

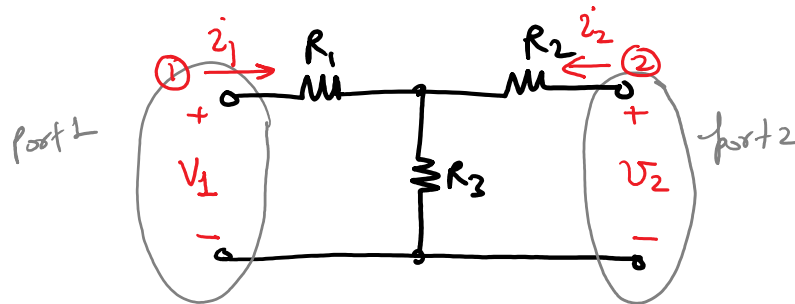
ECE 513 - Lecture 11

Tuesday, September 25, 2018 9:28 AM

Chapter 3: Two ports:

Linear Network Analysis

↳ small signal parameters.



$i \Rightarrow$ independent
 $V \Rightarrow$ dependent variables

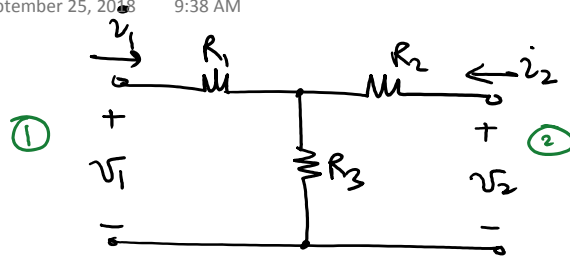
$$V_1 = i_1 Z_{11} + i_2 Z_{12}$$

$$V_2 = i_1 Z_{21} + i_2 Z_{22}$$

$$\begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$$

$$V = Z i$$

two-port Z -parameters \Rightarrow can be complex

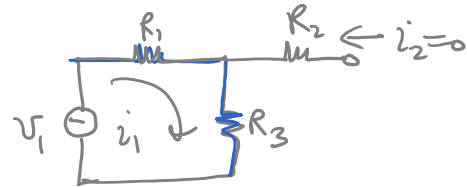


$$v_1 = Z_{11} i_1 + Z_{12} i_2$$

$$v_2 = Z_{21} i_1 + Z_{22} i_2$$

$Z_{11} = \frac{v_1}{i_1} \Big|_{i_2=0} \Rightarrow \text{Port 2 is open circuit}$

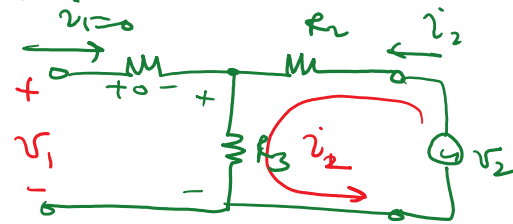
$$= R_1 + R_3$$



$Z_{12} = \frac{v_1}{i_2} \Big|_{i_1=0}$

$$= R_3$$

Port 1 is open circuit



$$v_1 = R_3 \cdot i_2$$

$Z_{21} = \frac{v_2}{i_1} \Big|_{i_2=0} = R_3$

$Z_{22} = \frac{v_2}{i_2} \Big|_{i_1=0} = R_2 + R_3$

$$\mathbf{Z} = \begin{bmatrix} R_1 + R_3 & R_3 \\ R_3 & R_2 + R_3 \end{bmatrix}$$

Y-parameters:

$$i_1 = y_{11} v_1 + y_{12} v_2$$

$$i_2 = y_{21} v_1 + y_{22} v_2$$

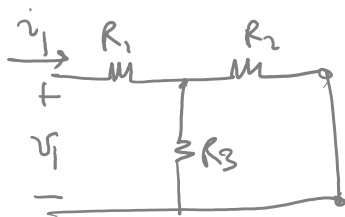
(admittance parameters)

