

EC6 So 4 - Lecture 20

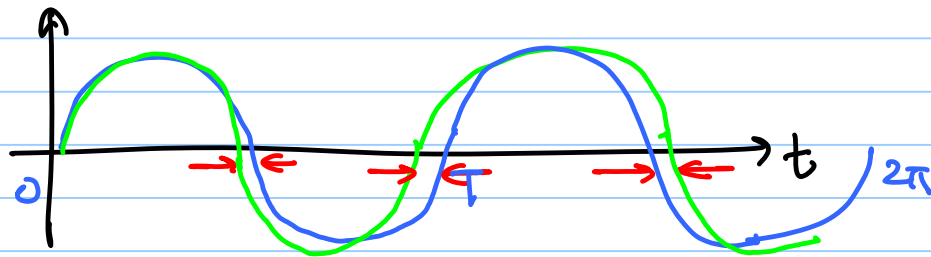
Note Title

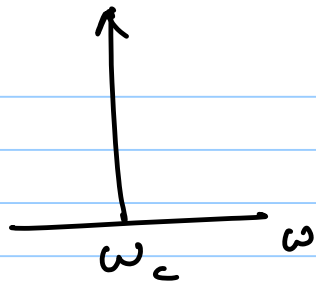
11/1/2016

Oscillator Phase Noise :

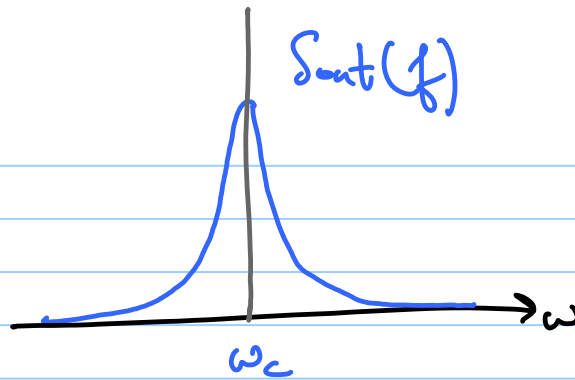
$$V_{out}(t) = A \cos(\omega_c t + \phi_n(t))$$

↳ $\phi_n(t)$ is a random phase quantity that deviates the zero crossing from the multiple of clock period.

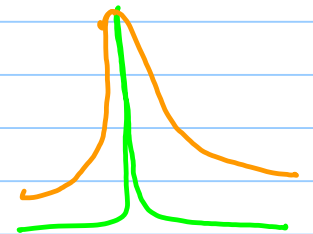
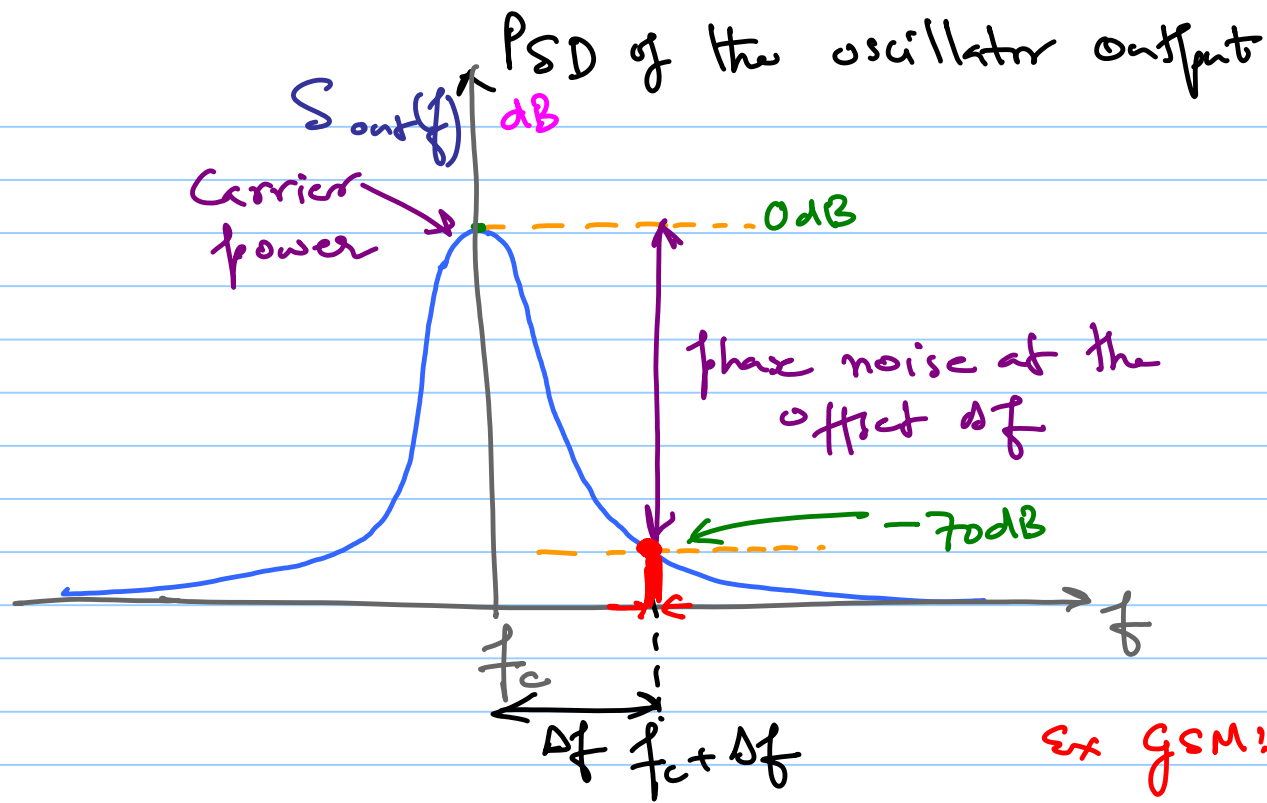




