

Computational Electromagnetics in Antenna Analysis and Design

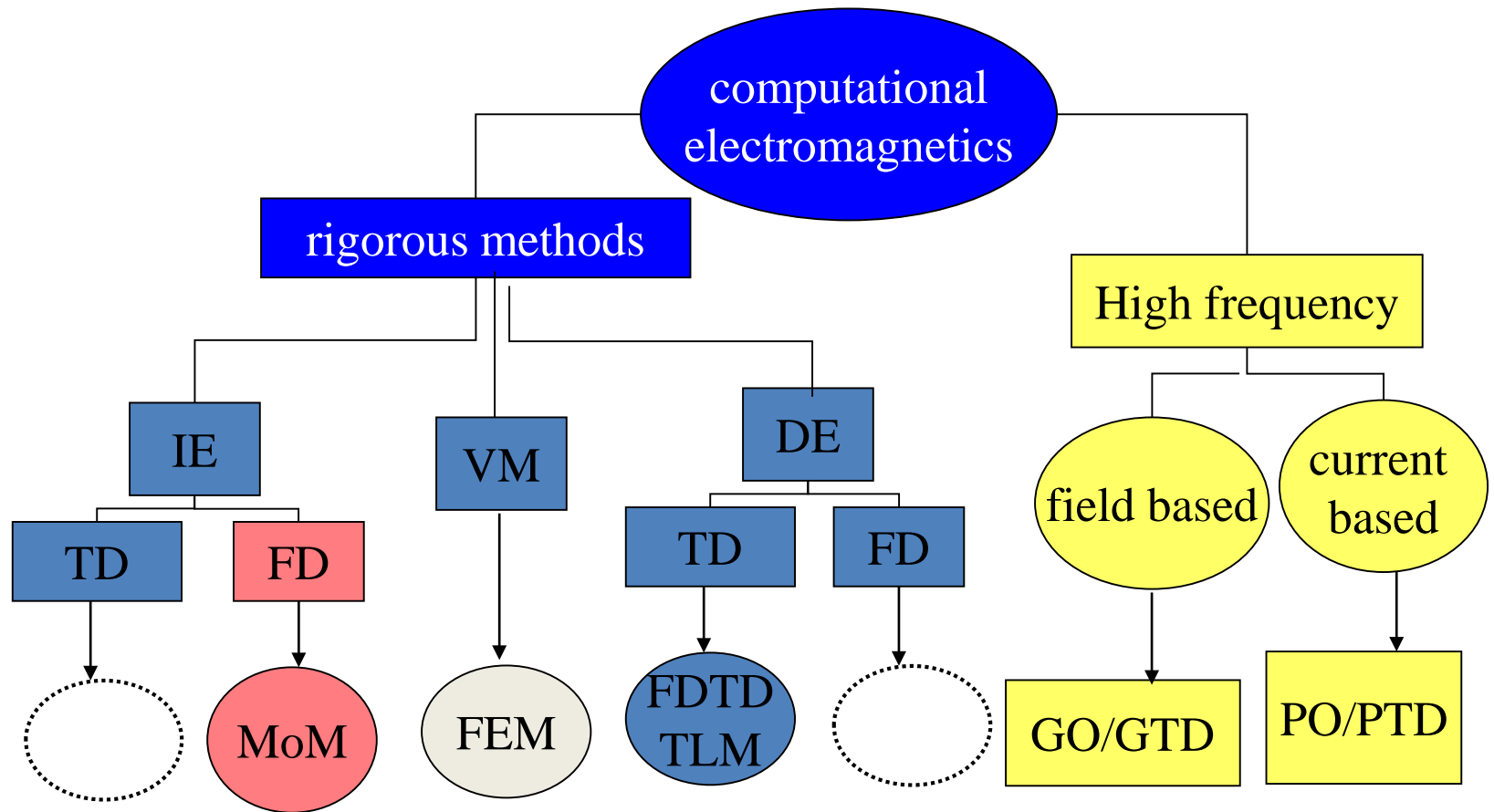
➤ It is rare for real-life EM problems to fall neatly into a class that can be solved by the analytical methods presented in the preceding lectures. Classical approaches may fail if:

- the material is not linear and cannot be linearized without seriously affecting the result
- the solution region is complex (i.e. the various boundaries do not coincide with any well described coordinate system).
- the boundary conditions are time-dependent
- the medium is inhomogeneous or anisotropic

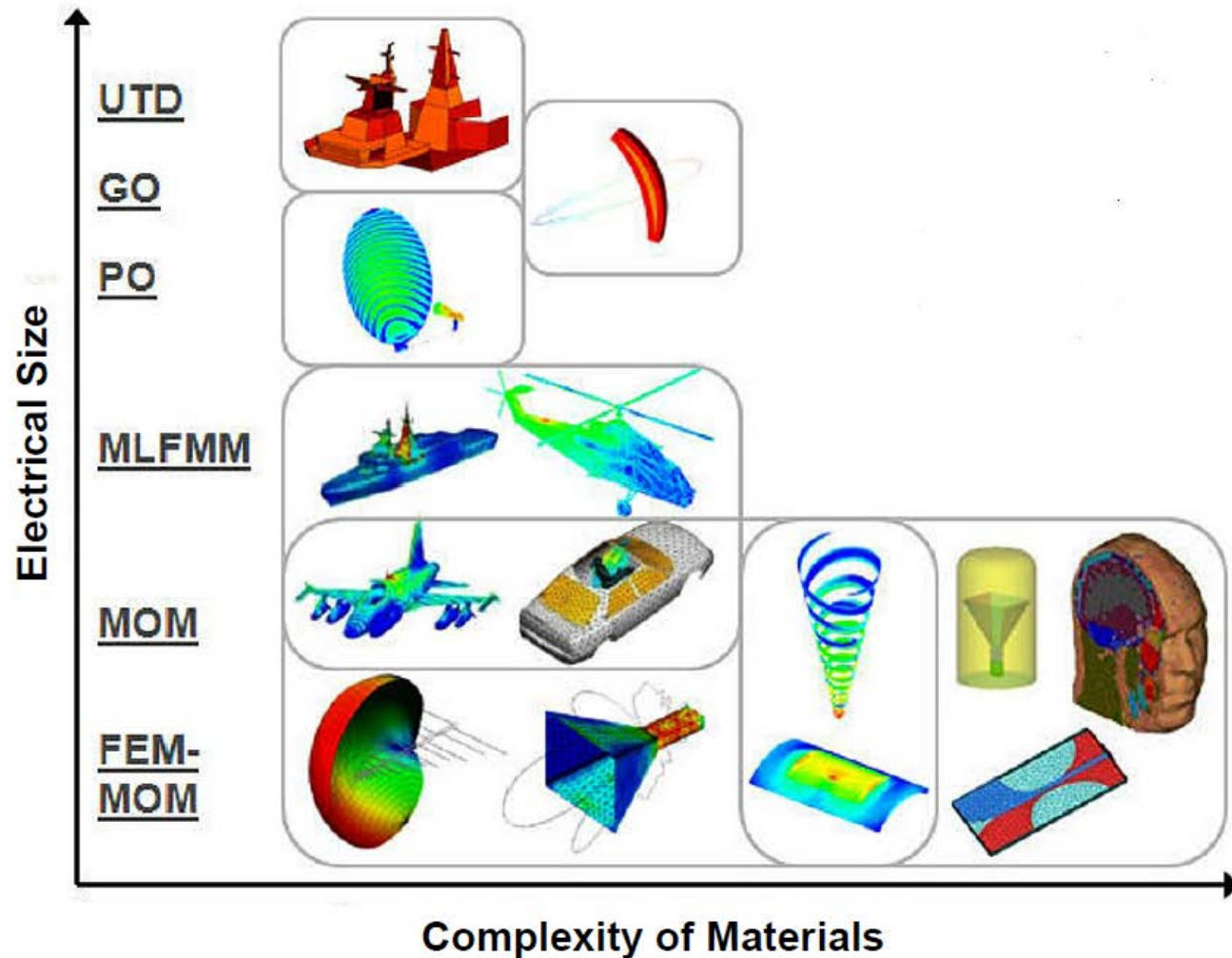
➤ Whenever a problem with such complexity arises, numerical solutions must be employed.

➤ Fortunately there are a large number of very good commercial programs available for solving antenna problems.

Computational Electromagnetics



The Universe of Antenna Modeling Methods



Courtesy of EMSS

Computational Electromagnetics

- **Method of moments (MoM)**

- A method for solving integro-differential equations such as Hallen's or Pocklington's equation at a given frequency
- Earliest and longest legacy of software codes for antenna modeling
- BRACT, WIRA, AMP, NEC, NEC-2, NEC-3, NEC-4, MiniNEC, ELNEC, EZNEC, winNECPlus, 4nec2, FEKO, WIPL-D, Zeland IE3D

- **Finite element method (FEM)**

- Best for design of small antennas of complex structure
- Ansoft HFSS

- **Finite difference time-domain method (FDTD)**

- Time-domain method
- Best for design of small antennas for broadband applications
- CST Microwave Studio, Zeland Fidelity, Faustus MEFiSTo

- **Geometric, physical, and uniform theories of diffraction**

- Best for electrically large antennas

Comparison of Methods

	Domain	Generality	Accuracy	Memory N= number of elements	Antenna Types
MoM	Frequency	Homogeneous or discretely homogeneous regions	Very accurate	@(N ²)	All but harder for large reflector antennas
FDTD	Time (all frequencies in one run)	Very general. inhomogeneous, dispersive, anisotropic	Moderately accurate	@(N)	All but harder for large reflector antennas
FEM	Frequency	Very general. inhomogeneous, dispersive, anisotropic	Very accurate	@(N log N)	All but harder for large reflector antennas
High Frequency Methods	Frequency	Only good for structures much larger than the wavelength	Only accurate for large structures	@(N)	Only good for large antennas (mostly used for reflectors)

Goal of all of these methods

Approximate these

$$\begin{aligned}\nabla \times \vec{E} &= -\frac{\partial \vec{B}}{\partial t} - \vec{M} & \nabla \times \vec{H} &= \frac{\partial \vec{D}}{\partial t} + \vec{J} \\ \nabla \cdot \vec{D} &= \rho & \nabla \cdot \vec{B} &= \rho_m\end{aligned}$$

With this

$$[A] \cdot [x] = [b]$$

The Method of Moments

Originators



I.G. Bubnov
1872-1919



Leonid Vitaliyevich Kantorovich
1912-1986



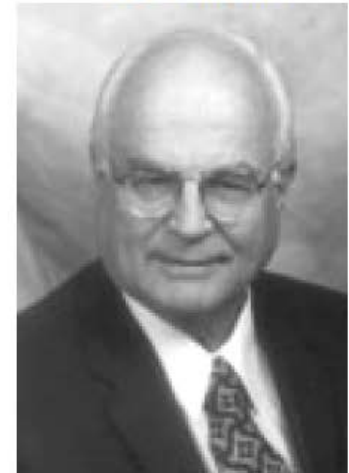
Jack H. Richmond
1922-1990



Boris Grigoryevich Galerkin
1871-1945



Gleb Pavlovich Akilov
1924-1964



Roger F. Harrington
1925-

Equations for Obtaining the Current Along a Wire

- Pocklington's equation (1897)

$$\int_{-l/2}^{l/2} I_z(z') \left[\left(\frac{\partial^2}{\partial z^2} + k^2 \right) G(z, z') \right] dz' = -j\omega\epsilon E_z^i(\rho = a)$$

- Hallen's equation (1938)

$$\int_{-l/2}^{l/2} I_z(z') \frac{e^{-jkR}}{4\pi R} dz' = -j\sqrt{\frac{\epsilon}{\mu}} [B_1 \cos(kz) + C_1 \sin(k|z|)]$$