$$Y = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix}$$

$$Y = Z^{-1}$$

$$y_{11} = \left. \frac{i_1}{v_1} \right|_{v_2=0}$$

port 2 is short circuit



$$v_1 = (R_1 + R_2 \parallel R_3) i_1$$

$$y_{11} = \frac{i_1}{v_1} = \frac{1}{R_1 + R_2 \parallel R_3}$$

$$y_{12} = \frac{-R_3}{(R_2 + R_1 \parallel R_3)(R_1 + R_3)}$$

$$y_{21} = \frac{-R_3}{(R_1 + R_2 \parallel R_3)(R_2 + R_3)}$$

$$y_{22} = \frac{1}{R_2 + R_1 \parallel R_3}$$

$$y_{12} = \left. \frac{i_1}{v_1} \right|_{v_2=0}$$

$$y_{21} = \left. \frac{i_2}{v_1} \right|_{v_2=0}$$

$$y_{22} = \left. \frac{i_2}{v_2} \right|_{v_1=0}$$

We can verify that

$$Y = Z^{-1}$$

$$\begin{bmatrix} a & b \\ c & d \end{bmatrix}^{-1} = \frac{1}{ad-bc} \begin{bmatrix} d & -b \\ -c & a \end{bmatrix}$$

h-parameters .

$$\begin{bmatrix} v_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \begin{bmatrix} i_1 \\ v_2 \end{bmatrix}$$

↳ useful for analyzing circuits with series-shunt feedback

↳ for extraction of R_g of MOSFETs

g-params :

$$\begin{bmatrix} i_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} g_{11} & g_{12} \\ g_{21} & g_{22} \end{bmatrix} \begin{bmatrix} v_1 \\ i_2 \end{bmatrix}$$

↳ useful in shunt-series feedback

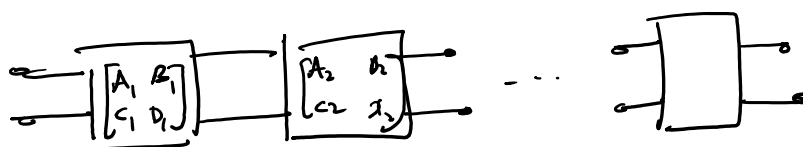
H & g matrices are only defined for 2-ports
but Z & Y can be extended to N-ports.

ABCD Matrices:

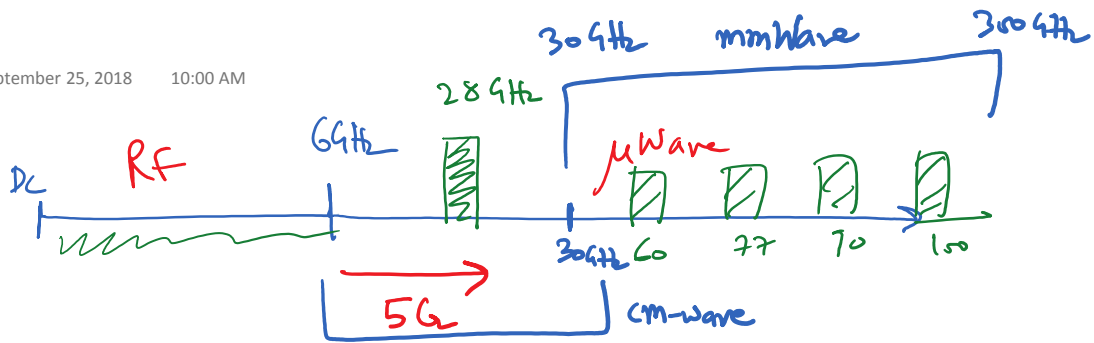
Useful for cascaded two-port analysis

$$\begin{bmatrix} V_1 \\ i_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ -i_2 \end{bmatrix}$$

$$A = \left. \frac{V_1}{V_2} \right|_{i_2=0}, \quad B = \left. \frac{-V_1}{I_2} \right|_{V_2=0}, \quad C = \left. \frac{I_1}{V_2} \right|_{I_2=0}, \quad D = \left. \frac{-I_1}{I_2} \right|_{V_2=0}$$



$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \prod_{i=1}^n \begin{bmatrix} A_i & B_i \\ C_i & D_i \end{bmatrix}$$



* $\lambda \geq \frac{\lambda}{20}$ transmission line effects show up in Integrated Circuits
 ↓
 length or size of interconnects (wires)

@ 3 GHz

$$\lambda = \frac{3 \times 10^8}{3 \times 10^9} = 0.1 \text{ m} = 10 \text{ cm}$$

@ 30 GHz

$$\lambda = 1 \text{ cm}$$

$$\frac{\lambda}{20} = 0.05 \text{ cm} = 0.5 \text{ mm}$$

* at "high-frequency" need to account for possible impedance mismatches between signal sources, load, and interconnect impedances.