Ideal oscillator



Oscillator with $\wedge$ phase noise



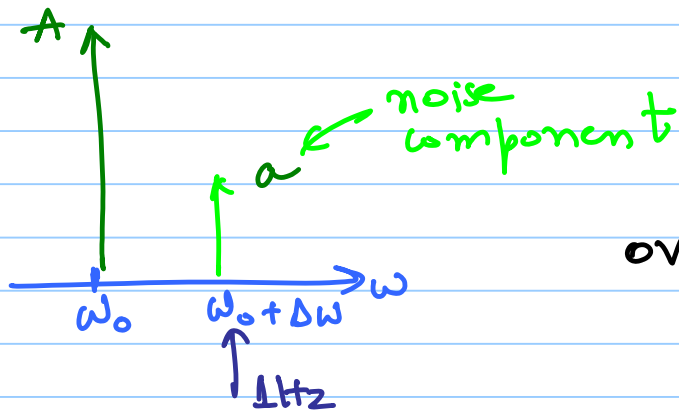
Example
phase noise is
-70 dBc/Hz at an
offset $\Delta f = 1 \text{ kHz}$

ex GSM:

< -115 dBc/Hz at
600 kHz offset

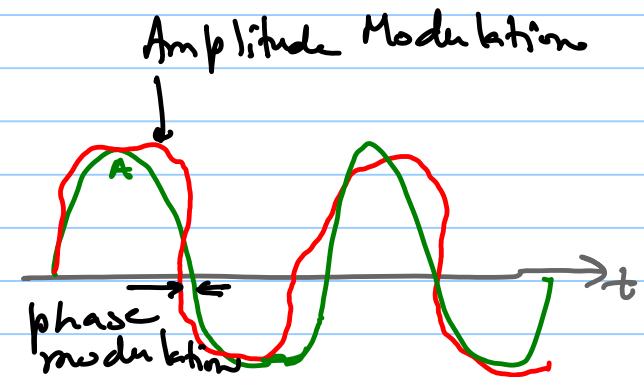
Phase Noise Overview

$$a \ll A$$

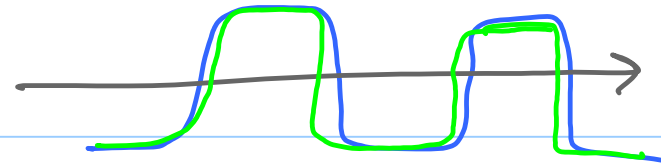


overall waveform

$$x(t) = A \cos \omega_0 t + \underbrace{a \cos((\omega_0 + \Delta\omega)t)}_{\text{noise component}}$$



