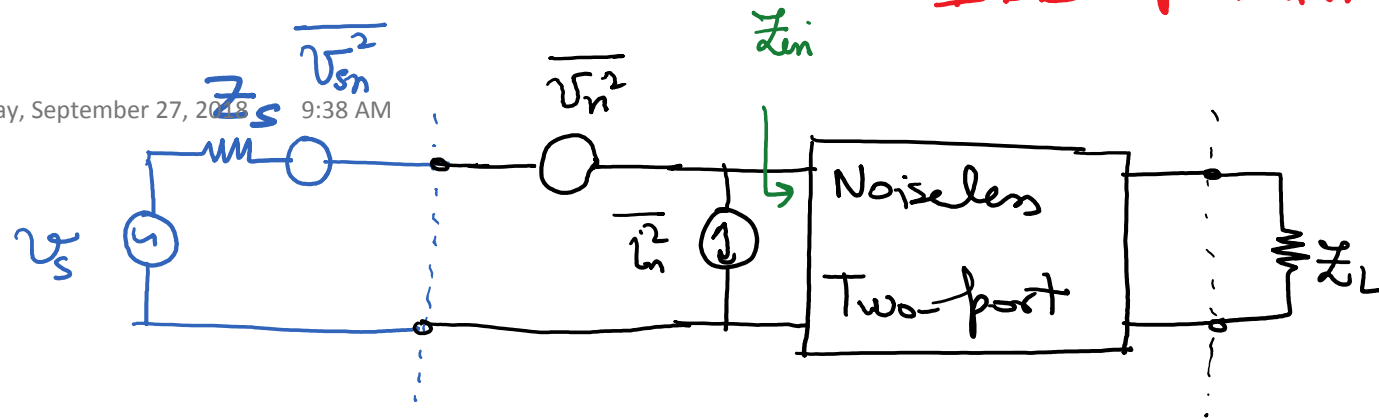


Linear Analysis

Two-port Noise Model

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IEEE representation of the noisy two-port



- \* Can represent a noisy two-port with two noise sources
  - ↳ a voltage source & a current source ( $v_n$  &  $i_n$ )
    - ↳ represent all internal noise sources
    - ↳ They are usually statistically correlated

Correlation coefficient

$$c = \frac{\langle i_n, v_n^* \rangle}{\sqrt{i_n^2 \cdot v_n^2}}$$

Correlation

$$\langle v_1, v_2^* \rangle$$

$$= \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T v_1(t) v_2^*(t) dt$$

$$= 0 \text{ iff } v_1 \& v_2 \text{ are uncorrelated}$$

\* There are 'four' real numbers that completely describe the noise of the linear two-port:

$$\underbrace{V_n}_{(1)}, \underbrace{i_n}_{(2)}$$

$$c = \underbrace{\text{Re}\{c\}}_{(3)} + j \underbrace{\text{Im}\{c\}}_{(4)}$$

'c' is a complex number.

\* Let's say that the two-port is driven by a signal source,  $V_s$ , with source impedance

$$Z_s = \underbrace{R_s}_{\text{generates noise}} + jX_s$$

$\Rightarrow \overline{V_{sn}^2} = 4kTR_s \cdot \Delta f$

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\* Initially assume  $c=0 \Rightarrow V_n$  &  $i_n$  are uncorrelated