Reflection Coefficient.

Z_0 = characteristic impedance of the TL \Rightarrow 50 Ω

$$\Gamma = \frac{Z - Z_0}{Z + Z_0}$$

$$= \frac{Y_0 - Y}{Y + Y_0}$$

normalized form

$$\Gamma = \frac{z - 1}{z + 1} \quad \text{where } z = \frac{Z}{Z_0}$$

$\Gamma \Rightarrow$ can be complex \Rightarrow typically use Smith Charts to visualize and manipulate these impedances.

$$V_{SWR} = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$

Voltage standing
wave ratio

S-parameters :

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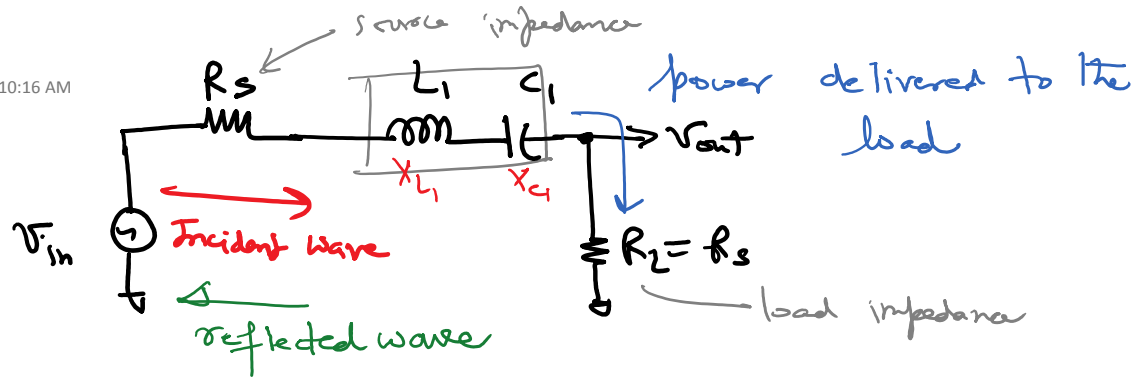
* measurement of high frequency voltages & currents is difficult experimentally

↳ opening & shorting of ports is not feasible

* transfer of power from one stage to next. instead of voltage or current.

↳ scattering parameters or "S-parameters"

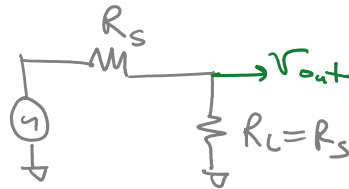
Example:



$$X_{L_1} + X_{C_1} = j\omega L_1 + \frac{1}{j\omega C_1} = j\omega L_1 - \frac{j}{\omega C_1}$$

$$@ \omega = \frac{1}{\sqrt{L_1 C_1}} = \omega_0 \quad \text{resonance occurs}$$

$$\Gamma = \frac{R_s - R_L}{R_s + R_L} = 0$$

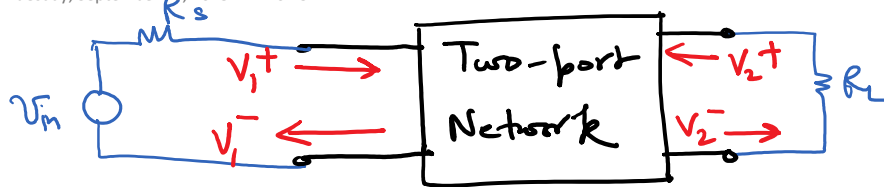


For maximum power transfer

$$Z_L = Z_s^*$$

"Conjugate Match"

* We say that the input port of the circuit generates a "reflected wave" that returns to the source



* incident and reflected waves at the input port are V_1^+ & V_1^-
 Similarly, waves at the output are V_2^+ & V_2^-