↳ Both AM & PM



↳ The composite waveform is applied to a hard limiter

↳ clips the magnitude and removes AM

↳ only phase modulation remains

After hard limiting, it can be shown that

$$\begin{aligned} x_{\text{lim}}(t) &= \frac{A}{2} \cos \omega_0 t - \frac{a}{2} \cos((\omega_0 + \Delta\omega)t) + \frac{a}{2} \cos((\omega_0 - \Delta\omega)t) \\ &\approx \frac{A}{2} \cos\left(\omega_0 t - \underbrace{\frac{2a}{A} \sin(\Delta\omega t)}_{\text{PM component}}\right) \end{aligned}$$

↳ Narrowband random noise in the vicinity of ω_0 results in a phase whose spectrum has the same shape as that of the noise, but translated by ω_0 and normalized by $\frac{A}{2}$

$$x(t) \approx \frac{A}{2} \cos \left(\omega_0 t - \left(\frac{2}{A} \right) a \sin(\Delta \omega t) \right)$$

$\Delta \omega$ effect

$a \cdot \cos(\underbrace{(\omega_0 + \Delta \omega)t})$

In general,

$$x(t) = A \cos \omega_0 t + n(t)$$

narrowband noise
↓

$$\hookrightarrow n(t) = n_I(t) \cos \omega_0 t - n_Q(t) \sin \omega_0 t$$

n_I & n_Q have the same spectrum

↳ quadrature components

$$x(t) = (A + n_I(t)) \cos \omega_0 t - n_Q(t) \sin \omega_0 t$$

$$= \sqrt{(A + n_I(t))^2 + n_Q^2(t)} \cdot \cos \left[\omega_0 t + \underbrace{\tan^{-1} \frac{n_Q(t)}{A + n_I(t)}}_{\phi_n(t)} \right]$$

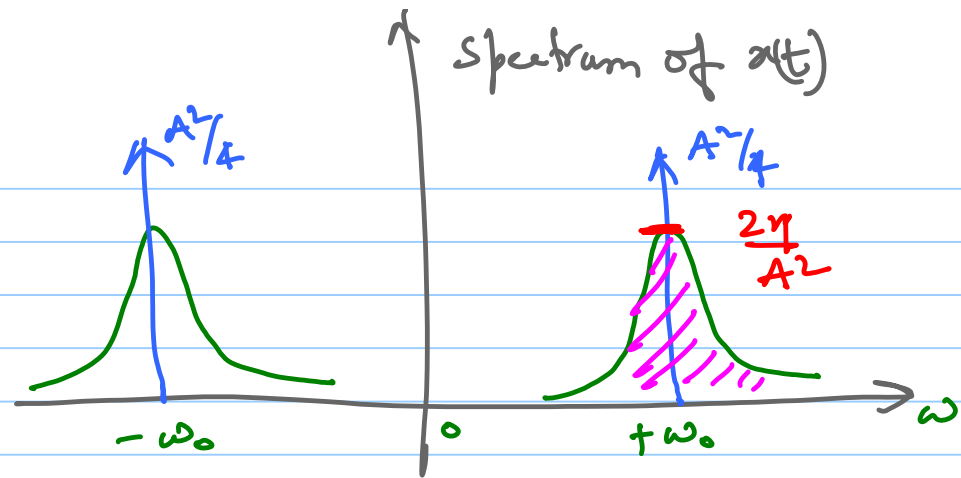
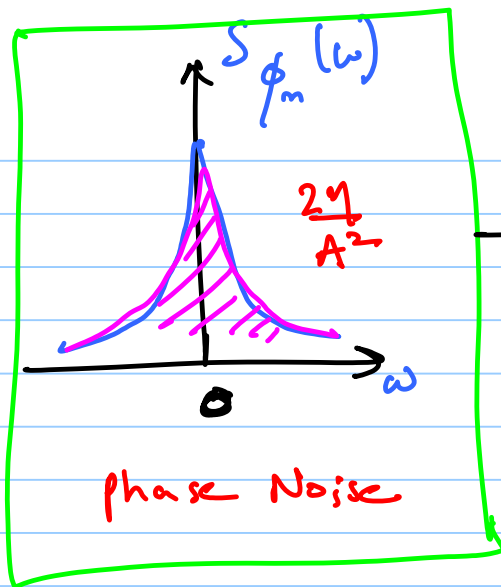
Since, $n_I(t), n_Q(t) \ll A$