- General form

$$L(f) = g$$

Linear operator Driving function

Unknown function

Integro-Differential Equations Made Simple

- Start with an equation. The analysis problem is to find f

$$L(f) = g$$

- Assume f can be expanded as a weighted sum of basis functions

$$L(f) = L\left(\sum_n a_n f_n\right) = g$$

- Set all projections (via test functions) of left and right sides equal

$$\sum_n a_n L(f_n \bullet \phi_m) = g \bullet \phi_m$$

- Write as a matrix equation

$$\begin{bmatrix} L(f_1 \bullet \phi_1) & \cdots & L(f_N \bullet \phi_1) \\ \vdots & \ddots & \vdots \\ L(f_1 \bullet \phi_M) & \cdots & L(f_N \bullet \phi_M) \end{bmatrix} \begin{bmatrix} a_1 \\ \vdots \\ a_N \end{bmatrix} = \begin{bmatrix} g \bullet \phi_1 \\ \vdots \\ g \bullet \phi_M \end{bmatrix}$$

The Solution

- Solve for the vector of expansion coefficients

$$\begin{bmatrix} a_1 \\ \vdots \\ a_N \end{bmatrix} = \begin{bmatrix} L(f_1 \bullet \phi_1) & \cdots & L(f_N \bullet \phi_1) \\ \vdots & \ddots & \vdots \\ L(f_1 \bullet \phi_M) & \cdots & L(f_N \bullet \phi_M) \end{bmatrix}^{-1} \begin{bmatrix} g \bullet \phi_1 \\ \vdots \\ g \bullet \phi_M \end{bmatrix}$$

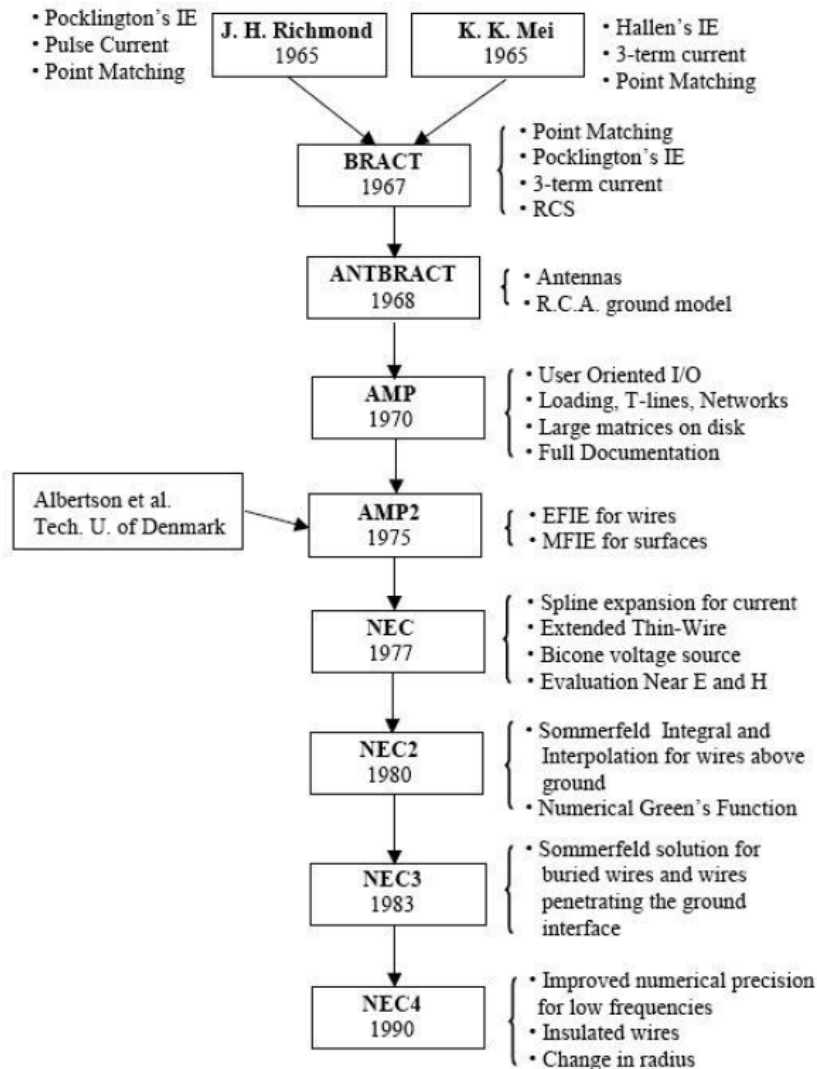
- Obtain f

$$f = \sum_n a_n f_n = [f_1 \quad \cdots \quad f_N] \begin{bmatrix} L(f_1 \bullet \phi_1) & \cdots & L(f_N \bullet \phi_1) \\ \vdots & \ddots & \vdots \\ L(f_1 \bullet \phi_M) & \cdots & L(f_N \bullet \phi_M) \end{bmatrix}^{-1} \begin{bmatrix} g \bullet \phi_1 \\ \vdots \\ g \bullet \phi_M \end{bmatrix}$$

Principle MoM Computer Codes

- **BRAC T & ANTBRAC T** – Developed late 1960's at MBAssociates, San Ramon
- **WIRA** – Developed early 1970's by M. Andreasen, F. Harris and R. Tanner at TCI
- **AMP/AMP2** – Developed mid 1970's by G. Burke at MBAssociates, San Ramon
- **NEC-1 (1979)** – Added more accurate current expansions; multiple wire junctions; thick wires
- **NEC-2 (1981)** – Sommerfield-Norton ground interaction for wire structures above lossy ground; numerical Green's function allows modifying without repeating whole calculation
- **NEC-3 (1985)** – Buried wires
- **NEC-4 (1992)** – Improved accuracy for stepped-radius wires and electrically-small segments, end caps and insulated wires, catenary-shaped wires, improved error detection
- **Zeland IE3D (1992)** – Adaptive meshing, developed by Dr. Jian-Xiong Zheng. Company in Fremont, CA
- **WIPL-D (ca 2000)** – Advanced MoM for wires, plates, and dielectrics based on work of A.R. Djordjevic, B.M. Kolundzija, U. Belgrade, Serbia
- **FEKO (ca 2000)** – Hybrid method developed by U. Jakobus at EMSS, Stellenbosch. South Africa

The Development of NEC



EZNEC <http://www.eznec.com/>

- **Developed by Roy Lewallen, W7EL**
- **Now in version 5.0**
- **Six products available**
 - EZNEC v.5 demo program \$0 (free)
 - EZNEC-ARRL v.3 & v.4 \$45 (on ARRL Antenna Book CD-ROM)
 - EZNEC v.5 \$90
 - EZNEC+ v.5 \$140
 - EZNEC Pro/2 v.5 \$500
 - EZNEC Pro/4 v.5 \$650 (sold only to NEC-4 licensees)
- **EZNEC includes either the NEC-2 or NEC-4 engines**
- **NEC-4 license for qualified US academic and noncommercial users can be obtained from Lawrence Livermore National Laboratory for \$300. This probably includes you!**
 - Form at: <https://ipo.llnl.gov/technology/software/documents/NEC.pdf>

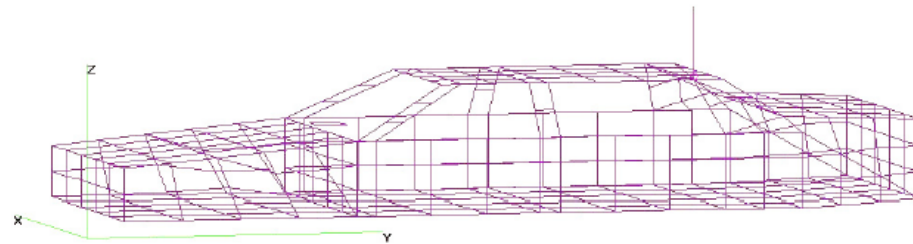
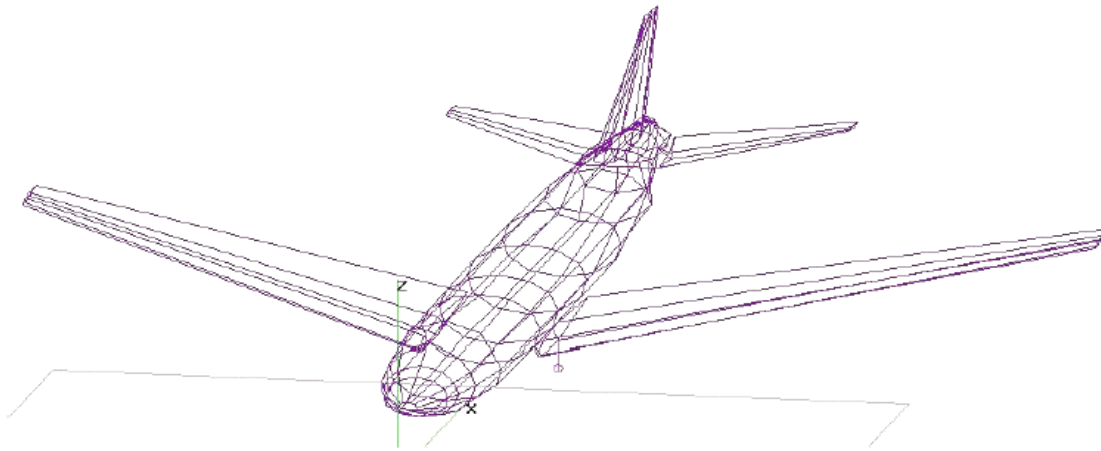
Key Parts of EZNEC

- **Specifying the antenna model**
 - Wire geometry (including radials)
 - Excitation sources
 - Wire loads
 - Transmission lines
 - Ground type and parameters
 - Frequency or sweep range
- **Specifying the desired outputs**
 - Radiation pattern crosssection at a given frequency
 - Gain in a specific direction
 - Pattern beamwidth
 - Front-to-back ratio
 - Front-to-rear ratio
 - Impedance
 - SWR
 - Output data files for other programs

4nec2 <http://home.ict.nl/~arivoors/>

- **A free full-featured GUI for NEC-2 and NEC-4**
- **Written and supported by Arie Voors, Netherlands**
- **Runs under Windows 2000 and XP**
- **Includes standard EZNEC models as .nec files**
- **Comes with NEC-2 executables but can use NEC-4 executables**
- **Comes configured for up to 11,000 segments but can be increased by to any number by recompiling the NEC-2 or NEC-4 source codes**
- **Two versions**
 - 4nec2 – limited to machine memory
 - 4nec2X – uses virtual memory for bigger problems
- **Has 3D graphics and two optimizers**
 - Gradient descent optimizer
 - Genetic optimizer
- **Permits writing NEC script, thereby giving access to all NEC-2 and NEC-4 commands**

4nec2 Wire-Grid Models of Boeing 747 and Automobile



4nec2 Screen Displays

Main screen

Main [V5.7.2] (F2)

File Edit Settings Calculate Window Show Run Help

Filename: 747PLANE.NEC Frequency: 2 Mhz
Wavelength: 149.9 mtr

Voltage: _____ Current: _____

Impedance: _____ Series comp.: _____
Parallel form: _____ Parallel comp.: _____

S.W.R. 50: _____ Input power: _____ W
Efficiency: _____ % Structure loss: _____ W
Radiat-eff.: _____ % Network loss: _____ W
Radiat-power: _____ W

Environment

Ground symmetry, wires for Z=0 not connected.
Finite/Fast ground, diel-const.=13, conduct.=5 mS

Comment

"747-200 Wire frame AWG 12 2 brake points 500-150"
Location Wire length Seg length # Seg Diam(IN) Dim (M)
Devisors are 200 150 and 25
Card wire # # sect x1 y1 z1 x2 y2 z2 wire size ! Wires

