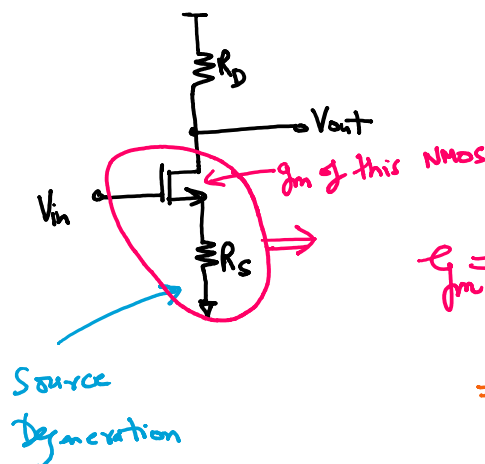
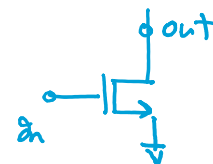


FCE 310- Lecture 24

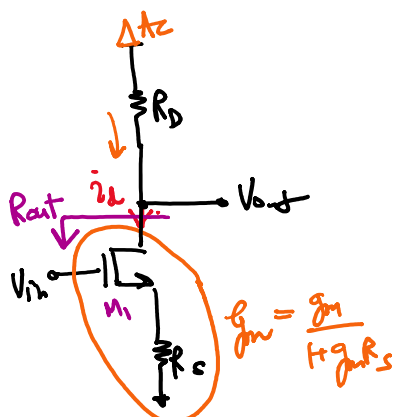
Wednesday, March 21, 2018 10:30 AM

Common source with Source-Degeneration:



$$g_m = \frac{g_m}{1 + g_m R_S}$$

$$= \frac{g_m \text{ of NMOS}}{1 + g_m \times R_S} \rightarrow \text{more linear input-output behavior}$$

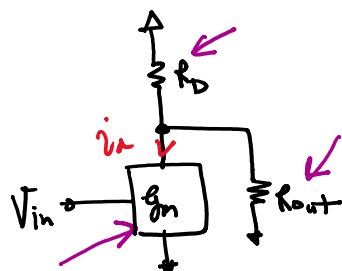


$$i_d = g_m v_{in}$$

$$v_{out} = -i_d (R_D \parallel R_{out})$$

$$\approx -i_d R_D$$

$$= -\frac{g_m}{1 + g_m R_S} \cdot R_D \cdot v_{in}$$



assume $r_{o1} \rightarrow \infty$
 $\rightarrow R_{out} \rightarrow \infty$

$$\Rightarrow A_v = \frac{v_{out}}{v_{in}} = -\frac{g_m R_D}{1 + g_m R_S}$$

$$= -\frac{R_D}{\frac{1}{g_m} + R_S}$$

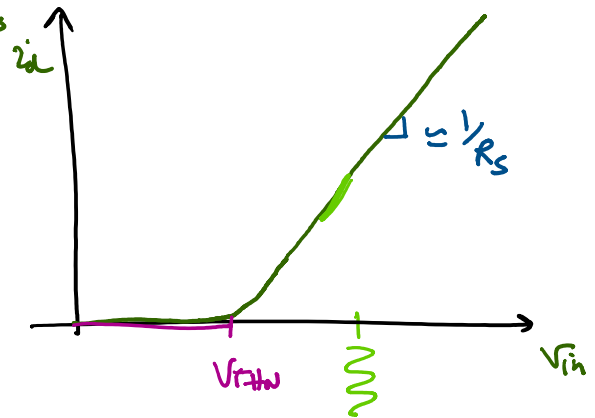
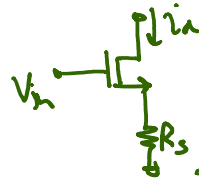
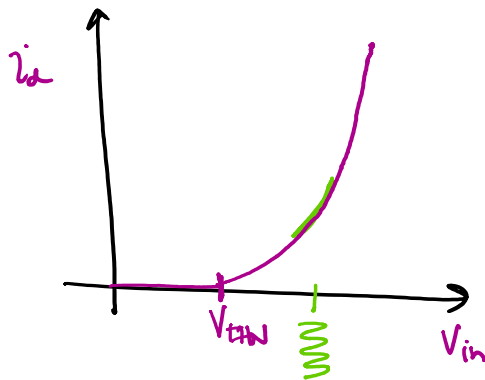
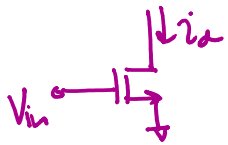
If $\frac{1}{g_m} \ll R_S$
 $\Rightarrow g_m R_S \gg 1$