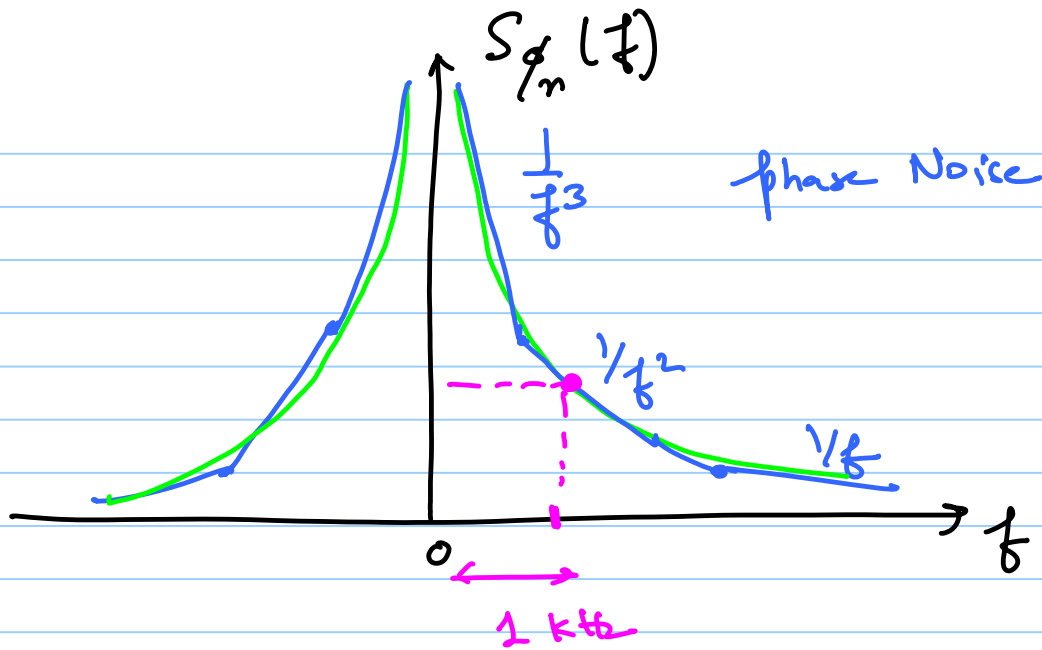
$$\phi_n(t) \approx \frac{n_Q(t)}{A}$$

Power spectral density

$$S_{\phi_n}(\omega) = \frac{S_{n_Q}(\omega)}{A^2}$$

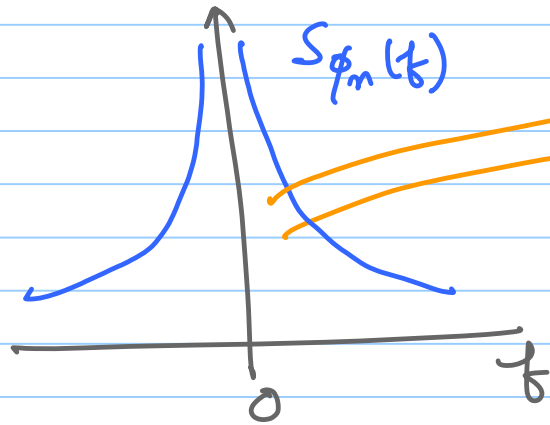
relate the phase noise, $\phi_n(t)$ to oscillator's noise component, $n_Q(t)$