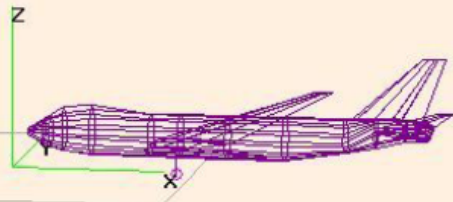
Seg's/patches: 1603 start stop count step
Pattern lines: _____
Freq/Eval steps: 1
Calculation time: 65.050 s

Geometry screen

Geometry (F3)

Show View Validate Currents Far-field Near-field Wire Plot

747PLANE.NEC 2 MHz



Theta : 80 Axis : 20 mtr Phi : 280

Edit screen

747PLANE.NEC - 4nec2 Edit

File Cell Rows Selection Options

Upd Ins Del

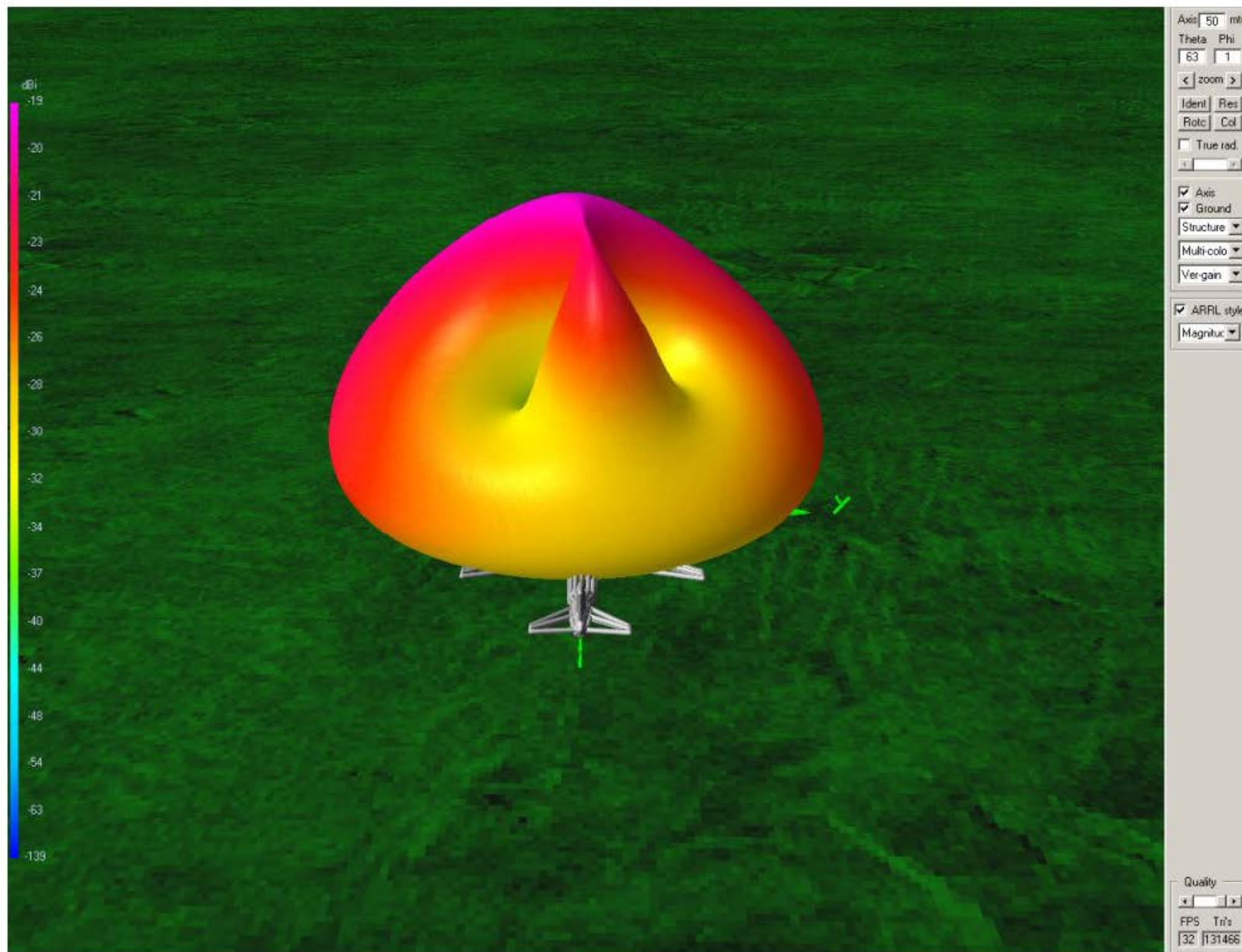
Symbols **Geometry** Source/Load Freq./Ground Others Comment

Geometry (Scaling=02) Use wire tapering

Nr	Type	Tag	Segs	X1	Y1	Z1	X2	Y2	Z2	Radius
1	Wire	1	5	1102.48	-128.50	118.35	1102.00	-128.50	0.00	81.0E-3
2	Wire	2	1	100.00	20.00	226.00	100.00	15.00	239.00	81.0E-3
3	Wire	3	1	100.00	15.00	239.00	100.00	9.00	245.00	81.0E-3
4	Wire	4	1	100.00	9.00	245.00	100.00	0.00	246.00	81.0E-3
5	Wire	5	1	100.00	0.00	246.00	100.00	-9.00	245.00	81.0E-3
6	Wire	6	1	100.00	-9.00	245.00	100.00	-15.00	239.00	81.0E-3
7	Wire	7	1	100.00	-15.00	239.00	100.00	-20.00	226.00	81.0E-3
8	Wire	8	1	100.00	-20.00	226.00	100.00	-19.00	219.00	81.0E-3

Wire tab

4nec2 3D Pattern of Antenna on 747 – Vert Pol

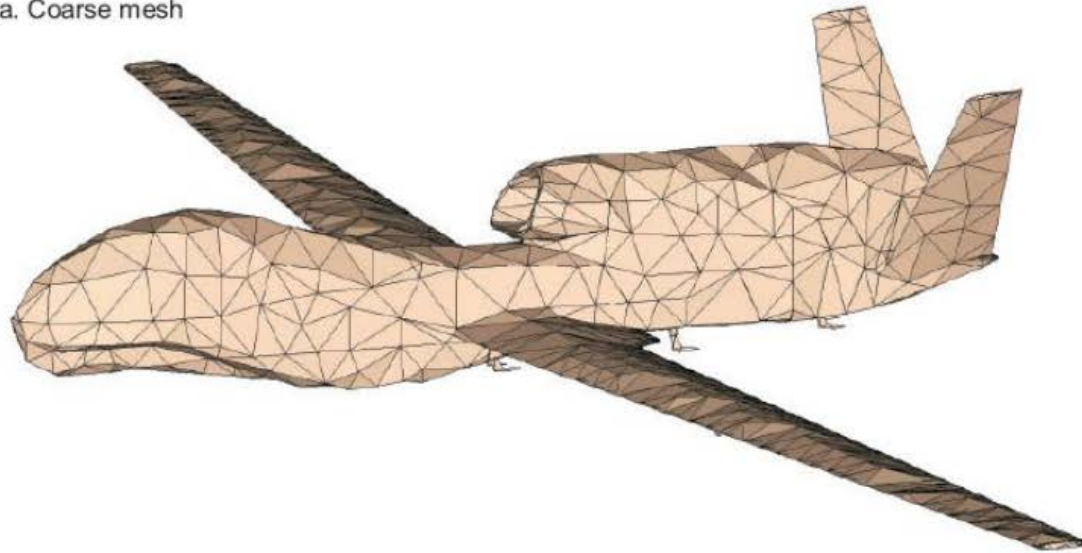


FEKO <http://www.feko.info/>

- Developed and sold by EM Software & Systems (EMSS), South Africa
- Switches automatically among multiple “engines” like a Toyota Prius
- Main method is MoM/SIE, but has MoM/VIE, FEM, FMM, and several optics approximations
- Capabilities similar to WIPL-D: lossy conductors, dielectric and magnetic materials, near and farfield calculations, optimizer
- Curved surfaces are approximated by many flat triangles
- Triangle surface meshing and low-order basis functions give heavy computation burden, hence the need for multiple engines
- Has infinite Sommerfeld-Norton ground
- Limited LITE version of interest to Radio Amateurs
 - FEKO LITE – Free download from <http://www.feko.info/sales>

FEKO Model of Global Hawk (RQ-4A)