↳ we'll fix this later

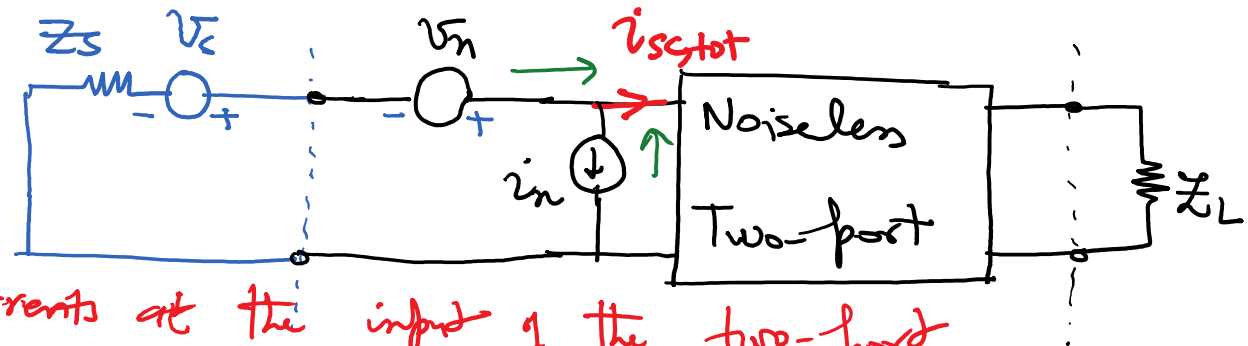
To find  $F$  for the arrangement;

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- ① find noise power in the load due to  $V_{sn}$  alone
- ② find noise power in the load due to both external ( $V_{sn}$ ) and internal ( $V_{n, in}$ ) noise sources.

\* We only need to calculate short-circuit noise current at the input of the noiseless two-port  
↳ the circuit that follows is noiseless.



Short circuit noise currents at the input of the two-port

$$i_{sc,tot} = \frac{-V_{sn} - V_n}{Z_s} - i_n$$

$$i_{sc,s} = \frac{-V_{sn}}{Z_s}$$

$$\overline{V_n^2} = \langle V_n, V_n^* \rangle$$

$$\overline{i_{sc,tot}^2} = \left\langle \frac{V_{sn} + V_n}{Z_s} + i_n, \frac{V_{sn}^* + V_n^*}{Z_s} + i_n \right\rangle$$

$$= \frac{\overline{V_{sn}^2} + \overline{V_n^2}}{|Z_s|^2} + \overline{i_n^2}$$

$$\overline{i_{sc,s}^2} = \frac{\overline{V_{sn}^2}}{|Z_s|^2}$$

we used

$$\langle V_n, i_n^* \rangle = 0$$

$$F = \frac{SNR_i}{SNR_o} = \frac{P_s/N_i}{P_s/N_o} = \frac{N_o}{N_i}$$

$$F = \frac{\overline{v_{sc,tot}^2}}{\overline{v_{sc,s}^2}} = 1 + \frac{\overline{v_n^2}}{\overline{v_{sn}^2}} + |Z_g|^2 \frac{\overline{v_n^2}}{\overline{v_n^2}}$$

$$\Rightarrow F = 1 + \frac{\overline{v_n^2}}{4kT R_s \Delta f} + \frac{(R_s^2 + X_s^2) \overline{v_n^2}}{4kT R_s \Delta f} \rightarrow \textcircled{1}$$

F depends upon  $v_n, i_n$  & the  $R_s, X_s$

\* Minimum Noise factor,  $F_{min}$

$$\frac{\partial F(R_s, X_s)}{\partial R_s} = 0 \quad \& \quad \frac{\partial F(R_s, X_s)}{\partial X_s} = 0.$$

$$F_{\min} = F(R_s = R_{s,\text{opt}}, X_s = X_{s,\text{opt}}) = 1 + \frac{\sqrt{\overline{v_n^2} \cdot \overline{i_n^2}}}{2kT\Delta f}$$

$$R_{s,\text{opt}} = \sqrt{\frac{\overline{v_n^2}}{\overline{i_n^2}}} \quad \text{and} \quad X_{s,\text{opt}} = 0 \quad \Rightarrow \quad Z_{s,\text{opt}} = R_{s,\text{opt}}$$

Noise  
impedance

$$F_{\min} = 1 + \frac{\sqrt{\overline{v_n^2} \cdot \overline{i_n^2}}}{2kT\Delta f}$$

\* If  $Z_s = R_{s,\text{opt}}$  then the maximum transfer of noise from the two-port to the input termination occurs without reflections.

↳ least amount of noise generated in the two-port is transferred to the load, resulting in the least degradation of SNR  $\Rightarrow$  best F.