$$= -\frac{R_D}{R_S}$$

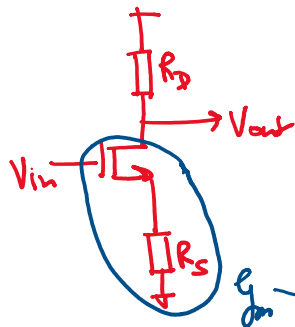
for large $g_m R_S \gg 1$

$$\Rightarrow \underline{A_v} \approx -\frac{R_D}{R_S} \Rightarrow \text{independent of } g_m$$

↑
gain is insensitive to NMOSFET variations.



"Linearized CS Amplifier"



$$\Rightarrow \underline{A_v} \approx -\left(\frac{g_m}{1 + g_m R_S}\right) \times R_D$$

$g_m \rightarrow g_m$

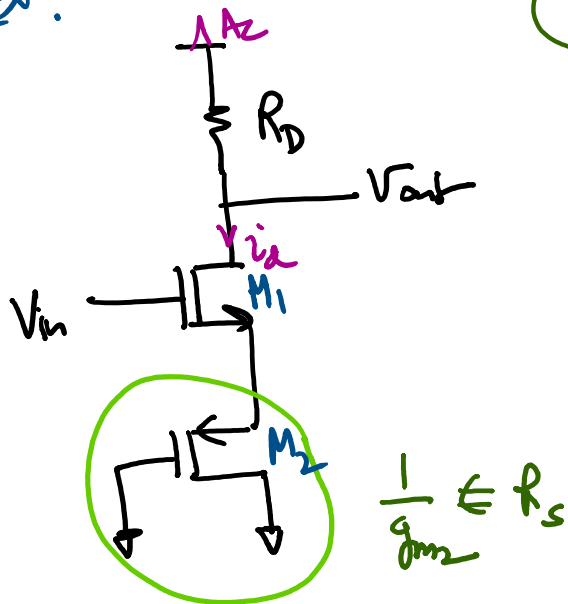
gain is reduced by a factor of

$$(1 + g_m R_S)$$

↳ Trading gain with linearity.

Ex.

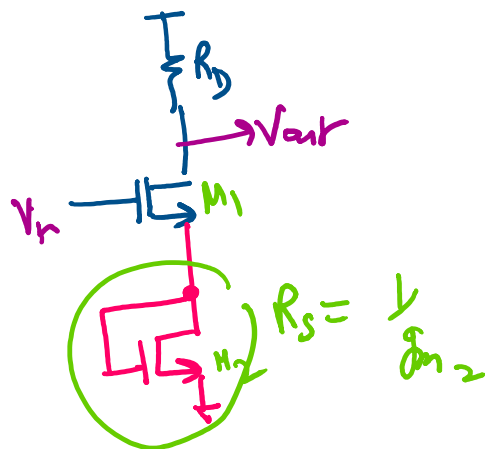
Assume
 $\lambda = 0 \Rightarrow r_{o1} \Rightarrow \infty$