a. Coarse mesh



b. Refined mesh

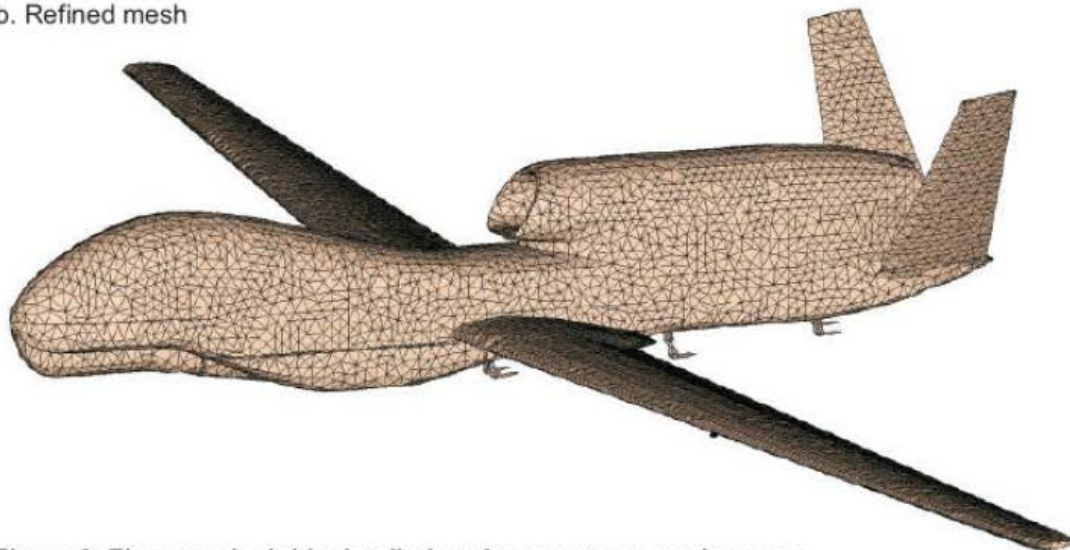


Figure 2. Finer mesh yields detailed surface contour, as shown on

FEKO Pattern of Horn Antenna in Wing Pod

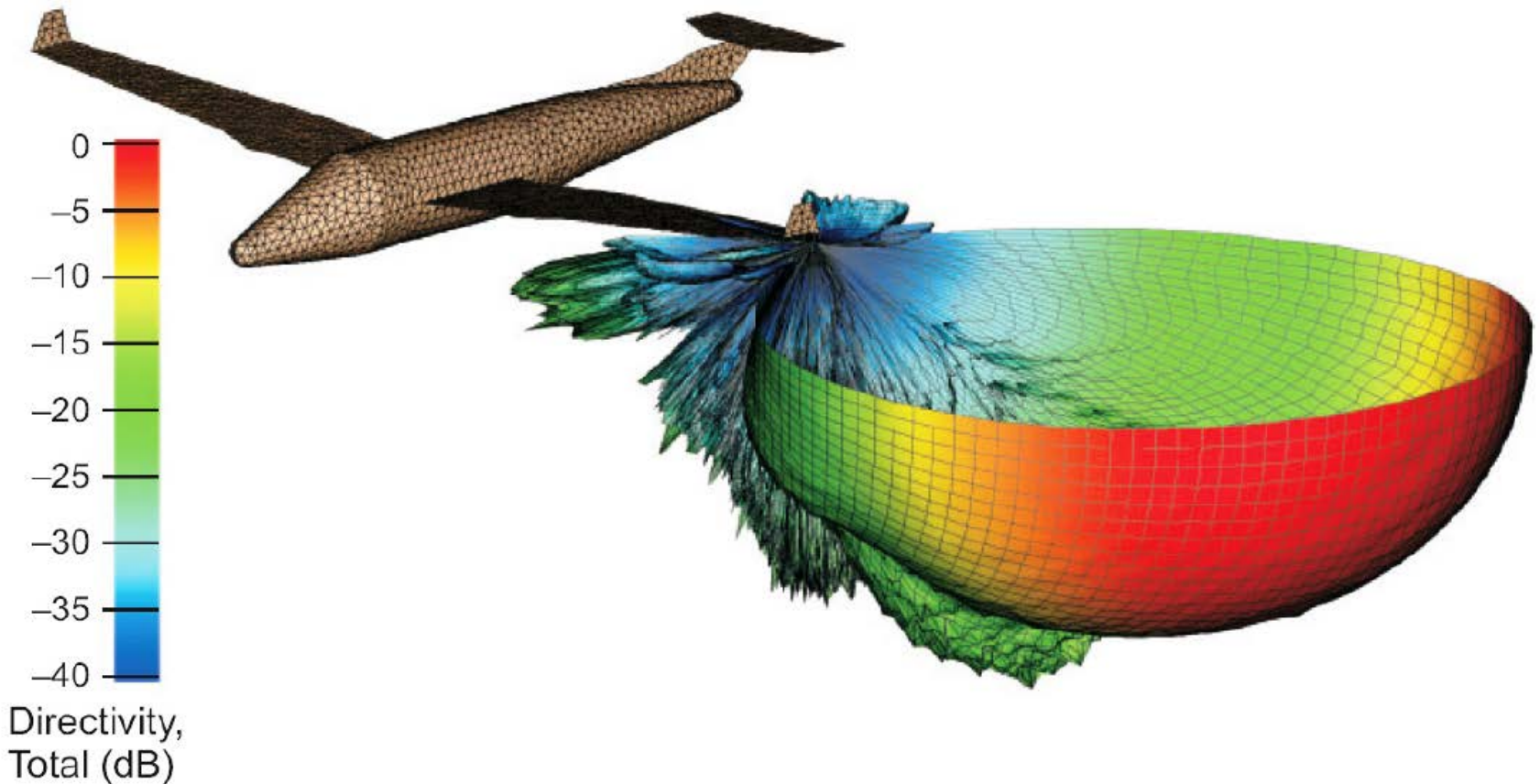
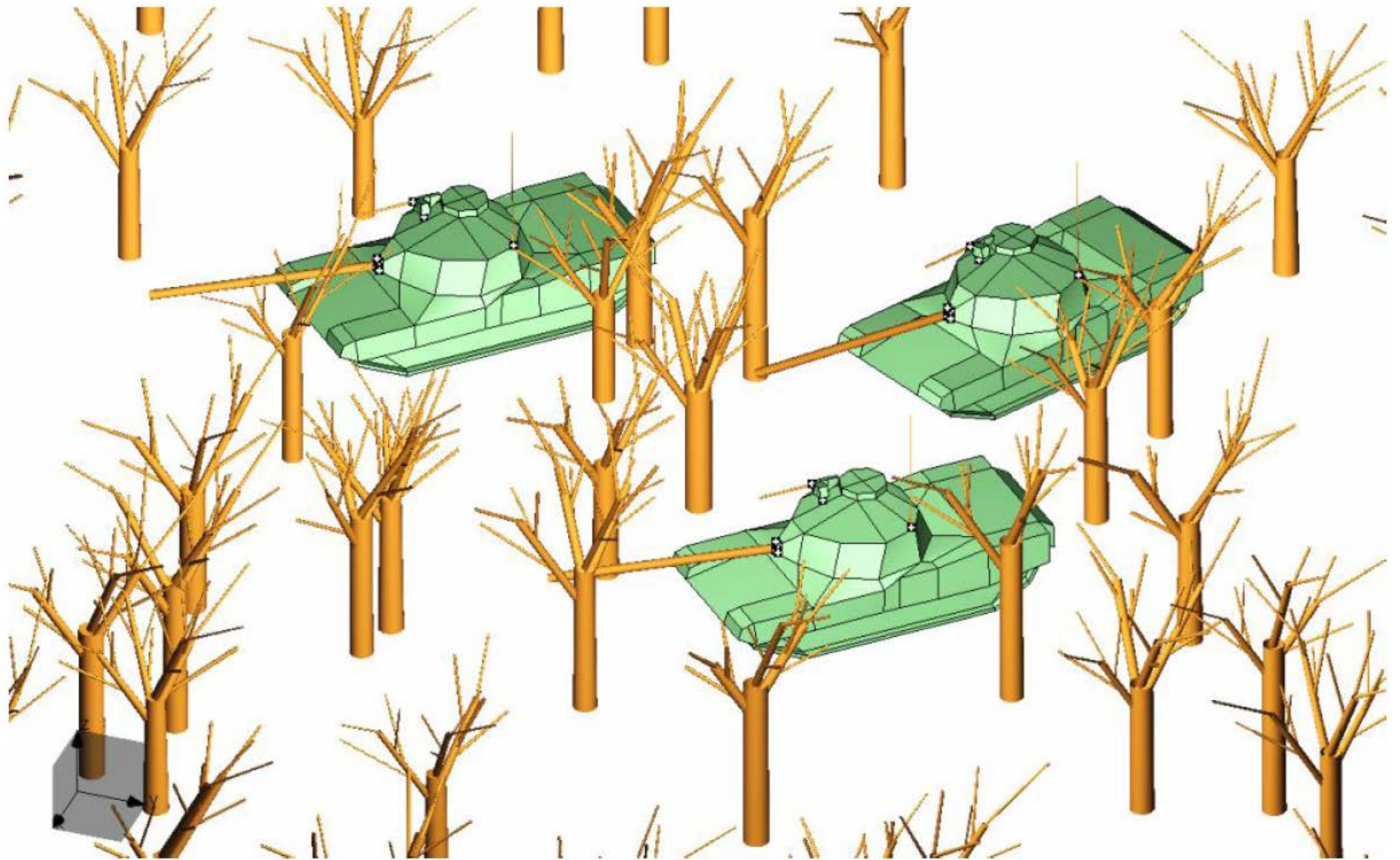
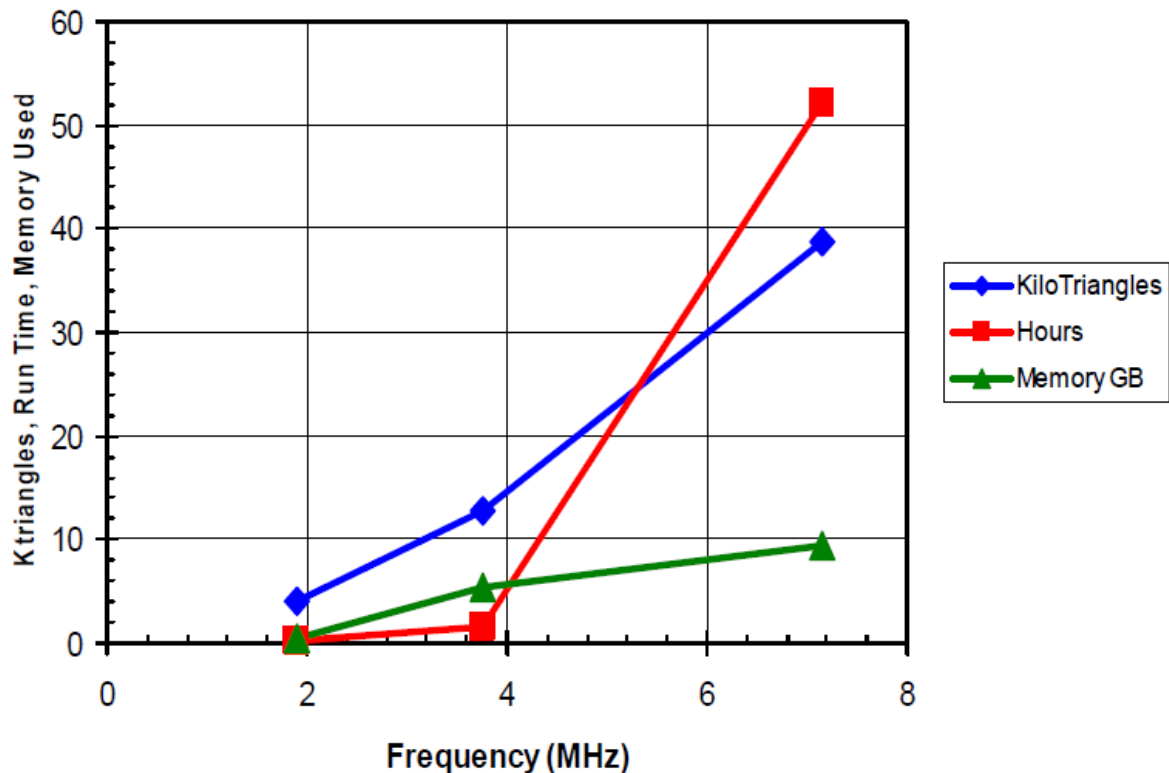


Figure 8. Pod location, performance of horn array at 90 deg

The Next Step – Modeling the Landscape



Required Computation



Frequency (kHz)	Triangles	Hours	Memory (GB)
1,900	3,928	0.125	0.53
3,750	12,834	1.54	5.48
7,150	38,717	52.1	9.38

Other Useful Antenna Software

- **winSMITH 2.0 by Agilent (formerly Eagleware)**
 - ISBN 1884932908
 - \$127 from SciTech Publishing <http://www.scitechpublishing.com/>
 - \$149 from Amazon.com
 - For interactive design of ladder networks for impedance matching
 - Excellent tool for learning to use the Smith chart
 - Grossly overpriced
- **MultiNEC by Dan Maguire, AC6LA, <http://www.ac6la.com>**
 - Excel/Visual Basic program; low cost but currently unavailable
 - Puts NEC, EZNEC, and 4nec2 on autopilot for making a series of runs
 - Inexpensive alternative to a real optimizer
 - Doesn't work with EZNEC-ARRL
 - Temporarily unavailable

Finite Difference Time Domain

FDTD

Reason for interest in FDTD

In the time domain, Maxwell's equations give rise to PDEs involving time and spatial derivatives.

Some good reasons for dealing with PDE's are:

- Complex-value materials easily accommodated.
- Computer resources are adequate.
- PDE solutions are robust.
- Time domain PDE methods usually have no matrices.
- Geometries to be solved can be more varied.

Some big advantages

- Broadband response with a single excitation.
- 3D models easily.
- Memory requirement scales linearly with problem size
- Frequency dependent materials accommodated.
- Most parameters can be generated e.g.

Scattered fields

antenna patterns

RCS

S-parameters

etc.....

How does it work?