In general  $v_n$  &  $i_n$  are correlated

Also  $Z_{s,\text{opt}} \neq Z_{in}^*$  of the two-port



\* Let's use  $C \neq 0$

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$V_n$  &  $i_n$  are partially correlated

$$\text{let } \begin{cases} V_n = V_n \\ i_n = i_u + i_c = i_u + \underbrace{Y_{cor} V_n}_{\text{Correlated}} \end{cases}$$

unrelated

$Y_{cor} \equiv$  correlation admittance

$$\Rightarrow Y_{cor} \triangleq \frac{\overline{i_n V_n^*}}{\overline{V_n^2}} = g_{cor} + jB_{cor}$$

$$Z = R + jX$$

$$Y = G + jB$$

$$1/R = G \Rightarrow \text{conductance}$$

$$1/X = B \Rightarrow \text{susceptance}$$

# Noise Admittance Formalism (IEEE parameters)

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$$\text{Finding } R_n \text{ and } Y_{s,opt} = G_{s,opt} + jB_{opt}$$

$$\text{Noise resistance } R_n \triangleq \frac{\overline{V_n^2}}{4kT\Delta f}$$

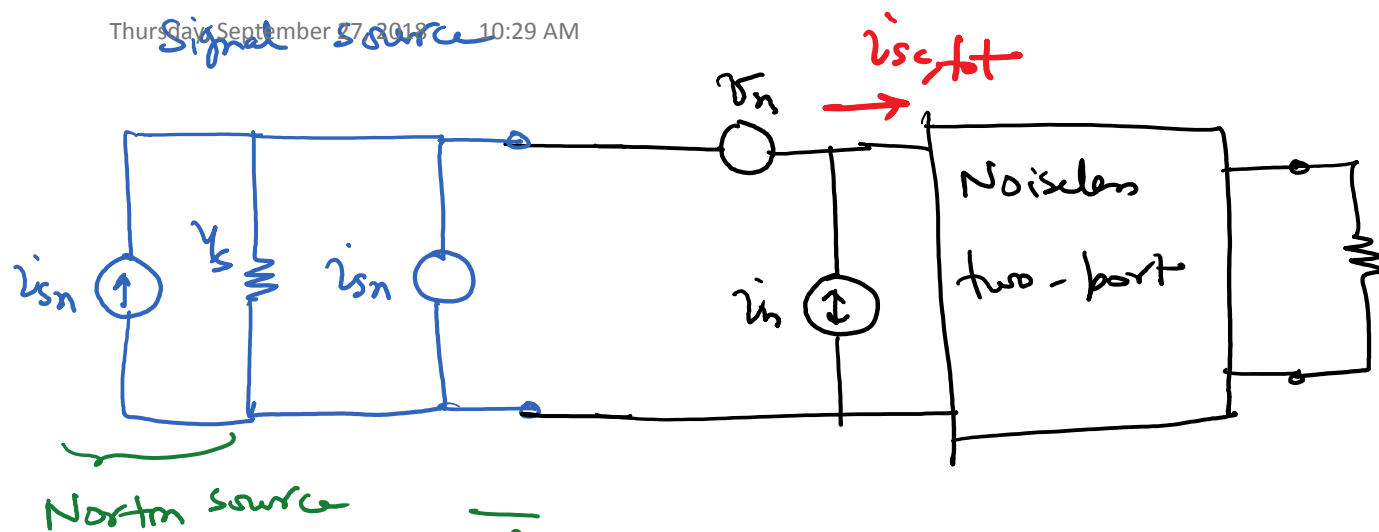
$$\text{Noise conductance } G_n \triangleq \frac{\overline{i_n^2}}{4kT\Delta f}$$

$$\begin{aligned} V_n \\ i_n &= i_u + i_c \\ &= i_u + Y_{cr} \cdot V_n \end{aligned}$$