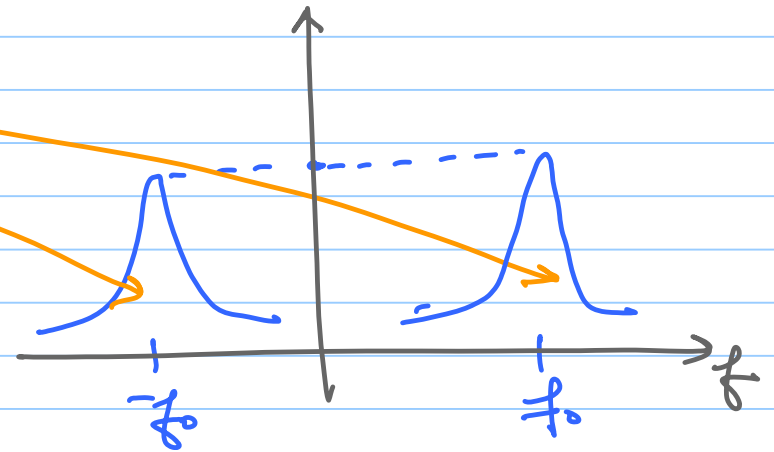


$\phi_n(t) \rightarrow$ phase
 domain
 signal

Phase domain ($\phi_n(t)$)



Voltage domain ($x(t)$)



Noise in PLLs

Noise Sources

Deterministic

Supply noise

Coupling

Substrate Noise

Random

→ Thermal Noise

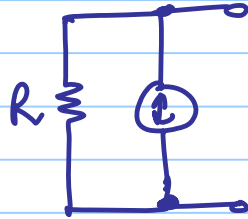
→ Flicker Noise

↳ Reference feedthrough

Thermal Noise

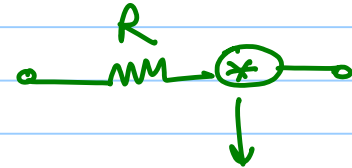


$\Rightarrow$



$$\overline{I_n^2} = \frac{4kT}{R}$$

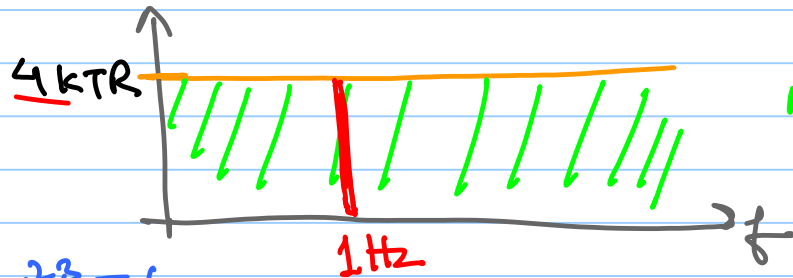
$\triangleq$



$$\overline{V_n^2} = 4kTR$$

mean square value
 $\hookrightarrow$ power in 1Hz BW

$S_v(f)$



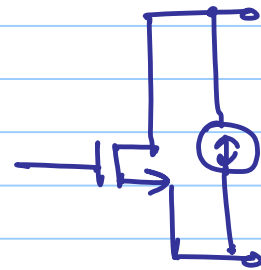
Noise PSD

$$\overline{V_n^2} = 4kTR$$



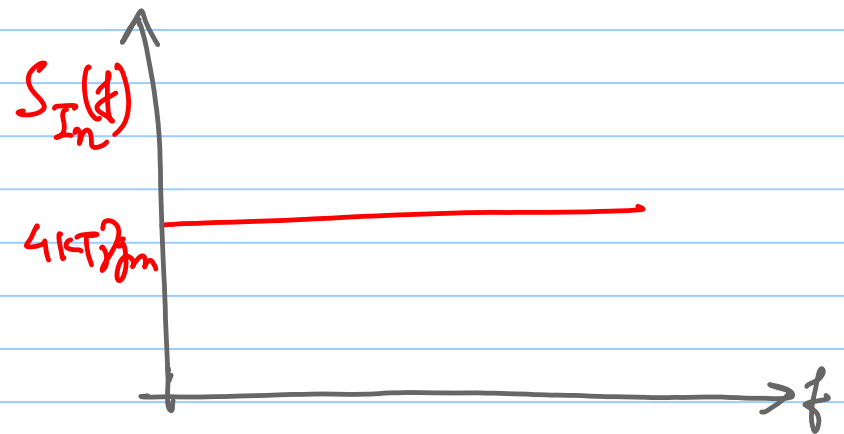
Boltzmann's constant
 $k = 1.38 \times 10^{-23} \text{ J/K}$