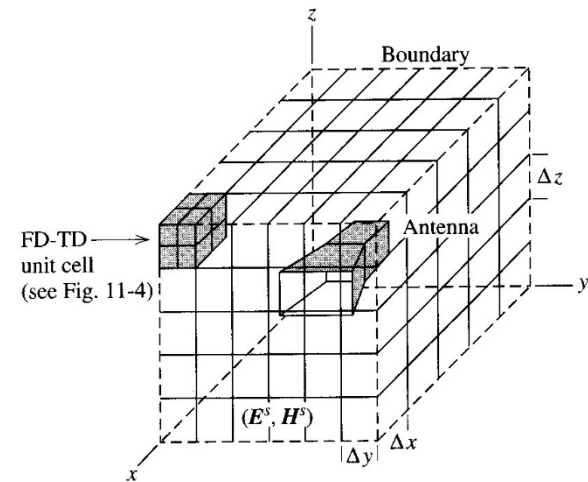
Based on the two Maxwell curl equations in derivative form. These are linearized by central finite differencing. We only consider nearest neighbor interactions because all the fields are advanced temporally in discrete time steps over spatial cells.

ie we sample in space & time

embedding of an antenna

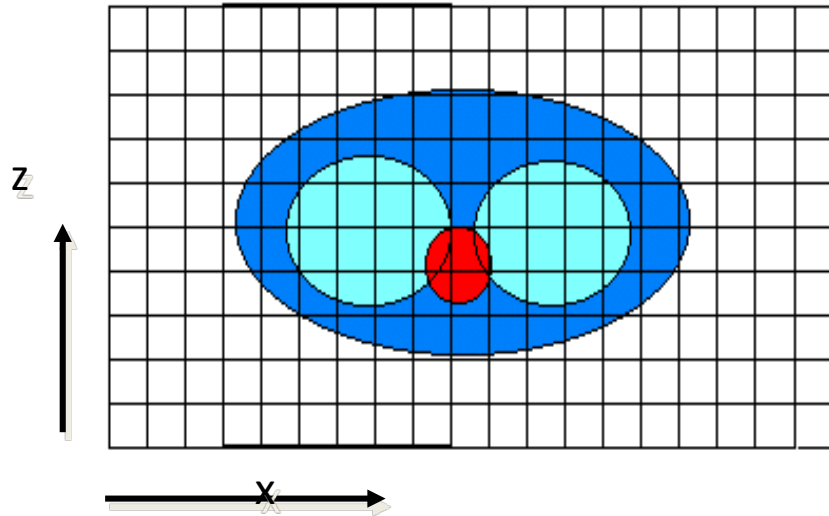
in a FDTD space lattice

(note that the whole volume is meshed!)

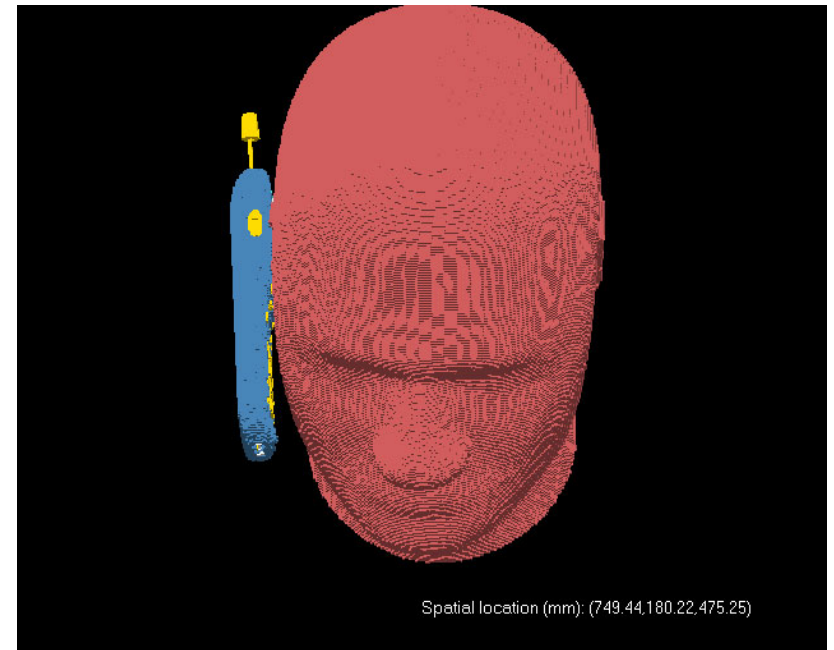


Discretize Objects in Space using Cartesian Grid

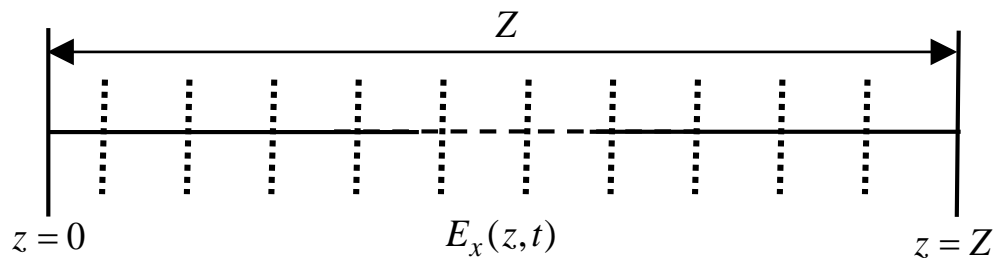
2D Discretization



3D Discretization

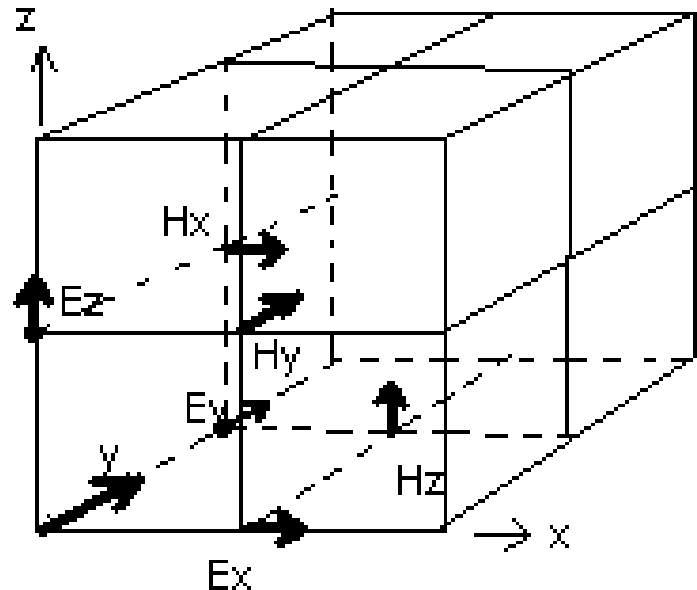


1D Discretization



Define Locations of Field Components: FDTD Cell called Yee Cell

- Finite-Difference
 - Space is divided into small cells
One Cell: $(dx)(dy)(dz)$
 - E and H components are distributed in space around the Yee cell (note: field components are not collocated)



FDTD: Yee, K. S.: Numerical solution of initial boundary value problems involving Maxwell's equations in isotropic media. *IEEE Transactions on Antennas Propagation*, Vol. AP-14, pp. 302-307, 1966.

3D formulation

$$\frac{\partial H_x}{\partial t} = \frac{1}{\mu} \left(\frac{\partial E_y}{\partial z} - \frac{\partial E_z}{\partial y} - \rho' H_x \right)$$

$$\frac{\partial H_y}{\partial t} = \frac{1}{\mu} \left(\frac{\partial E_z}{\partial x} - \frac{\partial E_x}{\partial z} - \rho' H_y \right)$$

$$\frac{\partial H_z}{\partial t} = \frac{1}{\mu} \left(\frac{\partial E_x}{\partial y} - \frac{\partial E_y}{\partial x} - \rho' H_z \right)$$

Convert
equations like
these

$$\frac{\partial E_x}{\partial t} = \frac{1}{\varepsilon} \left(\frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} - \sigma E_x \right)$$

$$\frac{\partial E_y}{\partial t} = \frac{1}{\varepsilon} \left(\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} - \sigma E_y \right)$$

$$\frac{\partial E_z}{\partial t} = \frac{1}{\varepsilon} \left(\frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} - \sigma E_z \right)$$

To ones like
these

$$H_x^{n+\frac{1}{2}}(i, j+\frac{1}{2}, k+\frac{1}{2}) - H_x^{n-\frac{1}{2}}(i, j+\frac{1}{2}, k+\frac{1}{2}) = \frac{1}{\mu_0 \mu_r(i, j+\frac{1}{2}, k+\frac{1}{2})} \left[\frac{E_y^n(i, j+\frac{1}{2}, k+\frac{1}{2}) - E_y^n(i, j+\frac{1}{2}, k)}{\Delta z} - \frac{E_z^n(i, j+\frac{1}{2}, k+\frac{1}{2}) - E_z^n(i, j, k+\frac{1}{2})}{\Delta y} \right]$$

$$H_x^{n+\frac{1}{2}}(i+\frac{1}{2}, j, k+\frac{1}{2}) - H_x^{n-\frac{1}{2}}(i+\frac{1}{2}, j, k+\frac{1}{2}) = \frac{1}{\mu_0 \mu_r(i+\frac{1}{2}, j, k+\frac{1}{2})} \left[\frac{E_z^n(i+1, j, k+\frac{1}{2}) - E_z^n(i, j, k+\frac{1}{2})}{\Delta x} - \frac{E_x^n(i+\frac{1}{2}, j, k+1) - E_x^n(i+\frac{1}{2}, j, k)}{\Delta z} \right]$$

$$\frac{H_z^{n+\frac{1}{2}}(i+\frac{1}{2}, j+\frac{1}{2}, k) - H_z^{n-\frac{1}{2}}(i+\frac{1}{2}, j+\frac{1}{2}, k)}{\Delta t} = \frac{1}{\mu_0 \mu_r(i+\frac{1}{2}, j+\frac{1}{2}, k)} \left[\frac{E_x^n(i+\frac{1}{2}, j+1, k) - E_x^n(i+\frac{1}{2}, j, k)}{\Delta y} - \frac{E_y^n(i+1, j+\frac{1}{2}, k) - E_y^n(i, j+\frac{1}{2}, k)}{\Delta x} \right]$$

$$\frac{E_x^{n+1}(i+\frac{1}{2}, j, k) - E_x^n(i+\frac{1}{2}, j, k)}{\Delta t} = \frac{1}{\varepsilon_0 \varepsilon_r(i+\frac{1}{2}, j, k)} \left[\frac{H_z^{n+\frac{1}{2}}(i+\frac{1}{2}, j+\frac{1}{2}, k) - H_z^{n+\frac{1}{2}}(i+\frac{1}{2}, j-\frac{1}{2}, k)}{\Delta y} - \frac{H_y^{n+\frac{1}{2}}(i+\frac{1}{2}, j, k+\frac{1}{2}) - H_y^{n+\frac{1}{2}}(i+\frac{1}{2}, j, k-\frac{1}{2})}{\Delta z} \right] -$$

$$\sigma(i+\frac{1}{2}, j, k) \left[\frac{E_x^{n+1}(i+\frac{1}{2}, j, k) + E_x^n(i+\frac{1}{2}, j, k)}{2} \right]$$

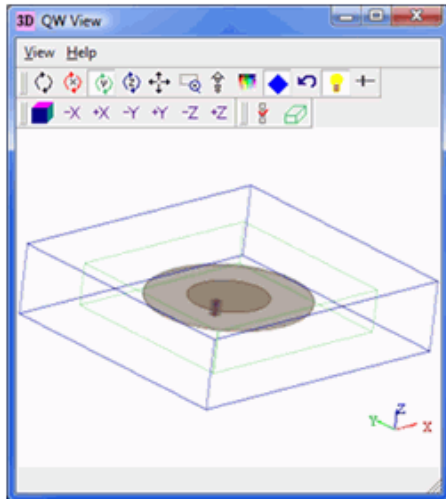
QuickWave (<http://www.qwed.eu/>)

- **Commercial FDTD package with CAD interface**
- **Uses conformal FDTD mesh**
- **Many special features for antenna problems**
- **Written and supported by QWED, Poland**
- **Runs under 32/x64 bit Windows platforms and Linux**