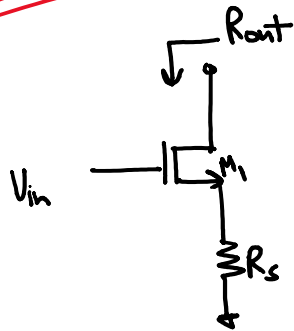
$$A_{v2} = -g_{m1} \cdot R_D$$

$$= - \frac{g_{m1}}{1 + g_{m1} \cdot \frac{1}{g_{m2}}} \cdot R_D$$

$$= - \frac{R_D}{\frac{1}{g_{m1}} + \frac{1}{g_{m2}}}$$



Important

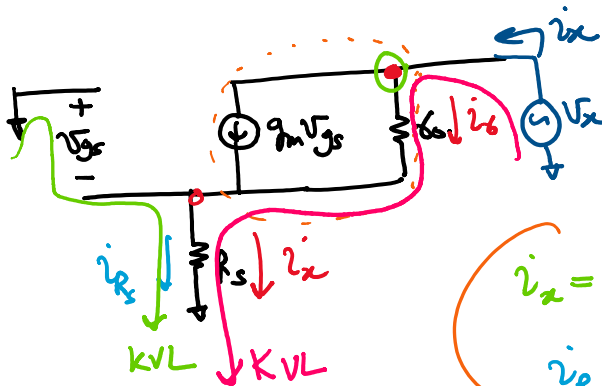


$\neq f_0$

$$R_{out} = \frac{V_x}{i_x}$$

replace by small-signal model

\Rightarrow



$$i_x = i_{ro} + g_m V_{gs}$$

$$i_{R_s} = g_m V_{gs} + i_{ro} = i_x$$

KVL:

$$V_{gs} + i_x R_s = 0$$

$$\Rightarrow V_{gs} = -i_x R_s \rightarrow \textcircled{1}$$

KVL:

$$V_x = (\overbrace{i_x - g_m V_{gs}}^{i_{ro}}) r_o - V_{gs} \rightarrow \textcircled{2}$$

Combine $\textcircled{1}$ & $\textcircled{2}$

$$\begin{aligned} V_x &= [i_x - g_m(-i_x R_s)] r_o - (-i_x R_s) \\ &= i_x r_o + (g_m R_s r_o) i_x + i_x R_s \\ &= i_x [r_o (1 + g_m R_s) + R_s] \end{aligned}$$

$$= v_x \cdot (g_m + g_{m2})$$

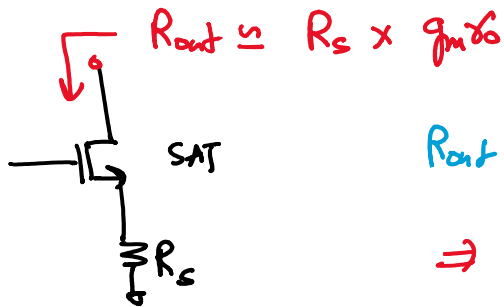
$$= i_x [g_m r_o + R_s + r_o]$$

→

$$R_{out} = \frac{v_x}{i_x} = (1 + g_m R_s) r_o + R_s = \boxed{(g_m r_o) R_s + R_s + r_o}$$