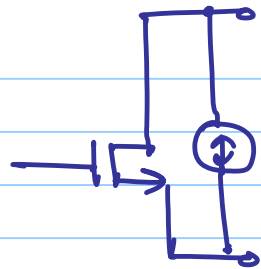
Transistor in Saturation



$$\overline{I_n^2} = 4kT\gamma g_m$$

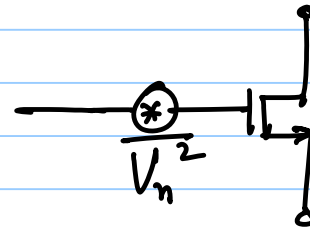
$\gamma = \frac{2}{3}$ for long channel
 $L \geq 10\mu m$





$$\overline{I_n^2} = 4kT\gamma g_m$$

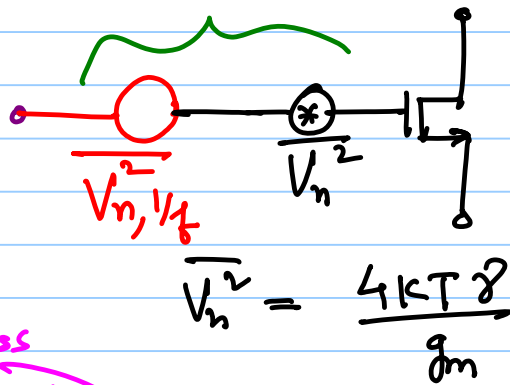
$\equiv$



$$\overline{V_n^2} = \frac{4kT\gamma}{g_m}$$

Flicker Noise

Total Noise

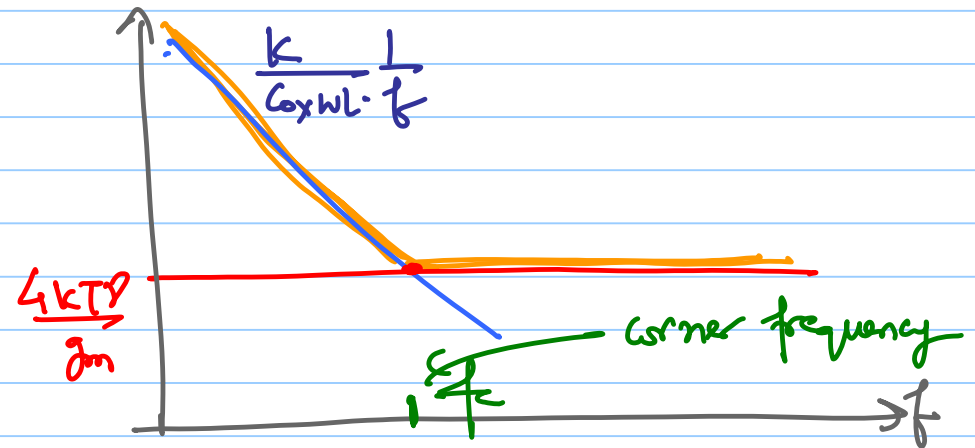


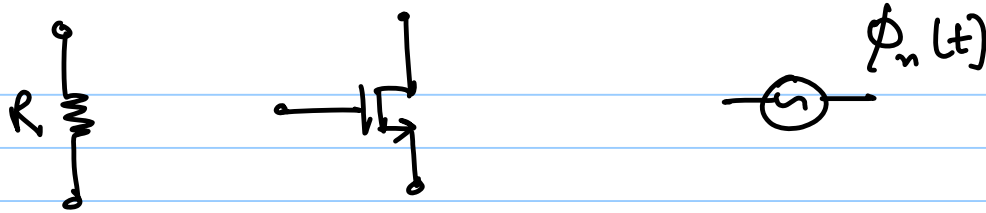
process constant

$$S_{n, 1/f} = \frac{K}{C_{ox}WL} \cdot \frac{1}{f}$$

$\overline{V_n^2} \propto \frac{1}{f}$ → frequency dependent noise

$$S_{n, 1/f} \propto \frac{1}{f}$$





Generic Noise Analysis:

* Small signal analysis with several noise sources

Procedure:

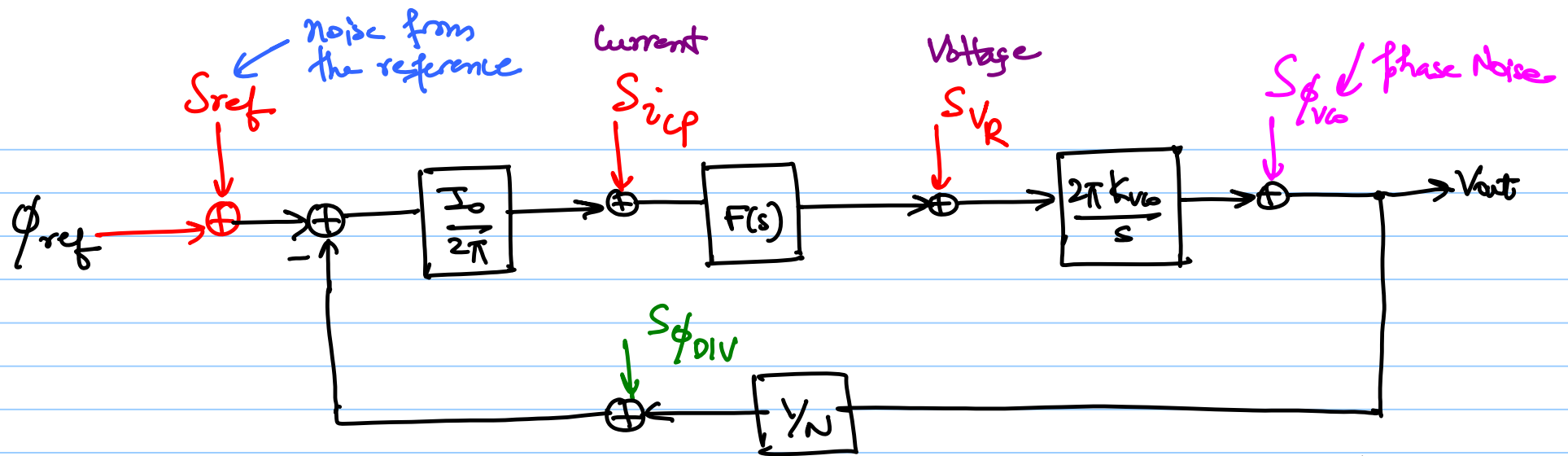
- ① Identify all noise sources
- ② Calculate (estimate from simulations) PSD of each noise source $S_i(f)$

③ Evaluate transfer function from each of noise sources to the output, $H_i(f)$

↳ output noise contribution $|H_i(f)|^2 S_i(f)$

⑤ Sum all the contributions to obtain total output noise

$$= \sum_i |H_i(f)|^2 S_i(f)$$



$S_{\phi ref}$: Reference clock noise PSD

S_{icp} : PFD/cp noise PSD

S_{VR} : Loop filter resistor noise PSD

PSD $\Rightarrow$ power spectral density

$S_{\phi_{vco}}$: Vco phase Noise PSD

$S_{\phi_{div}}$: Divider Noise PSD

Noise Transfer Functions: ($H_i(f)$)

$$\text{Loop gain} \Rightarrow L(s) = \frac{I_o}{2\pi} F(s) \cdot \frac{2\pi K_{vco}}{s \cdot N} = \frac{I_o K_{vco}}{N} \cdot \frac{F(s)}{s}$$

$$NTF_{ref}(s) = \frac{\phi_{out}}{\phi_{ref}}(s) = \frac{N \cdot L(s)}{1 + L(s)} \quad \text{LPF}$$