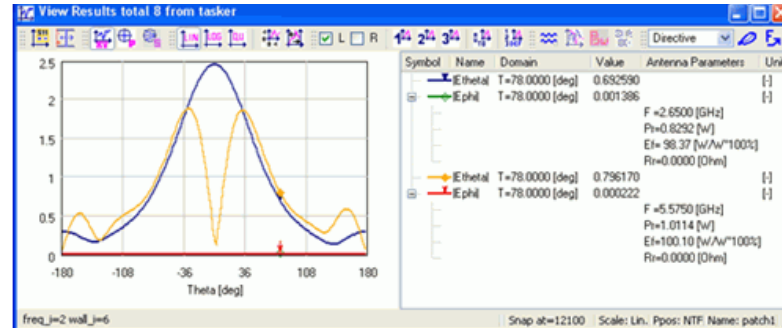
QuickWave (<http://www.qwed.eu/>)

Examples:

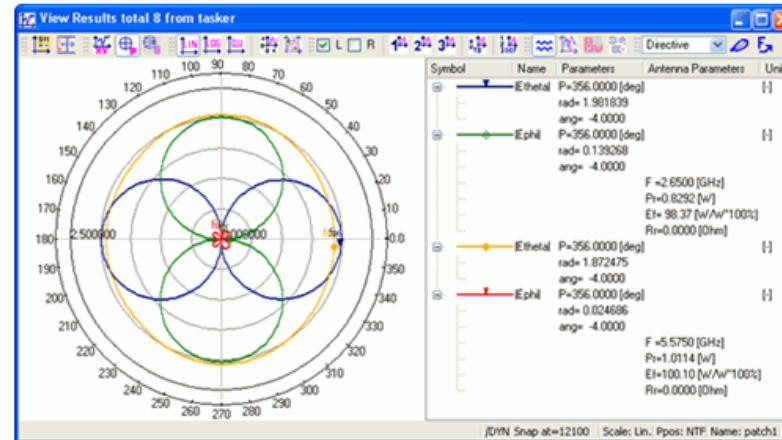
Circular Patch Antenna - a circular patch fed by a thin vertical coax line



Circular patch antenna model



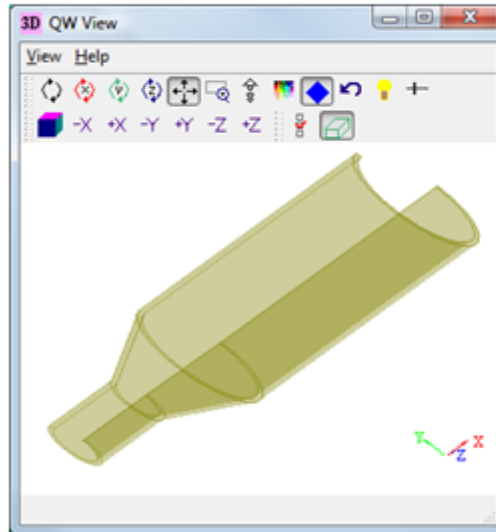
Radiation patterns versus elevation angle Θ with azimuthal angle $\Phi=0$, calculated for two frequencies: 2.65 and 5.575 GHz.



Radiation patterns versus azimuthal angle Φ with elevation angle $\Theta=30^\circ$, calculated for two frequencies: 2.65 and 5.575 GHz.

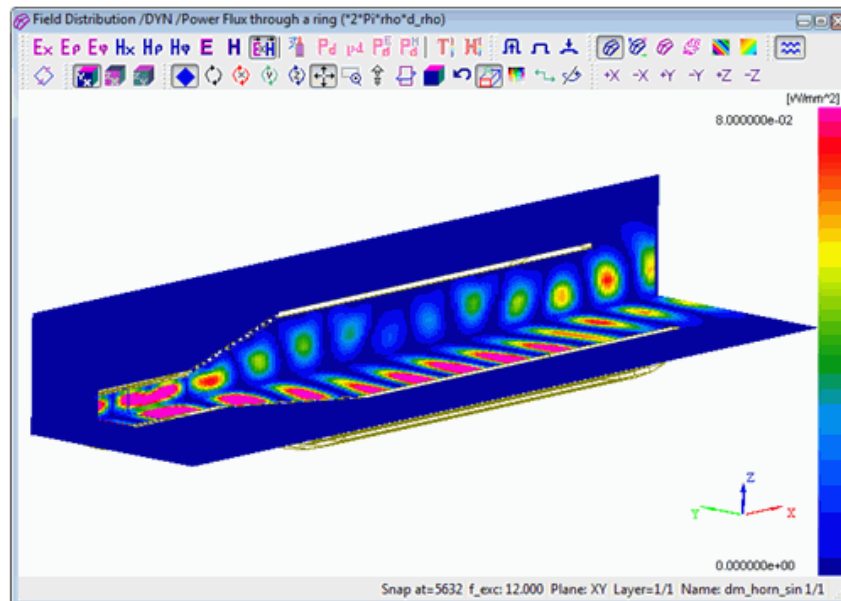
QuickWave (<http://www.qwed.eu/>)

Examples: Dual mode horn antenna (V2D example)



Consider *Standard/Dmhorn/dm_horn.pro*, which is an example of dual-mode axisymmetrical horn antenna [43]. Input of the antenna is excited with the fundamental mode TE₁₁ of 10..14 GHz spectrum range. However, as the wave propagates through the tapered section, some of its energy is transformed into TM₁₁ mode. Thus, an appropriate design allows us to equalise polarisation in E and H planes. It makes this horn a good feed for reflector antennas. Additionally, proper choices of flare angle and length of the horn's tube help suppress the side lobes in the radiation pattern. Changing *Gain Reference* in the *Radiation pattern* window from *Relative* to *Directive* we see that the gain of this antenna is about 14.5 dB for both E and H planes. The 3 dB beamwidth is 35.4° and 37° for the E and H plane, respectively.

Dual mode horn antenna model



Sinusoidal excitation of the model at the central frequency ($f = 12$ GHz) confirms that the same radiation levels at both E and H planes are obtained at the end of the antenna.

Poynting vector for example with sinusoidal excitation.

XFtdt (<http://www.remcom.com/>)

- **Commercial FDTD package with CAD interface**
- **Probably the most popular FDTD package for antenna problems**
- **Many special features for antenna problems including full human body mesh**
- **Written and supported by Remcom, USA**
- **Runs under 32/x64 bit Windows, Mac OS X and Linux**

XFDTD (<http://www.remcom.edu/>)

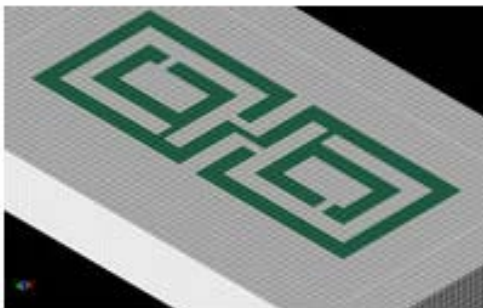
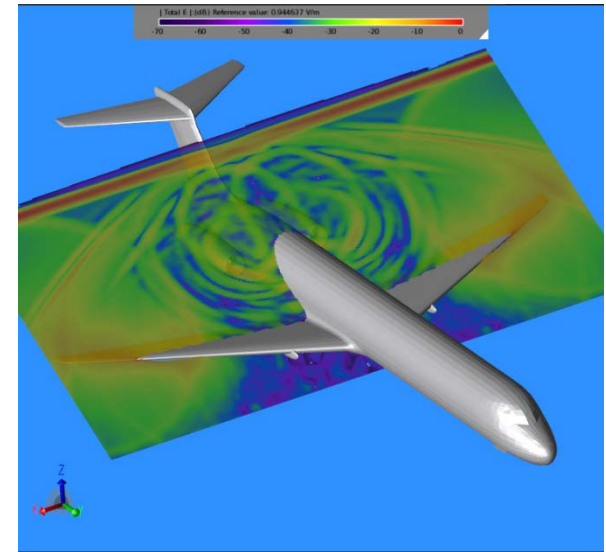
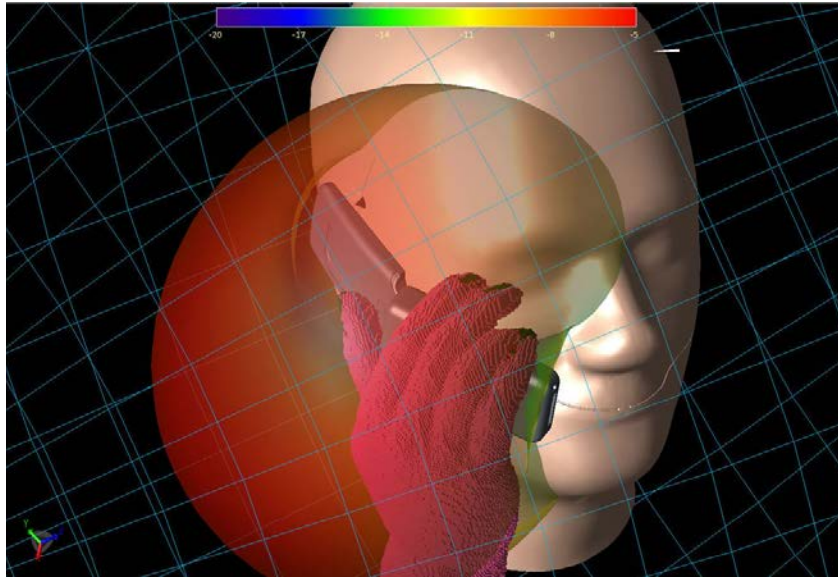


Figure 1
A CAD representation of the cavity-backed antenna. The white material represents the metal layers while the green color is the dielectric substrate under the slots.

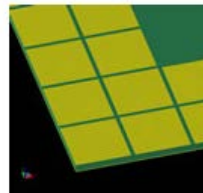


Figure 5
Mesh representation of EBG reflector.

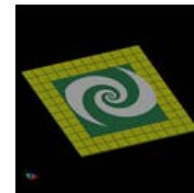


Figure 6
Full model with spiral antenna and EBG reflector.

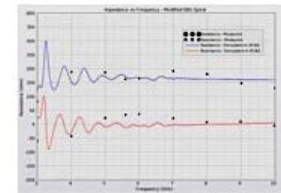


Figure 7
Comparison of impedance of antenna over EBG reflector.

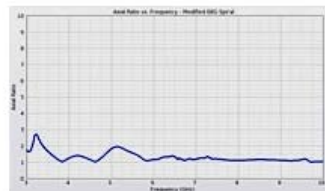


Figure 8
Axial ratio of antenna over EBG reflector.