if $g_m R_s \gg 1$

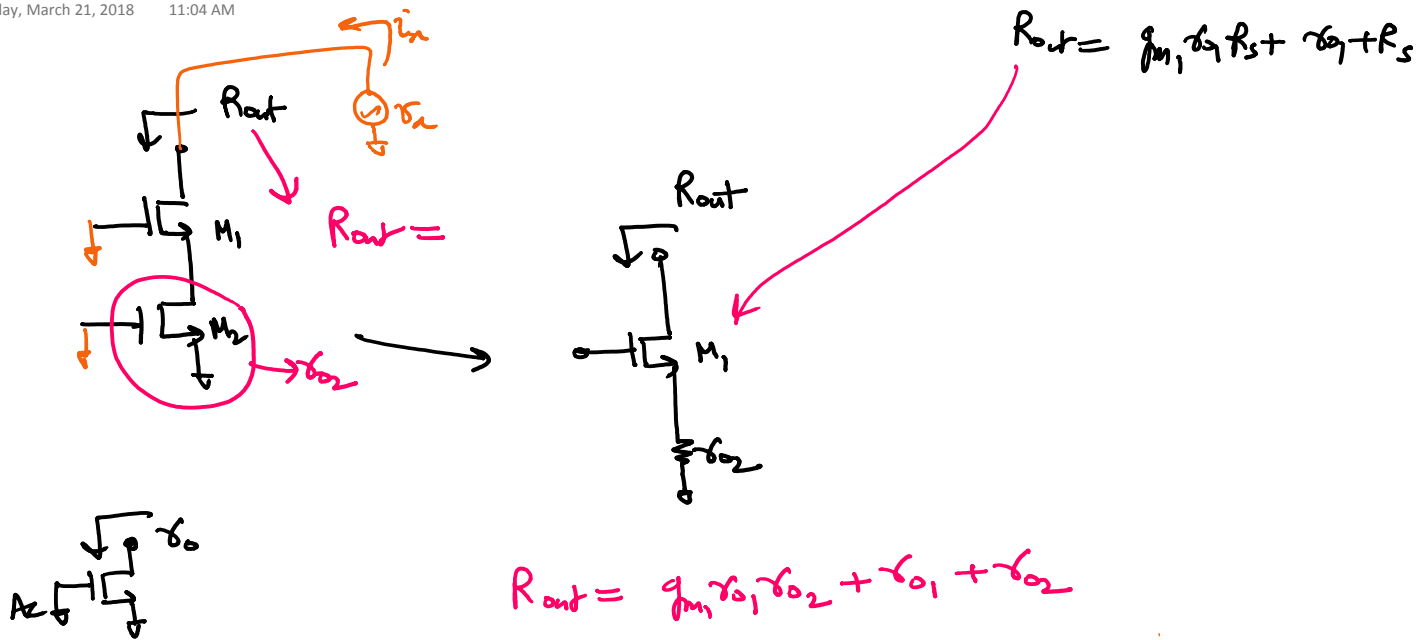
$$\approx (g_m r_o) R_s$$



R_{out} is raised from r_o to $(g_m r_o) R_s$

⇒ Method to obtain higher output resistance

⇒ "CASCODING"

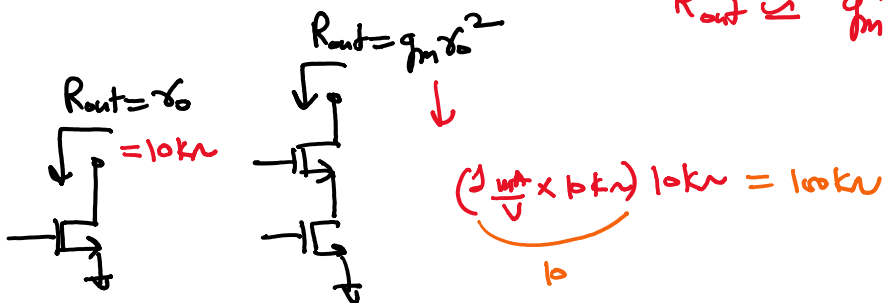


$$R_{out} = g_{m1} r_{o1} r_{o2} + r_{o1} + r_{o2}$$

Let M_1 & M_2 are identical

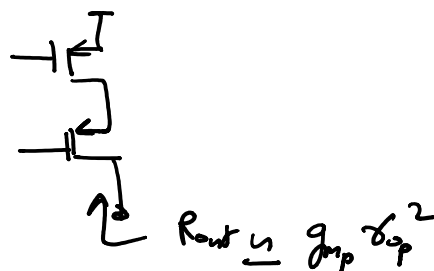
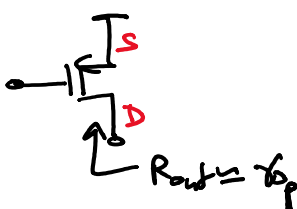
$$\Rightarrow g_{m1} = g_{m2} \quad r_{o1} = r_{o2} = r_o$$