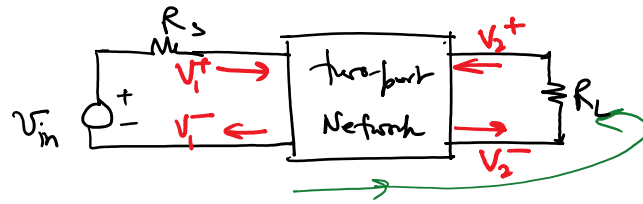
$$\begin{array}{lcl} \text{Net voltage at the input} & = & V_1^+ + V_1^- \\ \text{" " " " output} & = & V_2^+ + V_2^- \end{array}$$

$$\begin{aligned} V_1^- &= S_{11} V_1^+ + S_{12} V_2^+ \\ V_2^- &= S_{21} V_1^+ + S_{22} V_2^+ \end{aligned}$$

$$\begin{bmatrix} V_1^- \\ V_2^- \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix} \begin{bmatrix} V_1^+ \\ V_2^+ \end{bmatrix}$$

$\hookrightarrow [S]$

①
$$S_{11} = \left. \frac{V_1^-}{V_1^+} \right|_{V_2^+ = 0}$$



Ratio of reflected and incident waves at the input port when the reflection from R_L (i.e. V_2^+) is zero.

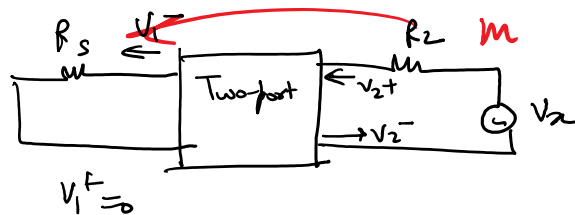
↳ represents the accuracy of input matching

② S_{12} :

$$S_{12} = \left. \frac{V_1^-}{V_2^+} \right|_{V_1^+ = 0}$$

* S_{12} is the ratio of reflected wave at the input port to the incident wave into the output port when the input port is matched

↳ characterizes the reverse isolation



③ S_{21} :

$$S_{21} = \left. \frac{V_2^-}{V_1^+} \right|_{V_2^+ = 0}$$

S_{21} is the ratio of the wave incident on the load to that going to the input, when the reflection from R_L is zero.

↳ Represents the gain of the circuit

$$S_{21} \Rightarrow \text{gain}$$

④ $S_{22} = \left. \frac{V_2^-}{V_2^+} \right|_{V_1^+ = 0} \Rightarrow$ ratio of reflected and incident waves at the output when the reflection from R_S is zero ($V_1^+ = 0$)

↳ Represents the accuracy of the output "matching"

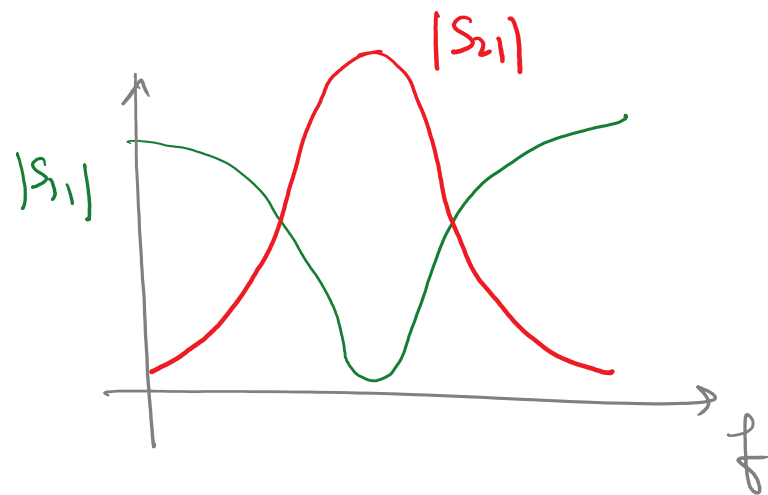
* S-params typically have frequency dependent complex values and often expressed in dB.

$$S_{mn} \Big|_{\text{dB}} = 20 \log |S_{mn}|$$

Input reflection



reverse isolation



Normalized incident wave	$a_n = \frac{V_n^+}{\sqrt{Z_0}}$	} formalism used in the book
" reflected wave	$b_n = \frac{V_n^-}{\sqrt{Z_0}}$	

avg. power for incident wave, $P_{avg,i} = \frac{V_n^+ \times I_n^{+*}}{2} = \frac{|a_i|^2}{2}$

" " reflected wave, $P_{avg,r} = \frac{V_n^- \times I_n^{-*}}{2} = \frac{|b_i|^2}{2}$

power going to load $\left(\frac{|a_i|^2 - |b_i|^2}{2} \right)$