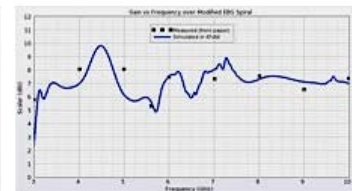
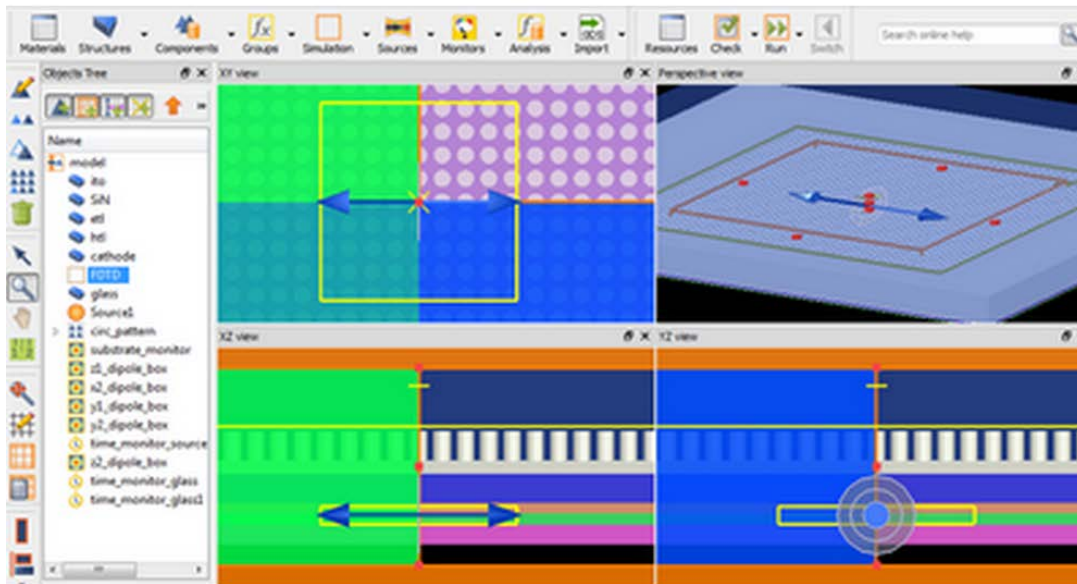
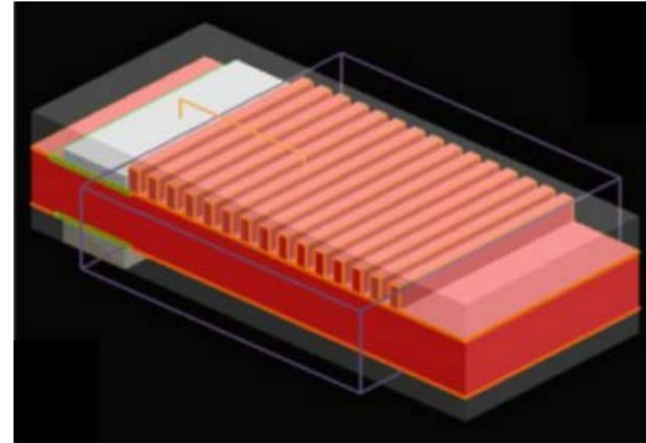
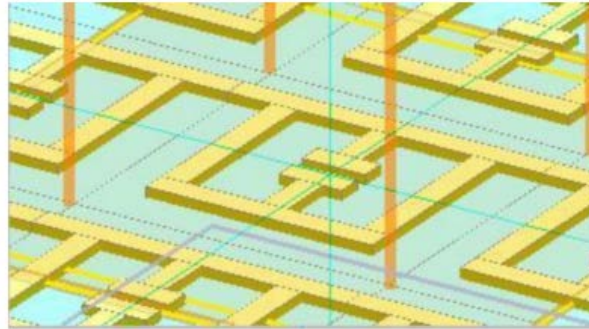
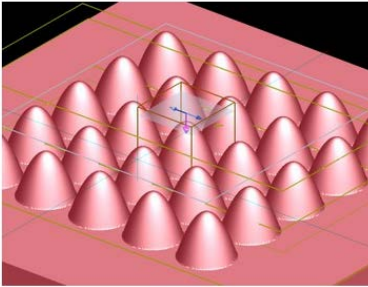


Figure 9
Comparison of peak gain of antenna over EBG reflector.

Lumerical (<http://www.lumerical.com> /)

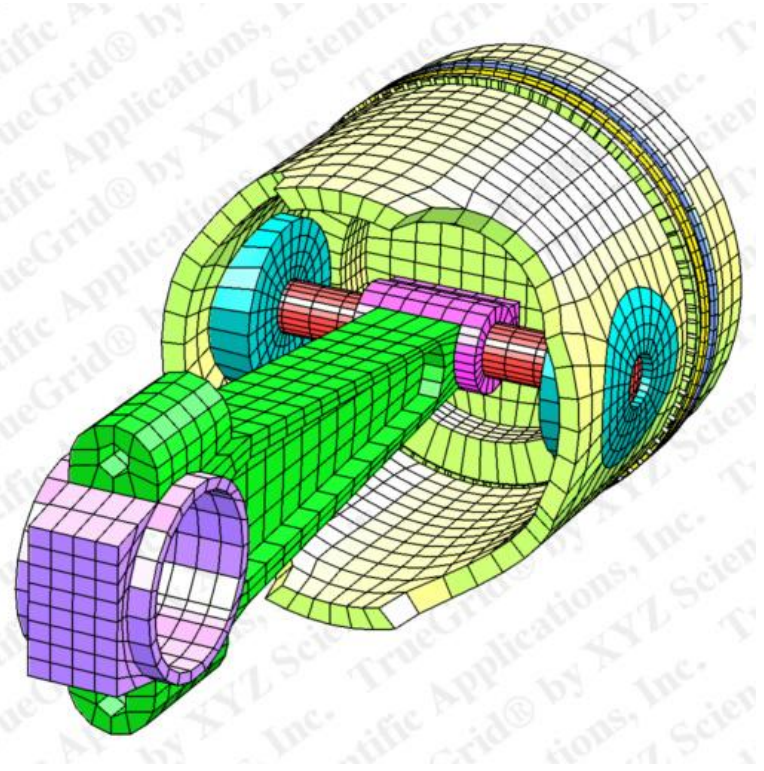
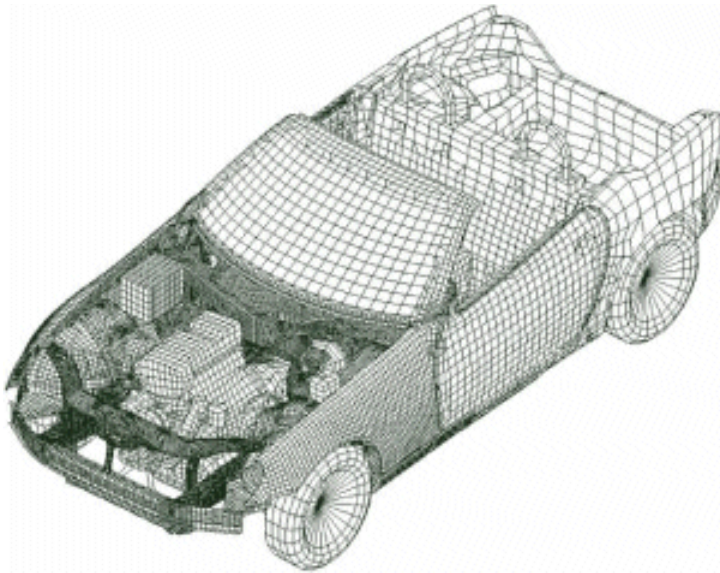
- Commercial FDTD package with CAD interface
- Popular FDTD package for the optics folks (i.e. integrated optics, light scattering, plasmonics)
- Large library of materials at optical wavelengths
- Has very nice scripting language for defining large complicated problems.
- Has nice built in optimization
- Runs under 32/x64 bit Windows, Mac OS X and Linux

Lumerical (<http://www.lumerical.com/>)



Finite Element Method

Finite Element Method



Variational Approach

In solving problems arising in physics and engineering it is often possible to replace the problem of integrating a differential equation by the equivalent problem of seeking a function that gives a minimum value of some integral. Problems of this type are called *variational problems*.

The methods that allow us to reduce the problem of integrating a differential equation to the equivalent variational problem are usually called *variational methods*.

Variational Approach

Name of equations	PDE	Variational principle
Homogeneous wave equation with sources	$\nabla^2 \Phi + k^2 \Phi = g$	$I(\Phi) = \frac{1}{2} \int_v [\nabla \Phi ^2 - k^2 \Phi^2 + 2g\Phi] dv$
Homogeneous wave equation without sources	$\nabla^2 \Phi + k^2 \Phi = 0$	$I(\Phi) = \frac{1}{2} \int_v [\nabla \Phi ^2 - k^2 \Phi^2] dv$
Diffusion equation	$\nabla^2 \Phi - k \frac{\partial \Phi}{\partial t} = 0$	$I(\Phi) = \frac{1}{2} \int_t \int_v [\nabla \Phi ^2 - k^2 \Phi \frac{\partial \Phi}{\partial t}] dv dt$
Poisson's equation	$\nabla^2 \Phi = g$	$I(\Phi) = \frac{1}{2} \int_v [\nabla \Phi ^2 + 2g\Phi] dv$
Homogenous Laplace's equation	$\nabla^2 \Phi = 0$	$I(\Phi) = \frac{1}{2} \int_v [\nabla \Phi ^2] dv$

Finite Element Method

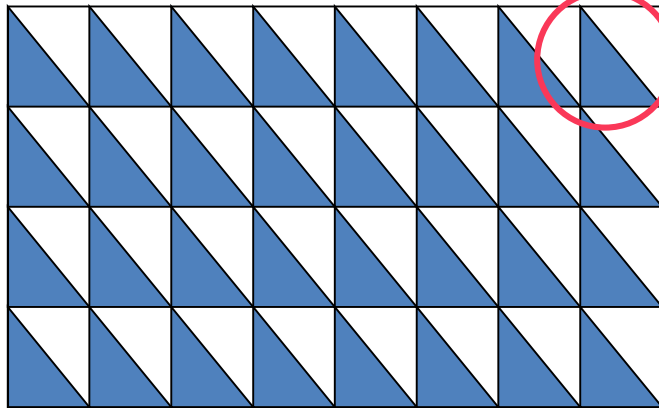
The finite element method (FEM) has its origin in the field of structural analysis. However, since then the method has been employed in nearly all areas of computational physics and engineering.

The FEM method, while more difficult to program than either the finite difference (FD) or method of moments (MOM), is a more powerful and versatile numerical technique for handling problems involving complex geometries and inhomogeneous media.

Basic concept

Although the behaviour may be complex when viewed over a large region, a simple approximation may suffice over a small subregion.

The region is divided up into **finite elements**.



(usually, triangles or squares,
but can be more complicated)

Regardless of the shape the field is approximated by a different expression over each element, maintaining continuity at adjoining elements.

Solution Strategy: Variational Approach

The equations to be solved are usually stated not in terms of field the variables but in terms of an integral-type functional such as energy.