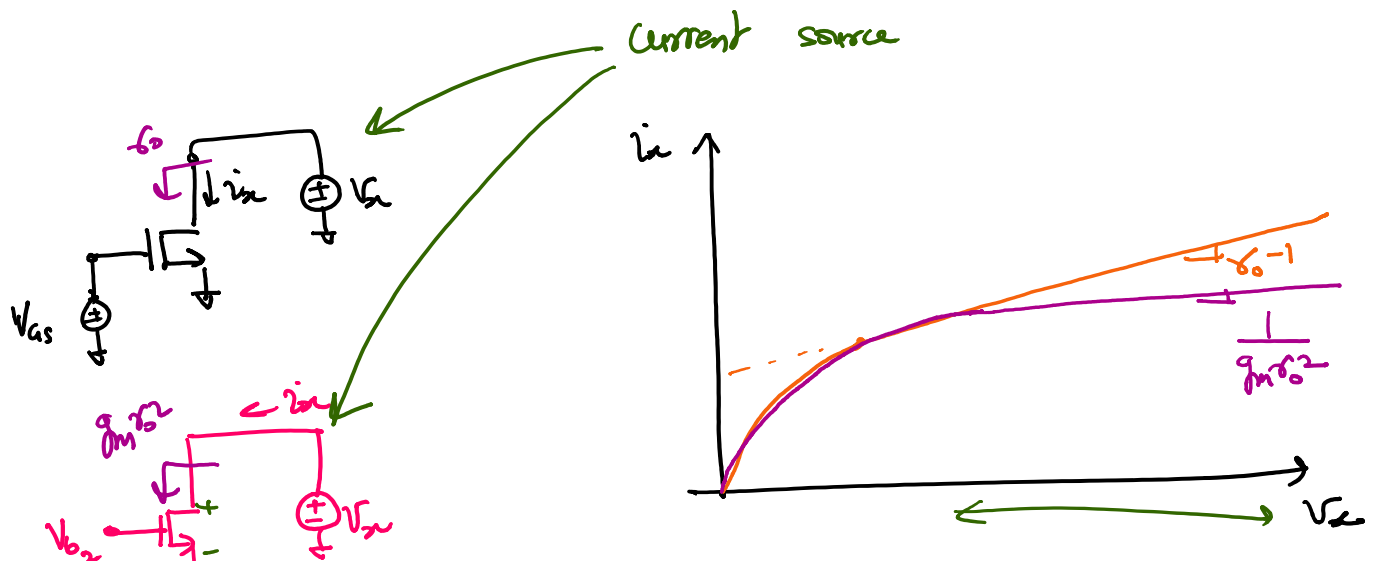
$$R_{out} \leq g_m r_o^2 + 2r_o \leq g_m r_o^2$$



Let $r_o = 10k\Omega$

$$g_m = \frac{1mA}{V}$$





forms a more precise current source (reference)
 $\Rightarrow R_{out} = g_m r_o^2 \Rightarrow r_o$

CASCODE current mirror/source

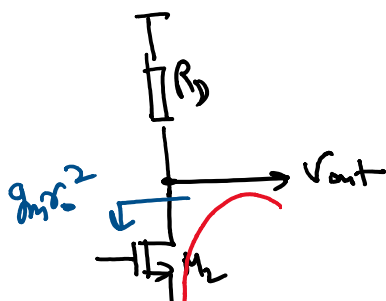
Cascade of Common Source & Common Gate
 $\sim |g|_o$

Common Source

CS + SD

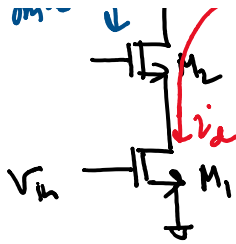
Output resistance ($g_m r_o^2$)

Cascode Structures



$$V_{out} = -i_d (R_D \parallel g_m r_o^2)$$

$$= -a_{v_i} (R_D \parallel a_{v_i})$$



$$v_{out} = -i_o (R_D \parallel g_{m2}^{-1})$$

$$= -g_{m1} v_{in} (R_D \parallel g_{m2}^{-1})$$

$$\Rightarrow A_v = -g_{m1} (R_D \parallel g_{m2}^{-1})$$

\uparrow
 $R_D = g_{m2}^{-1} \approx \frac{1}{g_{m2}}$

$$= -g_{m1} \underbrace{(g_{m2}^{-1} \parallel g_{m2}^{-1})}_{1/g_{m2}}$$

get gains boosted by 100-1000x