The short circuit currents at the input of the noiseless two-port

$$\begin{aligned} i_{sc,tot} &= i_{sn} + i_n + Y_s V_n \\ &= i_{sn} + i_u + (Y_{cr} + Y_s) V_n \longrightarrow \textcircled{3} \end{aligned}$$

$$i_{sg,s} = i_{sn} \longrightarrow \textcircled{4}$$



$$\overline{i_{sn}^2} = 4kT \Delta f g_s$$

$$F = \frac{\overline{i_{sc,tot}^2}}{\overline{i_{sc,s}^2}} = 1 + \frac{\overline{i_v^2}}{\overline{i_{sn}^2}} + \frac{\overline{v_n^2} |Y_{in} + Y_s|^2}{\overline{i_{sn}^2}} \quad \swarrow \text{from } \textcircled{3} \text{ \& } \textcircled{4}$$

$$= 1 + \frac{\cancel{4kT g_n \Delta f}}{\cancel{4kT g_s \Delta f}} + \frac{\cancel{4kT R_n \Delta f} |Y_{in} + Y_s|^2}{\cancel{4kT g_s \Delta f}}$$

$$F = 1 + \frac{R_n}{g_s} |Y_{in} + Y_s|^2 + \frac{g_n}{g_s}$$

$$Y_{cor} = G_{cor} + j B_{cor}$$

$$Y_s = G_s + j B_s$$

$$F = 1 + \frac{R_n}{G_s} |Y_{cor} + Y_s|^2 + \frac{G_{pu}}{G_s}$$

$$= 1 + \frac{R_n}{G_s} [(G_{cor} + G_s)^2 + (B_{cor} + B_s)^2] + \frac{G_{pu}}{G_s}$$

$$\frac{\partial F}{\partial G_s} = \frac{-R_n}{G_s^2} [(G_{cor} + G_s)^2 + (B_{cor} + B_s)^2] + \frac{2R_n}{G_s} (G_{cor} + G_s) - \frac{G_{pu}}{G_s^2} = 0$$

$$\Rightarrow G_s^2 - G_{cor}^2 - (B_{cor} + B_s)^2 = \frac{G_{pu}}{R_n}$$

$$\Rightarrow G_s^2 = G_{cor}^2 + (B_{cor} + B_s)^2 + \frac{G_{pu}}{R_n} \longrightarrow (5)$$

$$\frac{\partial F}{\partial B_s} = \frac{2R_n}{g_s} (B_{cr} + B_s) \Rightarrow$$

$$\Rightarrow B_{cr} + B_s \Rightarrow$$

$$\Rightarrow B_{s,opt} = -B_{cr} \longrightarrow \textcircled{6}$$

On combining  $\textcircled{5}$  &  $\textcircled{6}$ , we get

$$g_{s,opt} = \sqrt{g_{cr}^2 + \frac{g_u}{R_n}}$$

$$\& B_{s,opt} = -B_{cr}$$

$$F_{min} = 1 + \frac{R_n}{g_{s,opt}} (g_{cor} + g_{s,opt})^2 + \frac{g_{cor}}{g_{s,opt}}$$

$$= 1 + \frac{1}{g_{s,opt}} \left[ R_n (g_{cor} + g_{s,opt})^2 + (g_{s,opt}^2 - g_{cor}^2) R_n \right]$$

$$= 1 + \frac{R_n}{g_{s,opt}} \left[ \cancel{g_{cor}^2} + \overset{2}{g_{s,opt}^2} + 2\cancel{g_{cor}}\cancel{g_{s,opt}} + \overset{2}{g_{s,opt}^2} - \cancel{g_{cor}^2} \right]$$

$$F_{min} = 1 + 2R_n (g_{cor} + g_{s,opt})$$

$$F = F_{min} + \frac{R_n}{g_s} |y_s - y_{s,opt}|^2$$

\*  $R_n$  is an indicator of the sensitivity of the NF to noise impedance mismatch

A large  $R_n \Rightarrow$  NF will be very sensitive to variations in the value of  $Y_s$  (or  $Z_s$ )  
 $\Rightarrow$  more sensitive to process variations