The functional is chosen such that the field solution makes the functional stationary

The total functional is the sum of the integral over each element

Finite Element Method

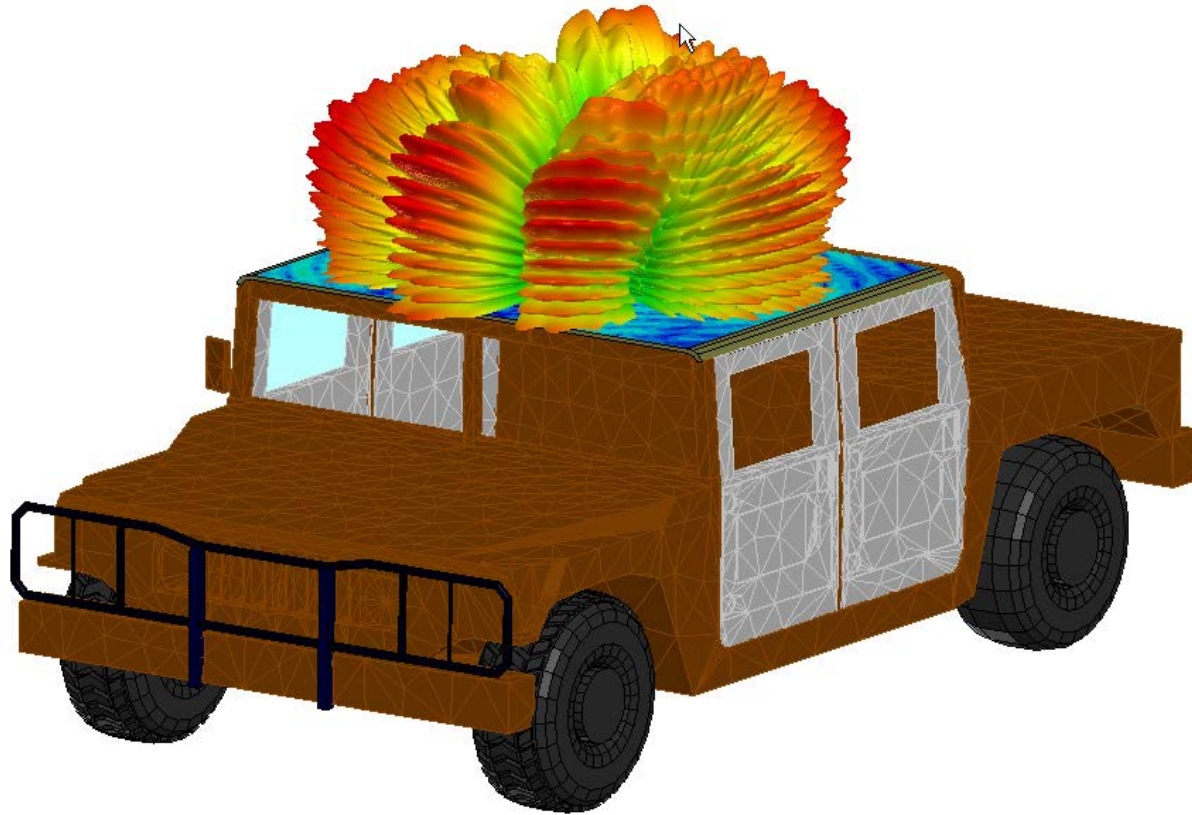
The finite element method (FEM) involves basically four steps:

- (1) Discretize the solution region into a finite number of subregions or elements
- (2) Derive the governing equations for each element based on either a variational approach or Galerkin's method
- (3) Assemble all the elements together in the solution space.
- (4) Solve the resulting system of equations

HFSS (<http://www.ansoft.com/>)

- Commercial FEM package with CAD interface
- Uses adaptive meshing
- Probably the most popular commercial package for antenna applications.
- Written and supported by Ansoft, USA
- Runs under 32/x64 bit Windows platforms, Redhat Linux, Solaris (Sun workstations).
- Has integrated hybrid finite element / boundary integral methods (MoM)
- Kind of expensive!
- Optional optimization package (optimetrics)

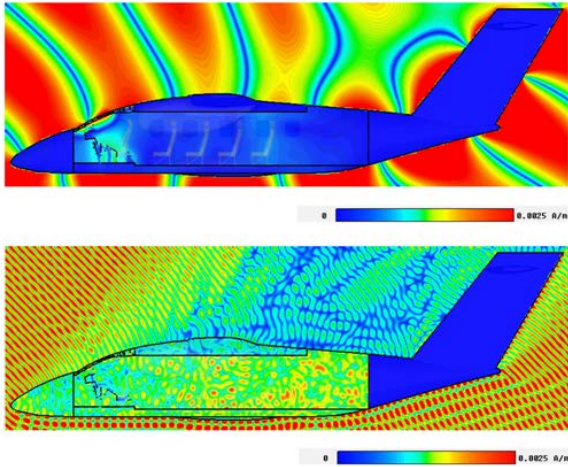
HFSS (<http://www.ansoft.com/>)



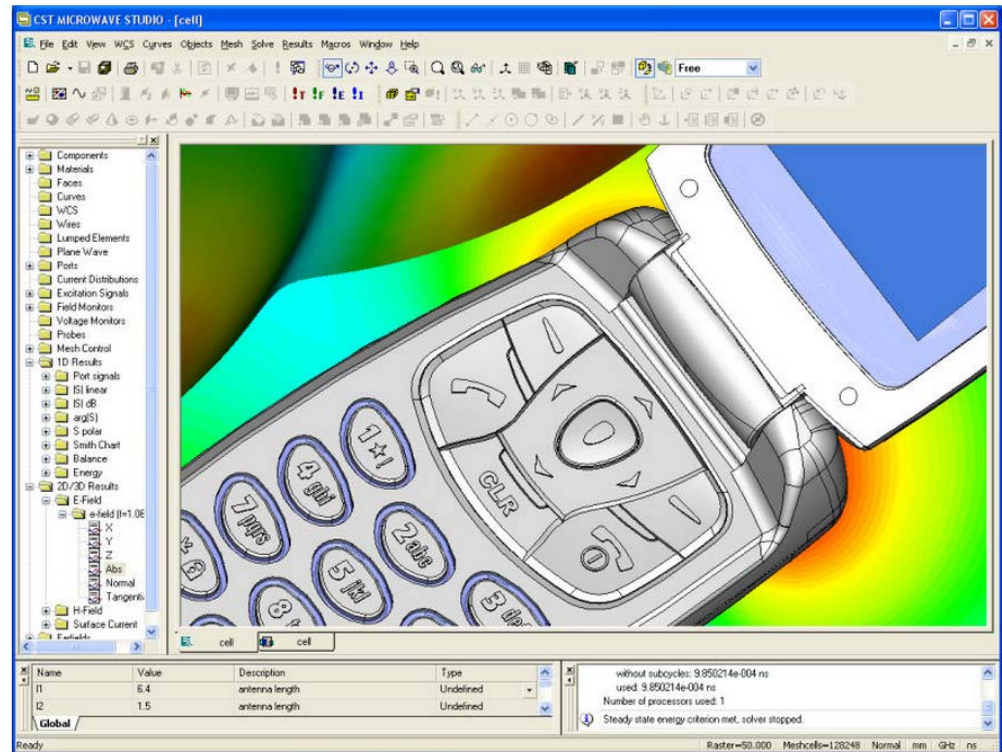
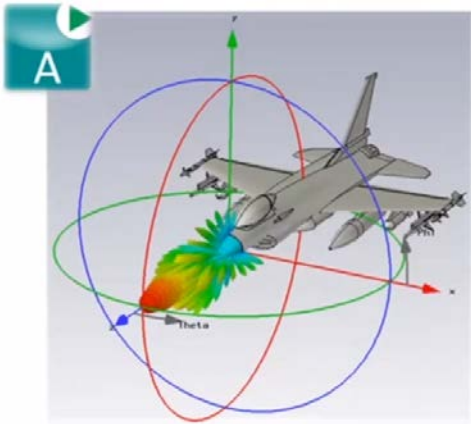
CST Microwave Studio (<http://www.cst.com/>)

- **Commercial FEM, MoM and TLM package with CAD interface**
- **Mature and easy to use interface**
- **Popular program for microwave circuit applications but also very useful for antennas.**
- **Written and supported by CST, International**
- **Runs under 32/x64 bit Windows platforms and Redhat Linux,**
- **Kind of expensive!**
- **Has a specific antenna design option called Magus**

CST Microwave Studio (<http://www.cst.com/>)



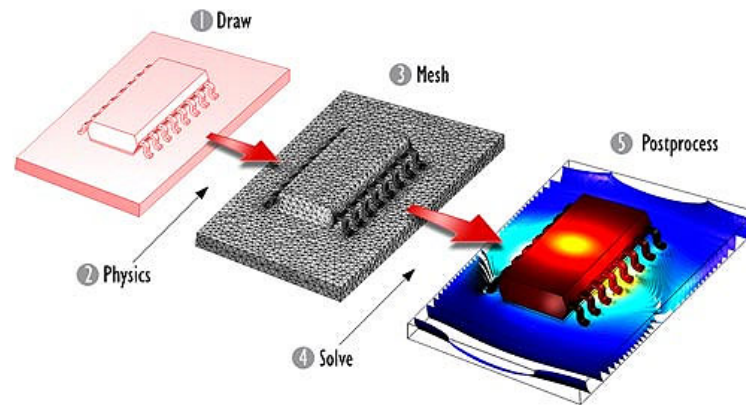
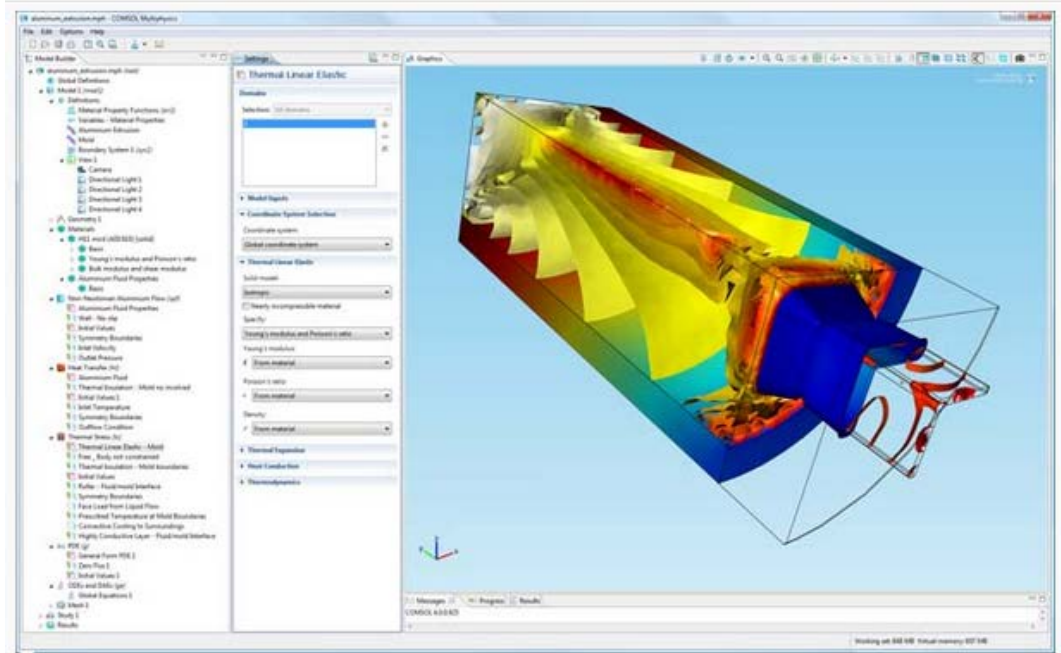
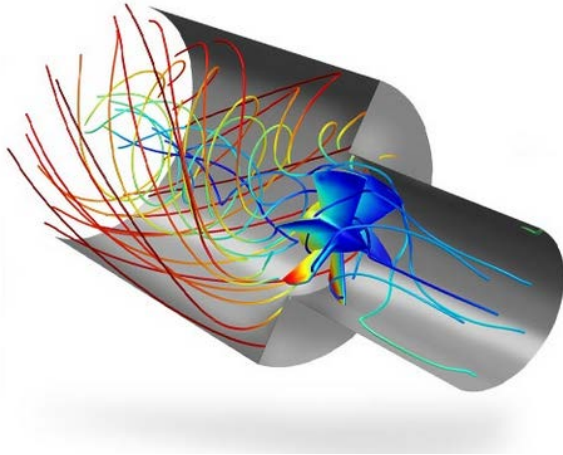
Installed Antenna Performance



Comsol Multiphysics(<http://www.comsol.com/>)

- **Commercial FEM package with CAD interface**
- **Is best known for its ability to solve multiphysics problems**
- **Becoming a very popular program.**
- **Links nicely with Matlab**
- **Easy to learn interface**
- **Runs under 32/x64 bit Windows platforms**
- **Moderately prices**

Comsol Multiphysics(<http://www.comsol.com/>)



References:

1. Clemson site lists all the free EM modeling tools

<http://www.clemson.edu/ces/cvel/modeling/EMAG/free-codes.html>

2. Clemson site lists all the commercial EM modeling tools

<http://www.clemson.edu/ces/cvel/modeling/EMAG/csoft.html>